TEMPORAL TUNING EFFECTS IN THE VISUALLY EVOKED RESPONSE

Ralph E. Parkansky

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This is a partial fulfillment of the requirement for a Master of Science in Physiological Optics

Temporal Tuning Effects in the Visually Evoked Response

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ABSTRACT

TEMPORAL TUNING EFFECTS IN THE VISUALLY EVOKED RESPONSE

By R. E. Parkansky

Electrophysical and psychophysical evidence indicates that there are channels in the visual system that are more sensitive to either spatially-structured stimuli or luminance-modulated stimuli. This sensitivity or tuning was demonstrated by having the largest or optimum response produced by either spatially-structured or luminance-modulated stimuli. The purpose of this study is to determine if the steady-state visually evoked response to three stimuli is significantly and predictably altered by the choice of temporal frequency. It is expected that, for each observer, there will be an optimal temporal frequency or frequencies corresponding to a given pattern size, contrast and intensity. Also, this relationship will likely vary between individuals, but will remain relatively constant for a given observer over time.

Three subjects were each presented with three stimuli. These stimuli were: (1) a square pattern of small checks where each check subtended 15 minutes of arc; (2) a square pattern of large checks where each check softended 57 minutes of arc; and, (3) an unpatterned square stimulus. The check stimuli were presented in such a manner that alternate checks were 180° out of phase with each other and the unpatterned stimulus was presented as a luminance charge. Each stimulus

presertation series contained 20 temporal frequencies presented in numerical sequence with the lowest frequency being 4 Hz and the highest at 23 Hz.

The results of this study were plotted using either the relative amplitude of response or phase change as a function of the temporal frequency of the stimulus. When comparing each subject's response, the relative amplitude, curve shape, stimulus frequency of the largest response, and signal-to-noise ratio were considered. None of the subjects responded in exactly the same manner.

The results of this study were compared to the studies conducted by Regan (1977, 1978), Tyler, Apkarian, and Nakayama (1978), Spekreijse, Estevez and Reits (1977), and van der Tweel and Verduyn (1965). The responses manifested by the subjects in this study were similar to the studies to which they were compared.

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INTRODUCTION

Historical Review

DuBois-Reymond (1848) demonstrated that nerves and muscles are capable of generating independent electromotive forces. The flow of electrical current was shown to be involved not only in muscle contraction but also in nerve conduction and the spike-like action potentials of nerve trunks which were the mechanism of the nerve impulse. Caton (1875) discovered the presence of continuous electrical activity at the exposed cortex of an experimental animal. He described these fluctuating potentials as "feeble currents of the brain." Prawdicz-Neminski (1925) demonstrated two principal frequency ranges of electrical activity in the dog's brain through the intact skull. These two frequency ranges were later found in man and are now known as alpha and beta activity.

Berger (1929) demonstrated that electrical activity could be recorded from the human brain through the intact skull and he was the first to refer to this recording as the electroencephalogram (EEG). He demonstrated that, when a subject's eyes were closed, a long train of regular waves at a frequency between eight and twelve Hertz (Hz) was present and these waves disappeared when the eyes were opened (Berger, 1932). He referred to this phenomenon as the alpha rhythm. Since the alpha rhythm is more prominent in the occipital region, Berger first speculated that it originated in the visual cortex. However, he later found that the alpha rhythm is not necessarily related to the visual

cortex because it can be recorded in other regions of the cortex.

Berger (1932) also observed that these brain waves are slowed in states of depressed function such as sleep activity and that they can be blocked by mental activity and attending to form perception. After the confirmation of brain recordings by Berger, other laboratories began investigating electrical recordings from the brain and expanded upon them. Some specialized in the study of normal patients and basic physiological mechanisms while others looked into the effects of brain lesions.

Adrian and Matthews (1934) confirmed Berger's finding that the presence of a light stimulus could give rise to a characteristic response which could be recorded from the occipital cortex of man. They demonstrated that slow waves of electrical activity were disrupted when light impinged on the retina. In man, this was done by having the subject open his previously closed eyes. This demonstration constituted the first attempt at recording a visually evoked response (VER). At about the same time, electroencephalography was introduced and developed in the United States. These data were of scientific interest but it had little clinical value to the person interested in vision because only a small percentage of normal individuals showed a recordable VER. Since that time, we have come to know that the VER is probably present in all normal individuals but hidden in the ongoing EEG.

Since 1936, great strides have been made in both the recording and the analysis of the EEG. Systematic investigation of evoked responses from the intact human became feasible when Dawson, in 1951, suggested that those potentials regularly evoked by a repetitive stimulus could be

discriminated from the irregularly occurring EEG potentials if all electrical activity subsequent to the stimulus was averaged. It was not until the late 1950's and early 1960's that commercially-built computers became available to facilitate such analysis.

Characteristics of the EEG

The EEG may be defined as a recording of the continuous and spontaneous fluctuations in electrical current generated by the brain. This recording can be obtained through surface electrodes attached to the scalp. The peak-to-peak amplitude of the recorded electrical potential is about 50 microvolts with transient amplitudes as low as 20 microvolts and as high as 200 microvolts. During life, it shows a continual, ever-varying mixture of frequency, phase, and amplitude which is most likely a reflection of metabolic and chemical events (Harding, 1974). Even though the EEG is a real and meaningful signal, it appears unrelated to the incoming stimuli. However, somewhere within the noise of this quasirandom signal, the specific electrical response to each discrete signal is hidden (Perry and Childers, 1969; Harding, 1974).

Characteristics of the VER

Evoked responses, while demonstrating characteristics similar to EEG fluctuations, are not spontaneous but result from specific sensory stimulation (Perry and Childers, 1969). Specifically, the VER is the electrical activity which can be elicited by a visual stimulus and recorded from the occipital cortex. The recordable VER amplitudes are much smaller than the recordable EEG amplitudes. They are typically between 1 and 20 microvolts.

With the use of computers, the VER can be separated from the EEG

because the VER is fixed in time to the stimulus presentation while the ongoing EEG will be random in relationship to the stimulus. Thus, if a stimulus is repetitively presented, and on each occasion the EEG at that time is stored, the common features will slowly add together to produce a clearer evoked response while the random noise which contains both positive and negative ongoing waves will slowly average to zero. This technique is called signal averaging and the result is either an average or sum of the number of discrete responses to a given stimulus (Harding, 1974; Sokol, 1976).

Characteristics of the VER Stimuli

VER stimuli generally fall into one of two spatial classifications, either patterned or non-patterned. The non-patterned stimuli, by definition, have no spatial structure, while the patterned stimuli generally have a spatial structure that is easily defined in terms of spatial frequency or area. Spatially structured stimuli can take several forms; e.g., checkerboards, dots, or bar-grating (Regan, 1972a; Sokol, 1976). Since one of the primary functions of the human visual system is to analyze contours and edges, the use of patterned stimuli has the potential of being more advantageous than the use of non-patterned stimuli (Sokol, 1976).

Temporally, the VER stimuli can be varied in one of three ways. Both the non-patterned and the patterned stimuli can be presented as flashed stimuli which are immediately replaced by a homogeneous non-patterned dark field. This presentation has an on-set/off-set relation-ship which can be varied from that of a stroboscopic presentation (5-to-50 microseconds) (Buddock, 1968) to a longer square wave presentation

(10-to-500 milliseconds). The remaining two methods pertain only to patternoù stimuli. The second method is similar to the first in that there is an abrupt appearance/disappearance of a pattern. However, the pattern, in this method, is immediately replaced by a homogeneous, non-patterned filed which has the same mean luminance as the patterned field. The third method is frequently referred to as "pattern reversal." Here the pattern is again presented to the subject, but instead of being replaced by either a dark field, as in method one, or by a light field, as in method two, it is replaced by a pattern which is its spatial compliment; the result is a counterphase alternation of the dark and light phases with a constant mean luminance (Sokol, 1976).

Stimuli that are presented by methods one and two can be presented as isolated transient events and all these methods can be used in repetitive trains. The repetitive trains produced by either square wave or sine wave modulation can have the luminance changes quantified in terms of modulation depth. The modulation depth (M) is typically expressed as the ratio of the change in luminance (L) divided by the mean luminance (L):

$$M = \frac{L}{L_{o}} \times 100$$
Where $L = \frac{Lmax - Lmin}{2}$
and $L_{o} = \frac{Lmax + Lmin}{2}$

Imax and Lmin are the luminances of the bright and dark areas, respectively, at the time of maximum contrast.

Although it might intuitively seem that the absolute change in stimulus luminance would be the most important determinant of evoked potential amplitude, the absolute change is often less important than the percentage change in luminance (Regan, 1972a). Therefore, an important feature of a stimulus in which the luminance is modulated is that the time-average luminance is held constant. The percentage luminance change can, therefore, be varied without changing the mean stimulus luminance level which determined adaptation (Kamp, Sem-Jacobson and Storm van Leeuwen, 1960).

Types of VER's

Visually evoked responses, as currently studied, fall into two major classes according to the method by which the stimulus is presented. VER's are classified as either transient responses or as steady-state responses (MacKay and Jefferys, 1973). Transient VER's, polyphasic in form and 200-500 milliseconds in duration, are evoked by stepwise changes in one or more parameters of stimulation at discrete points in time. These are usually separated by intervals long enough to allow the system to settle (somewhat) before the next stimulus. Regan (1977) refers to the transient VER as being produced when the visual system is given a repeated "kick" at intervals which are sufficiently long so that the response to one stimulus has died away before the arrival of the next stimulus.

Steady-state VER's are evoked by stimuli in which the parameter of interest is rhythmically modulated above and below a steady mean level, at a frequency high enough for the visual system to develop a rhythmic and stable response (MacKay and Jefferys, 1973). Steady-state VER's are produced when the visual system is "gently shaken" by an indefinitely

long train of repetitive stimuli which overlap to such an extent that, in general, no single response cycle can be associated with an individual stimulus and the running averages of both amplitude and phase are constant with time (Regan, 1972b; Regan, 1977). The point at which the VER is no longer transient and becomes steady-state is not clear; with sinusoidally modulated light, it can occur at a frequency as low as 4 Hz (Sokol, 1976; Levi and Harwerth, 1978), or as low as 3 Hz with flashing lights (Harding, 1974). While both the transient and steady-state VER's can be described in terms of voltage change as a function of time, only the steady-state VER can be described in terms of amplitude of phase as a function of the spatial frequency or the temporal frequency of the stimulus.

In a comparison between the two types of responses, Milner, Regan, and Heron (1972) found it more advantageous to study the steady-state responses than the transient responses for the following reasons: (1) the steady-state responses do not seem to be influenced, as the transient responses are, by the psychological state of the subject; (2) there is less intrusion of muscle and EEG activity with the steady-state VER recording as well as reduced effects of moment-to-moment variability; and, (3) the so-called Fourier-analyzed steady-state method of Regan's is much faster than conventional transient response averaging (up to a hundred times quicker). If one is concerned with studying the psychological variables associated with the VER, the steady-state response reportedly contains little or no information, as there appears to be a trade-off between speedy recordings and information - "greater speed, less information" (Regan, 1977).

Patterned or Contrast Modulated VER's

It can be demonstrated that a change in either the contrast or the spatial frequency of the stimuli can cause a change in the VER. Using transient presentations, Earter and White (1968) demonstrated that the relative peak-to-trough amplitudes of the VER are very sensitive to the sharpness of contour of a patterned visual stimulus. They focused and defocused patterned stimuli with a range of lenses and found that the responses to high spatial frequency stimuli (small checks) are more sensitive to a blurred target than are the responses to low spatial stimuli (large checks). When the high spatial frequency stimuli were blurred, there was a greater decrease in the peak-to-trough amplitude than when the low spatial frequency stimuli were blurred. Using steady-state presentations, Spekreijse (1966) and van der Tweel and Spekreijse (1968) demonstrated that, when the borders between spatial stimuli (checks) were masked, the responses decreased.

Regan and Richards (1971, 1973) demonstrated that the sensitivity of the visual system to high spatial frequency stimuli (small checks) was different than the sensitivity to low spatial frequency stimuli (large checks). They used a series of checks having the high fundamental spatial frequency of 10 cycles per degree (cpd) or three minutes of arc per check at one end and the low fundamental spatial frequency of 1 cpd or 30 minutes of arc per check at the other. They found that, when these checks were modulated at a temporal frequency of 6 Hz, the largest relative amplitude was found with the 11-minute check. There was no change in the VER amplitude or check size relationship when either the fixation distance or the convergence of the eyes was changed. There was a shift to a peak

amplitude at the five-minute check when the brightness was increased. When each of the stimuli was defocused, the greatest difference in the VER was found at the small check or high spatial frequency end of the series. The defocusing caused a 30-percent reduction of the VER amplitude for the small checks, a 65-percent increase of the VER amplitude for large checks and an elimination of the peak at 11 minutes. Regan and Richards (1971, 1973) reasoned that small-check VER's are almost completely contrast specific and dependent upon sharp focusing of the stimulus while large-check VER's are elicited by, at least to some degree, the local flicker within each check.

Unpatterned or Luminance Modulated Stimuli

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Whether presented as an isolated transient event or in a repetitive steady-state train, the VER elicited by changing the luminance of an unpatterned stimulus field differs from the VER elicited by changing the contrast of a pattern. It appears possible that the unpatterned response may be mediated by the activity of the central 6-12 degrees of the visual field providing a means of studying the temporal frequency characteristics of the visual system; e.g., studying latency times (Halliday, McDonald, and Muskin, 1972). However, the amplitudes of these temporal responses do not correlate with perceived flicker threshold or with sensory magnitude (Regan, 1977).

In studies by van der Tweel and Verduyn Lunel (1965) and Regan (1970), visual responses to modulated unpatterned stimuli have been categorized according to the temporal frequency of the stimulus. In each study, the temporal frequencies were divided into three groups. Van der Tweel and Verduyn Lunel (1965) placed the temporal frequencies below 9 Hz in

the low group, the frequencies from 9 Hz through 18 Hz in the middle group, and all the frequencies above 18 Hz in the high group. Regan (1970) centered the low-frequency group near 10 Hz, the middle-frequency group in the region of 16 Hz, and the high-frequency group above 50 Hz.

Van der Tweel and Verduyn Lunel (1965) found that the responses at stimulation frequencies below 9 Hz generally showed considerable distortion, even at modulation depths of 10 percent or less. In many cases, the second harmonics were larger in amplitude than the fundamental. This was particularly true at stimulation frequencies around 5 Hz. In some subjects, the change from undistorted to distorted (non-harmonic to harmonic) responses took place abruptly in a narrow stimulation frequency band. Independent stimulation of the eyes at 5 Hz by two light sources 180° out of phase did not lead to cancellation of the response, but yielded amplitudes comparable at least with those of one-eye stimulation.

The responses to sinusoidally modulated light at frequencies from 9 to 18 Hz generally approximated the sine wave form if diffuse illumination of the two eyes was used. When the eyes were independently stimulated 180° out of phase at 11 Hz, the response at 11 Hz had almost disappeared and only a response mainly at the second harmonic was left. These investigators (van der Tweel and Verduyn Lunel, 1965) noted that, in this frequency range, the alpha rhythms had an independent existence; i.e., the response to the light stimulation and the alpha rhythms can exist together at different frequencies.

Responses at the temporal stimulation frequencies above 18 Hz were generally obtained only with high light intensities (10,000 Trolands).

In some subjects, frequencies from 25 to 35 Hz showed a pure second harmonic response, whereas at lower stimulation frequencies responses at the fundamental frequencies prevailed (e.g., at a stimulation frequency of 27 Hz and modulation depth below 25 percent, a response at the second harmonic predominated and was considerably larger than the response obtained at stimulation frequencies in the 50 Hz range). Independent stimulation of the eyes 180° out of phase at 27 Hz evoked responses with comparable amplitudes to those obtained by the stimulation of one eye alone.

Regan (1970) also classified unpatterned steady-state evoked potentials into three different frequency regions. These were designated the low, medium, and high frequency classes. The low-frequency region is centered near 10 Hz. In many subjects, there is a particular stimulus frequency near 10 Hz for which the amplitude of the evoked potential is larger than at neighboring frequencies. This is also the same frequency range at which spontaneous alpha activity is most prominent. However, Regan (1966) points out that the alpha frequency is quite different and independent of the stimulus. In general, stimulus color intensity and field size have little effect on the shape and peak frequency of the amplitude versus frequency curve for the evoked potential near 10 Hz (Regan, 1970).

The second frequency class includes steady-state evoked potentials whose amplitudes are maximal for medium stimulus frequencies in the region of 16 Hz. The shape of the amplitude versus frequency curve for evoked potentials in this frequency region can be strongly influenced by red light with a blue adapting field and by the size of the stimulus

field (Regan, 1968). Also, this medium frequency range of evoked potentials may have little relation to the power spectrum of the spontaneous EEG activity and does not give a strong second harmonic response (Regan, 1970).

The last frequency range Regan (1970) found was at high frequencies where the maximum response amplitudes occur at about 50 to 55 Hz. For the high frequency as well as the low frequency response ranges, the amplitude versus frequency curve seems to be similar in shape to the corresponding power spectrum of spontaneous EEG activity. The high frequency evoked potentials may be differently distributed over the scalp and be less dependent on stimulus intensity than evoked potentials of the medium frequency range. The low, medium, and high frequency responses may be generated by different and/or overlapping populations of neurons that may differ functionally and anatomically (Regan and Heron, 1969; Milner, Regan, and Heron, 1972).

Spekreijse (1966) used sinusoidally-modulated unpatterned light. The results indicate that a relative peak of the fundamental was found in the 10-Hz range. His data show that there are significant differences in the relative peaks of the fundamental as a function of stimulus frequency across subjects.

Response Channels

The differences between the VER to contrast-modulated stimuli and luminance-modulated stimuli has been attributed to two types of detection channels or pathways in the visual system — one for detecting spatial contrast and one for detecting luminance changes. This dichotomy has been confirmed both electrophysiologically and psychophysically.

Electrophysiologically, this dichotomy in the visual system has been found to remain from the retina through the lateral geniculate nucleus (Cleland, Dubin and Levick, 1971) to the occipital cortex (Ikeda and Wright, 1974). These two channels are named for the type of retinal ganglion cells that are found in the pathway. The channel that responds to spatial contrast is called either the X-type (Enroth-Cugell and Robson, 1966) or sustained type (Cleland, et al, 1971). The channel that responds to luminance changes is called either the Y-type (Enroth-Cugell and Robson, 1966) or transient type (Cleland, et al, 1971). Sustained channel responses are more affected by a sharply focused stimulus than are transient channel responses (Ikeda and Wright, 1972). The sustained cells linearly sum the effects of stimuli presented to different parts of the receptive field (which is the area on the retina that the cells influence), whereas the transient cells do not (Enroth-Cugell and Robson, 1966). The sustained cells have longer response latencies, they respond to higher spatial frequencies, they are excited by slower movements of small targets, and they generally give a response of longer duration than do the transient cells (Hoffman, Stone and Sherman, 1972; Ellenberger, Shuttlesworth and Palmer, 1977). In other words, the sustained cells respond better to slow-moving, sharply focused, high spatial frequency targets while the transient cells respond better to large, fast-moving, blurred, low spatial frequency targets.

This two-channel characteristic may be demonstrated electrophysiologically in humans with VER's elicited from high spatial frequency stimuli such as small checks (Ellenberger et al, 1977). VER's elicited by small checks are mediated by the central retinal area (30 minutes of arc) providing a means of studying the spatial frequency characteristics of the visual system while the VER's elicited by low spatial frequency stimuli, such as large checks, are mediated by the more peripheral retinal area (4-6 degrees) providing a means of studying the temporal frequency characteristics of the human visual system (Ellensberger, et a), 1977).

Psychophysical evidence has shown that low spatial frequency channels are particularly sensitive to transient stimulation produced by rapid motion (Tolhurst, 1973), flicker (Keesey, 1972; Kulikowski and Tolhurst, 1973), and abrupt stimulus enset (Breitmeyer and Julesz, 1975; Tolhurst, 1975), and these channels respond with a shorter latency than do high spatial frequency channels (Breitmeyer, 1975). The high spatial frequency channels (Breitmeyer, 1975). The high spatial frequency channels seem to prefer slowly moving, or stationary, stimuli (Keesey, 1972; Kulikowski and Tolhurst, 1973) or stimuli presented by long flashes of 800 milliseconds (Tolhurst, 1975).

Kulikowski and Tolhurst (1973) demonstrated that the manner in which these channels responded to on/off and alternating patterns is indirect evidence for sustained and transient behavior. Two distinct detection thresholds for a temporally-modulated stimulus were found; at one contrast, the temporal character became evident; at a second contrast, the spatial structure of the stimulus became evident. The two thresholds varied independently with change in the temporal or spatial frequencies of the stimuli. The simplest explanation given for these differences was that the two thresholds were mediated by two independent sets of neurons with ifferent spatial and temporal properties. Kulikowski and

Tolhurst (1973) used the term "movement-analyzers" for those neurons responsible for flicker detection and the term "form-analyzers" for those neurons responsible for pattern recognition. They suggested that the neurons responsible for pattern recognition were similar to sustained cells because they did not decline in sensitivity at low temporal frequencies and they responded equally well to alternating and on/off gratings up to about 8 Hz. The neurons responsible for flicker detection were compared to transient cells because they responded better to low and medium spatial frequencies, they showed a pronounced decline in sensitivity at low sinusoidally-modulated temporal frequencies, and they responded twice as well to alternating phase grating than gratings that were turned on and off at the same temporal frequency (Kulikowski and Tolhurst, 1973).

Spatial and Temporal Tuning

Electrophysical and psychophysical evidence has been presented in the preceding sections that indicates there are channels in the visual system that are more sensitive to either spatially-structured stimuli or luminance-modulated stimuli. This sensitivity or tuning was demonstrated by having the largest or optimum response produced by either spatially structured or luminance modulated stimuli; i.e., the sustained channel was tuned to higher spatial frequencies than the transient channel while the transient channel was tuned to higher temporal frequencies than the sustained channel.

The notion that large and small checks demonstrate a selectivity to different temporal frequencies for an optimal response has been referred to as temporal tuning (Regan, 1977, 1978). Temporal tuning provides a

major distinction between VER's produced by flickering an unpatterned stimuli and VER's produced by the reversal of pattern stimuli (i.e., checks) (Regan, 1978). The VER's for fine patterns are optimal at low temporal frequencies (5-7 Hz), the VER's for large patterns are optimal at higher temporal frequencies (10-18 Hz), depending on the field size. Modulated unpatterned stimuli produce VER's that are optimal at temporal frequencies similar to the large check temporal frequencies (Berhman, Nissim and Arden, 1972; Regan, 1977; Regan, 1978). Regan (1978) suggests that the differences are due to responses from "pattern components" and "local flicker components." The VER's for fine patterns are chiefly due to the pattern components, the VER's for large patterns are due to a combination of both patterns and local flicker components, and the VER's for the unpatterned stimuli are chiefly due to the local flicker component. These responses may parallel the two-channel dector arrangement found psychophysically in humans (i.e., the pattern channel is more sensitive to slow moving, high spatial frequency stimuli and the flicker channel is more sensitive to fast moving, low spatial frequency stimuli) (Regan, 1978).

Tyler, Apkarian and Nakayama (1978) described a study that detailed the characteristics of the steady-state VER as a function of spatial frequency. They presented several spatial frequency stimuli at the same temporal frequency and measured spatial frequency tuning as a function of the temporal frequency for four observers. They observed that the temporal frequency tuning was very narrow and this tuning depended on spatial frequency. The sensitivity of this tuning was demonstrated when a large peak at one spatial frequency was completely altered by

a 10% change in the temporal frequency. They also observed that spatial frequency tuning was narrow. In some cases, there was a single peak of spatial frequency sensitivity at a given temporal frequency. A third observation was that all subjects showed a tendency toward spatiotemporal reciprocity. There was a pronounced tendency for high temporal frequency responses to be limited to the lower spatial frequency region and the high spatial frequency responses occur at lower temporal frequencies. The fourth observation was that multiple response peaks occurred at different spatial and temporal frequencies for different observers. While this inter-observer variability was evident, the within observer variability was very low. Replications of spatial frequency functions were obtained from the same observer over months. The final observation was that complex pattern responses of multiple peaks in spatial frequency tuning can occur in temporal regions where little or no response to a uniform field was evident. The authors claimed that this observation was important because it ruled out explanations of the complexity of pattern responses based on interactions between a single luminance response and a single pattern response.

PURPOSE

The purpose of this study is to further explore the relationship between temporal and spatial frequency in the visually evoked response. Specifically, this study will try to determine if the response to three checkerboard patterns is significantly and predictably altered by the choice of temporal frequency. The following postulates are to be tested:

(1) for each observer, there will be an optimal temporal frequency or

frequencies corresponding to a given pattern size, contrast, and intensity; and (2) this relationship will likely vary between individuals but will remain relatively constant for a given observer over time.

METHOD

Subjects

One male and two female observers, 25 through 31 years of age, were used in this study. All three observers had clear media and normal fundi. The male observer and one female observer were myopic but were corrected to a Snellen acuity of 20/20 or better. The third observer was emmetropic with a Snellen acuity of 20/20 or better. Normal accommodation and natural pupils were used.

Recording Apparatus

Organization of the recording apparatus used in this study is diagrammed in Figure 1. The visually evoked responses were obtained by means of a monopolar surface electrode (Beckman) placed on the subject's midline two centimeters above the inion and referenced to two linked electrodes located on the earlobes. A ground electrode was placed on the subject's forehead. Each subject was seated in a shielded room. The responses were amplified via a Grass P-15 amplifier with a gain of 1000 and a high and low 6 db roll-off of 3000 and 0.01 Hz, respectively. One hundred twenty-eight responses were averaged in a Nicolet 1070 signal averager that was interfaced with a Hewlett-Packard 2100 computer programmed to execute a Fourier analysis of the averaged data. Care was taken to insure maximum resolution of the Fourier analysis and to avoid windowing of artifacts. This was done by insuring that an exact integer

number of stimulus presentations (four repetitions per sweep) was incorporated in the data window. The signal averager's external address was electronically stepped 256 times for each pattern reversal, thus ensuring an exact integer number of stimulus presentations (4) within the recording window and eliminating the need to consider window effects in the transformation of the data (Levi and Walters, 1977).

PROCEDURE

Each subject was presented with three stimuli. These stimuli were:

(1) a 16-degree square pattern of small checks where each check subtended

15 minutes; (2) a 16-degree square pattern of large checks where each

check subtended 57 minutes; and, (3) an unpatterned square stimulus

which subtended 17 degrees. These stimuli were presented in the center

of a square screen that was 21 degrees wide and 21 degrees high at a

distance of two meters in front of the subject.

The two-check stimuli were produced from vectograph slides in a checkerboard arrangement with alternate check polarization aligned 45 degrees on either side of vertical (Millodot and Riggs, 1970; Behrman, Nissim and Arden, 1972; Walters and Yolton, 1976). The stimuli were projected by two Kodak Carousel projectors. One projector provided the background while the other projected the check pattern. A rotating polaroid disc was placed in front of the lens of the pattern projector. The rotation of the disc produced a sinusoidal modulation in such a way that alternate checks were 180 degrees out of phase with each other. A piece of reflecting silver tape was positioned on the disc so that an electrical pulse was produced once every revolution for

synchronization and triggering purposes. The unpatterned stimulus was produced from a vectrograph slide with its axis of polarization in only one direction.

The advantages in using the above stimulus arrangement are: (1) the number of measurable response parameters is reduced (e.g., Fourier components); (2) pattern reversal occurs automatically and precisely (Arden, Bodis-Wollner, Halliday, Jefferys, Kulikowski, Spekreijse, and Regan, 1977); (3) at high contrast, imperfections in the display can be ignored (Arden, et al, 1977); and, (4) precise fixation is not necessary (Arden, et al, 1977).

The stimuli were quantified in terms of luminance and modulation depth with a Pritchard photometer. The average luminance of the stimuli were: (1) 100 candelas per square meter for the small checks; (2) 115 candelas per square meter for the large checks; and, (3) 97 candelas per square meter for the unpatterned stimulus. The average luminance of the background was 72 candelas per square meter. The average percent modulation depth of the stimuli was 25 percent.

Each stimulus presentation series contained 20 temporal frequencies presented in numerical sequence in either an ascending or decending order. The lowest temporal frequency was 4 Hz and the highest was 23. The length of time required for each stimulus series was 35 minutes.

Once the amplitude and phase data from the Fourier components were calculated, the amplitude of the fundamental component and phase were plotted as a function of the stimulus temporal frequency. Curve fitting was done using a polynomial regression with either three or four degrees of freedom. The plots of these data were achieved with a Hewlett-Packard

7010A X-Y Plotter. All data represented in these plots were required to have a signal-to-noise ratio of at least two. That is to say, in this study, the fundamental component of the VER in a single averaging session was required to be at least twice the relative magnitude of the averaged noise level for that stimulus frequency in order for it to have been considered valid data. This criterion was empirically determined based on pilot work.

RESULTS

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The results of this study are graphically displayed in Figures 2 through 15. Figures 2 through 12 were plotted using a polynomial regression with four degrees of freedom while Figures 13, 14 and 15 were plotted using three degrees of freedom. The raw data from which these plots were produced are contained in Appendix A. In all figures, the X-axis displays the temporal frequency (Hz) of pattern reversal or luminance change (for the unpatterned stimulus only). The Y-axis represents either the relative amplitude of the fundamental VER component with a positive number (Figures 2 through 12) or the relative magnitude of the phase difference between the stimulus and the fundamental VER component with a negative number (Figures 13, 10 and 15) (Spekreijse, Estevez and Reits, 1977). As noted in the previous section, the criterion for selecting data for display was a signal-to-noise ratio of two or greater in any part. Occasionally, subjects produced no record above the criterion for an entire run. This phenomena will be discussed later.

Combined Presentations vs Single Presentation

When describing the differences between the responses to single stimuli from each subject (intersubject differences) and the differences between

the response to each stimulus from a single subject (intrasubject differences), data from both a single trial and multiple trials were used. The figures representing the data from a single trial had their data points included in the figure. In order to give the reader a perspective relating combined vs single trial raw data, Figures 2, 3 and 4 display a comparison between the combined data for each presentation of a stimulus and the data from a single stimulus series. Figures for the combined data, Figures 2A and 3A, contain the data collected from five stimulus series collected over a six-week period for the 15-minute and 57-minute checkerboard stimuli for subject RM. Figure 4A contains data collected from six series of the unpatterned stimulus collected over the same time period for subject RM. Figures 2B, 3B and 4B are presentations of one of the stimulus series contained within Figures 2A, 3A and 4A respectively. The single series presentations allow the use of the actual data points collected from a single series. The use of all of the data points collected for the combined series on a single graph would be too congested to be meaningful.

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Figures 2A and 2B display the data collected from subject RM using the 15-minute patterned stimulus. The maximum amplitude for both the combined trial (2A) and the single trial (2B) peak at the temporal frequency of approximately 10 Hz. Figures 3A and 3B display the data collected from subject RM using the 57-minute patterned stimulus. The maximum amplitudes for both the combined trials (3A) and the single trial (3B) peak at the temporal frequency of about 18 Hz. Figures 4A and 4B display the data collected from subject RM using the unpatterned stimulus. The maximum amplitudes for both figures peak at a temporal

frequency of 16 Hz.

- Though the maximum amplitude of the combined vs single responses from each run are different, the shape of the curves for the combined presentations and single presentation for each stimulus are very similar. This fact demonstrates subject stability over time for the subjects used in this study.

Intersubject Differences in VER's for Each Stimulus

Figures 5, 6 and 7 graphically display the differences in the response curves between each subject for the same stimulus condition.

Figures 5A, 5B and 5C display the response curves from each subject elicited by the 15-minute patterned stimulus. These figures indicate the relative magnitude of the responses for subjects RM, LP and RR respectively; RM's responses peak at 10 Hz, LP's peak at 7 Hz, and RR's responses peak at about 4 Hz. Figure 5D combines Figures 5A, 5B, and 5C on one set of axes for ease of comparison. Each of the three subjects elicited different response curves to the 15-minute check stimulus. Subject RM's data were plotted as a unimodal curve while LP's data were plotted as a bimodal curve with a primary peak at 7 Hz and a secondary peak at 21 Hz. LP's response curve had a dramatic rise and fall at the two peaks while RM's response curve had a definite peak but without the dramatic rise and fall of the response curve. The response curve for RR had the least definite peak except at the initial frequency of 4 Hz. The relative magnitude of the primary response curves for subjects RM and LP exceeded 250 units of amplitude while the secondary peak for LP was above 100 units. The peak of the response curve for RR was below 100 units with a commensurate low signal-to-noise ratio. It is interesting to note that when the data in Figure 5B is fit with a curve with three degrees of freedom, it is unimodal.

Figures 6A, 6B, and 6C graphically display the data elicited by the 57-minute patterned stimulus from subjects RM, LP and RR respectively. RM's response curve peaks at 17 Hz, LP's response curve peaks at 7 Hz and RR's response curve peaks at 9 Hz. Figure 6D compares all three functions on a single scale and illustrates the difference in response curves to the 57-minute stimulus for each subject. All three curves were unimodal with definite peaks. RM's response curve had the greatest relative magnitude at about 200 units, while LP's curve peaked above 150 units and RR's curve peaked at relative magnitude of slightly above 100 units.

Figures 7A, 7B and 7C graphically display the response curves from each subject elicited by the unpatterned stimulus. This stimulus was modulated at a temporal frequency twice that of the luminance change frequency used for the patterned stimuli so that the response frequency for both types of stimuli would be the same. These figures display the individual response curves from subjects RM, LP, and RR respectively. This stimulus produced a maximum relative amplitude at 15 Hz for subject RM and at 17 Hz for subjects LP and RR. While there are large differences in the magnitude of the responses, all three curves peak within the region of 15 to 17 Hz.

Figure 7D combines the response curves to the unpatterned stimulus

The response frequency for pattern alternation stimuli is most frequently found to be at the frequency of the pattern alternation rate or twice the rate of luminance change.

for each of the three subjects. All three curves were unimodal with definite peaks for subjects RM and LP at 15 Hz and 17 Hz respectively. RR's response curve had a less definite peak at 17 Hz. Of the three response curves, the most dramatic peak was found for subject LP's data at a relative magnitude between 600 and 700 units. The least dramatic peak was found for RR's data at a relative magnitude of approximately 150 units. RM's response curve peaked at a relative magnitude of almost 500 units. Visual inspection would suggest that while the amplitudes vary, there is considerable similarity in the shape of the response curves produced by the unpatterned stimulus.

The patterned background responses were achieved by presenting each subject with an unmodulated patterned visual stimulus. Figures 8A, 8B and 8C depict the response curves from each subject elicited by the patterned background noise. These figures display the response curves from subjects RM, LP and RR respectively. RM's response curve peaks at 4 Hz with approximately 45 units, LP's peaks at 8 Hz with approximately 35 units, and RR's response curve peaks at 6 Hz with approximately 32 units. Subject RM's data were plotted as a slightly bimodal curve with the greatest amplitude at 4 Hz with 45 units and a smaller secondary increase in amplitude of approximately 40 units at 16 Hz. Subject LP's response curve is definitely bimodal with a primary peak at 8 Hz and a secondary peak at 22 Hz with an amplitude of approximately 25 units. Subject RR's response curve peaks at 6 Hz and gradually decreases to its lowest amplitude of 25 units at 23 Hz.

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The unpatterned background responses were achieved by presenting each subject with the luminous visual stimulus without modulation.

Figures 9A, 9B and 9C depict the response curves from each subject elicited by the unpatterned background noise. These figures display the response curves from subjects RM, LP and RR respectively. RM's response curve peaks at 4 Hz with approximately 42 units of amplitude, LP's also peaks at 4 Hz with an amplitude of approximately 47 units, and RR's response curve peaks with an amplitude of approximately 37 units also at 4 Hz. Each subject's responses were plotted as a unimodal curve with the greatest amplitude at the lowest temporal frequency. In each curve, the relative amplitudes of response gradually decreased as the temporal frequencies increased.

Intrasubject Differences in VER's for each Stimulus

Figures 10, 11 and 12 plot the signal and noise data on the same coordinate for each of the three subjects. The upper curve in each case represents the evoked potential data while the lower curve presents the ambient noise.

Figures 10A, 10B and 10C display the response curves from subject RM to the 15-minute check stimulus, the 57-minute check stimulus, and the unpatterned stimulus respectively. Figures 11A, 11B and 11C display response curves from subject LP to the 15-minute check stimulus, the 57-minute check stimulus, and the unpatterned stimulus respectively. Similarly, Figures 12A, 12B and 12C display response curves from subject RR to the 15-minute check stimulus, the 57-minute check stimulus, and the unpatterned stimulus respectively.

Subject RM responded differently to each of the three stimuli as shown in Figures 10A, 10B and 10C. The peak from the 15-minute stimulus occurred at 10 Hz, the peak for the 57-minute stimulus at 17 Hz and for

the unpatterned stimulus at 15 Hz. The unpatterned stimulus produced the response with the greatest relative magnitude, over 400 units. The 15-minute stimulus produced the next greatest relative magnitude response with about 250 units. The 57-minute stimulus produced the peak with the least relative magnitude of less than 200 units. In each of these cases, the relative magnitude of the background noise response curve was less than 70 units.

Subject LP also presented a different response to each of the three stimuli as shown in Figures 11A, 11B and 11C. The response curve to the 15-minute stimulus was bimodal with a primary peak at about 7 Hz and a secondary peak at about 21 Hz. There was a dramatic rise and fall in amplitude on either side of the primary peak frequency. The unimodal response curve to the 57-minute stimulus also peaked at about 7 Hz. However, the rise and fall of this response curve was much less dramatic than found with the 15-minute stimulus. The unimodal response curve to the unpatterned stimulus had the greatest relative magnitude of any of the three stimuli with a magnitude greater than 400 units at about 17 Hz. The 15-minute stimulus produced the response curve with the next greatest relative magnitude with a primary peak of about 240 units and the secondary peak of about 160 units. The 57-minute stimulus produced the least relative amplitude with slightly more than 160 units at the peak frequency. The background noise response curve produced by each of the (stationary) stimuli was less than 75 units.

Figures 12A, 12B and 12C illustrate subject RR's responses to each of the three stimuli. The 15-minute stimulus resulted in a response curve with a peak at 4 Hz. The response curve, however, was not greater

than twice the background noise as seen in Figure 12A. In fact, the relative magnitude of the response curve was less than the relative magnitude of the background noise at 20 and 23 Hz. In Figure 12B, the data from the 57-minute stimulus produced a unimodal curve with a peak at 9 Hz with the greatest relative amplitude of approximately 90 units. The unpatterned stimulus also produced a unimodal response curve with a peak at 17 Hz with a relative amplitude of 150 units as seen in Figure 12C. While the signal-to-noise ratio at the peak temporal frequency was much greater than two, the signal-to-noise ratio at the lowest temporal frequencies, as seen in this figure, were much less than two. In fact, the background response was greater than the stimulus response at 4 and 6 Hz.

Clearly, subject RR's data has the poorest signal-to-noise ratios. Although his visual function was not materially different from the other subjects by clinical standards, his VER amplitudes (Figure 12A) are certainly substandard. The situation improved somewhat for the large check data (Figure 12B). In addition, unpatterned response data (Figure 12C) are respectable from a signal-to-noise ratio point of view for the middle and higher temporal frequencies.

The overview of the amplitude data provided by Figures 10, 11 and 12 is interesting. The unpatterned stimulus produced the largest response from each subject. The 57-minute patterned stimulus produced the next largest response for subject RR. The 57-minute stimulus produced the lowest responses for subjects RM and LP while the lowest for subject RR was produced by the 15-minute stimulus. Each stimulus produced essentially unimodal response curves for subjects RM and RR. Subject LP

had a definite bimodal response to the 15-minute stimulus while the other two stimuli produced unimodal response curves. Also, subject LP was the only subject whose peak responses to the patterned stimuli and the patterned background noise nearly coincided. Figure 8B displays a response curve from the patterned background noise which was bimodal with the primary peak at 8 Hz and the secondary peak at 22 Hz. Figure 11A displays a bimodal response curve from the 15-minute stimulus with the primary peak at 8 Hz and a secondary peak at 21 Hz. Figure 11B displays a unimodal response curve from the 57-minute stimulus with the peak relative amplitude also at 7 Hz. While these peaks did nearly coincide, the signal-to-noise ratios were well above two for this subject. The signal-to-noise ratios for subjects RM and LP were well above two in all cases while the signal-to-noise ratio for the patterned stimuli were less than two for subject RR. The signal-to-noise ratio produced by the 57-minute check stimulus from subject RR was 3:1.

Phase Characteristics

Figures 13, 14 and 15 display the plots of the relative phase difference between the stimulus and the fundamental VER component as a function of stimulus frequency (Spekreijse, Estevez and Reits, 1977). The phase (Y-axis) is shown in radians (e.g., $2\,\%$ radians equals 360°). The curves for these plots were fit with three degrees of freedom.

Figures 13A, 13B and 13C display the phase differences for subject RM as found with the 15-minute stimulus, the 57-minute stimulus and the unpatterned stimulus respectively. Figures 13A and 13C show a nearly linear relationship while Figure 13B shows a small "jump" in the phase difference between 17 Hz and 18 Hz. The curve plotted in Figure 6A

represents the amplitude data for the same stimulus array with a peak located at 17 Hz.

Figures 14A, 14B and 14C display the phase differences for subject LP produced by the 15-minute stimulus, the 57-minute stimulus and the unpatterned stimulus respectively. Figure 14A shows a slight "jump" in the phase difference between 12 Hz and 13 Hz. The response curve plotted in Figure 5B is the amplitude data for the stimulus of Figure 14A. Its peak was located at 7 Hz. Figures 14B and 14C show a nearly linear relationship between the phase difference and stimulus frequency and their response curves are displayed in Figures 6B and 7B respectively.

Figures 15A, 15B and 15C display the phase differences for subject RR. They represent the 15-minute, the 57-minute, and the unpatterned stimulus respectively. Figures 15A and 15B display a nearly linear relationship between the phase difference and stimulus frequency. Figure 15C displays a slight "jump" in the phase difference between 10 Hz and 11 Hz.

Figure 16 depicts the data for phase as a function of stimulus frequency from the Spekreijse, Estevez and Reits (1977) study using unstructured stimulus fields. These data were extrapolated from their graph and replotted using the same curve fitting technique used in Figures 13, 14 and 15 in this study. The resulting curve, appears nearly linear and not unlike several of the plots produced in this study.

In summary, Figures 13, 14 and 15 display the phase data for each subject. Interestingly, each subject showed a phase discontinuity or "jump" for different stimulus arrays.

DISCUSSION

<u>Problems</u>

Before attempting to discuss the specific results of this study, some remarks about a few of the problems encountered are in order. In this study, care was taken to vary the order of stimulus presentation. In addition, the numerical sequence of the temporal frequencies was varied (e.g., presented either in ascending or descending order). However, the stimulus response data are not equally balanced between the ascending and descending sequences. An inspection of the raw data revealed no influence of stimulus frequency order.

In this study, background noise was defined as the uncorrelated neural background activity present at each stimulus frequency (Tyler, Apkarian and Nakayama, 1978). When using the signal-to-noise ratio in the evaluation of the response amplitude, it may be helpful to record the response to a homogeneous stationary field during each recording session. However, in this study, each complete data collection series required 35 minutes and usually more than one stimulus series was completed during a single sitting. This amount of time precluded the measurement of the noise level at each sitting because the subjects tended to become restless. Therefore, the noise responses were measured only at varied intervals. This resulted in having more than one stimulus series compared to each background noise measurement.

A criteria signal-to-noise ratio of 2:1 was empirically determined as being efficacious from pilot data. Graphically, the influence of the background responses on the stimulus responses were easily determined.

A signal-to-noise ratio criteria of 2:1 worked well for subjects RM and LP. Most of the ratios from these two subjects were well above a 2:1 ratio. The small check evoked responses from subject RR, however, were always below the 2:1 ratio and occasionally the background noise was larger than the stimulus response. Subject RR's responses to the large check stimulus and unpatterned stimulus approached the magnitude of the responses from the other two subjects but occasionally the background noise was nearly as large as the stimulus response. Hence, the discussion will concentrate on the data from subjects RM and LP.

Data Assessment

Figures 10, 11 and 12 presented the data in the form of combined presentations from each stimulus for subjects RM, LP and RR respectively. The number of combined stimulus presentations for subject RM varied from five presentations of each of the pattern stimuli to six presentations of the unpatterned stimulus. The number of combined stimulus presentations for subject LP varied from four presentations of the 15-minute stimulus to five presentations of the 57-minute stimulus and the unpatterned stimulus. The number of combined stimulus presentations for subject RR varied from three combined presentations of the 15-minute stimulus to four presentations of the 57-minute stimulus and the unpatterned stimulus.

Figures 10A, 10B and 10C illustrate subject RM's responses to the 15-minute, the 57-minute and the unpatterned stimuli respectively. There are clear differences in the response curve for each stimulus. These differences are manifest in curve shape, the peak stimulus frequency response, the relative magnitude of the peak stimulus frequency response, and the signal-to-noise ratio.

The upper curve in Figure 10A is the response curve for the fundamental component of the VER from five combined presentations of the 15-minute stimulus. The lower data points represent the fundamental component of the VER from a single recording of the patterned background noise. The upper curve is unimodal with a peak located at the stimulus frequency of 10 Hz and a relative magnitude of more than 240 units. At the stimulus frequency of 10 Hz, the peak of the stimulus response curve is larger than the peak of the noise response by a ratio of almost 7:1; whereas, at other stimulus frequencies, the signal-to-noise ratio decreases. This increased signal-to-noise ratio draws attention to the fact that the peak of the stimulus response at this stimulus frequency is not contingent on the background noise. The lower noise data appear to have several peaks with the largest being at 4 and 5 Hz with a relative magnitude of 70 units. Also, at the stimulus frequency of 4 Hz (where the largest peak for the noise data is found), the stimulus response curve had its smallest response resulting in a signal-to-noise ratio of less than 2. Therefore, where the signal-to-noise ratio is largest, it can be assumed that the response peak is not influenced by the uncorrelated background noise at that stimulus frequency (Tyler, et al, 1978).

In Figure 10B, the upper curve represents the response for the fundamental component of the VER for five combined presentations of the 57-minute stimulus. The lower data points are the fundamental component of the VER from a single recording of patterned background noise and are the same data presented as background noise in Figure 10A. The upper curve appears unimodal with a peak at the 17 Hz stimulus frequency and a relative magnitude of about 175 units. The lower data points appear multipeaked, the largest being at 4 and 5 Hz with a relative

magnitude of 70 units. At the stimulus frequency of 17 Hz, the signal-to-noise ratio was at its maximum, in excess of 4:1. On either side of this stimulus frequency, the ratio appears to decrease. This indicates that the stimulus response peak is not influenced by the background noise. The signal-to-noise ratio appears to be the least in the 4 to 8 Hz stimulus frequency range which also indicates that the background noise does not affect the subject's responses to the stimulus at that stimulus frequency.

Subject RM's response curve to the unpatterned stimulus is shown as the upper curve in Figure 10C. This curve represents the fundamental component of the VER from six combined presentations of the unpatterned stimulus. The lower data points represent the fundamental component of the unpatterned background noise. The upper curve is unimodal with its peak located at a stimulus frequency of 15 Hz. The relative magnitude at the peaking so unitus frequency is approximately 450 units. The lower data points tend to be multipeaked with the greatest peak at 5 Hz and a relative magnitude of approximately 50 units. The maximum signal-to-noise ratio of 13:1 is found at the stimulus frequency of 15 Hz. This again demonstrates that the peak of the stimulus response curve is not dependent upon the background noise level. The maximum peak for the background noise for these data is located in the stimulus frequency range which produced the lowest amplitude first harmonic (fundamental) evoked potential.

Each of subject RM's VER response curve; for the 15-minute, 57-minute and unpatterned stimuli are unimodal. The peak of each curve occurs at a stimulus frequency where the signal-to-noise ratio is

maximum. This indicates that the maximum stimulus response is not the result of high amplitude ambient activity. While each stimulus curve is unimodal with the peak at the stimulus frequency of the maximum signalto-noise ratio, the peaks are located at different stimulus frequencies and they manifest different relative magnitudes. The 15-minute stimulus response curve has its peak located at 10 Hz for this subject while the 57-minute and unpatterned peaks are located at 17 Hz and 15 Hz stimulus frequencies respectively. Those peaks produced by the patterned stimuli follow the notion of spatiotemporal reciprocity with the lower spatial frequency stimulus producing a response in the higher temporal frequency region (Tyler, Apkarian and Nakayama, 1978). According to Regan (1977, 1978), large-check stimuli of 40 minutes or above produced responses which are a mixture of pattern responses and unpatterned responses with the peak stimulus frequency near the unpatterned peak stimulus frequency. This type of temporal tuning, described by Regan (1977, 1978), is clearly seen in the response curves produced by this subject.

In a comparison of the signal-to-noise ratios, the largest ratio of 13:1 is found with the unpatterned stimulus. The next largest ratio is slightly greater than 7:1 produced by the 15-minute stimulus. The smallest ratio of slightly more than 4:1 is found with the 57-minute stimulus.

Figures 11A, 11B and 11C are response curves based on the data produced by subject LP from the 15-minute, the 57-minute, and the unpatterned stimuli respectively. The response curve to each stimulus can be compared for curve shape, the stimulus frequency at which each curve peaks and the relative magnitude of each peak.

in Figure 11A, the upper curve is the response curve for the

fundamental component of the VER from four presentations with the 15minute stimulus. The lower data points represent the fundamental component of the VER from a single recording of the patterned background
noise. The upper stimulus response curve is bimodal with a primary
peak at 7 Hz and a secondary one at 21 Hz. The magnitude of the primary
peak is 240 units while the magnitude of the secondary peak is slightly
more than 160 units. The noise data have many peaks with a maximum at
a frequency of 8 Hz and a relative magnitude of 35 units. At a stimulus
frequency of 7 Hz, the signal-to-noise ratio is approximately 7:1. The
secondary peak frequency is 21 Hz and the signal-to-noise ratio is approximately 6:1.

The responses for the fundamental component of the VER from five combined presentations of the 57-minute stimulus are plotted as the upper curve in Figure 11B. In this same figure, the lower curve represents the fundamental component of the VER for a single recording of the background noise. The upper curve appears unimodal with a peak at the 7 Hz stimulus frequency and a relative magnitude of approximately 170 units. The lower data are multipeaked with the largest at 8 Hz with a relative magnitude of 35 units. A maximum signal-to-noise ratio of 5:1 is found at 7 Hz. The smallest signal-to-noise ratio is found in the higher temporal frequencies range where the background noise appears to be the greatest and the stimulus response appears to be the least.

The upper curve in Figure 11C represents the response curve for the fundamental component of the VER from five presentations of the unpatterned stimulus. The lower data points represent the responses for the fundamental component of the VER for a single recording of the unpatterned

background noise. The upper curve is unimodal with the stimulus response peak located at 17 Hz and a relative magnitude of approximately 500 units. The lower background noise data points are multipeaked with the largest response located at 9 Hz and a relative magnitude of 50 units. A maximum signal-to-noise ratio of approximately 11:1 is found at the 17 Hz stimulus frequency.

Subject LP's response curves representing the fundamental components of the VER from the 57-minute and the unpatt. and stimuli are unimodal while the response curve for the 15-minute stimulus was bimodal. The peaks of the 57-minute and unpatterned stimuli and the primary peak of the 15-minute stimulus occur at a place where the signal-to-noise ratio is a maximum. The peaks of the stimulus response to the two patterned stimuli are located at the same stimulus frequency, 7 Hz, while the peak of the unpatterned stimulus is located at 17 Hz. The peaking of the stimulus response curves for the patterned stimuli do not support spatiotemporal reciprocity since they peak at the same stimulus frequency. Additionally, the 57-minute stimulus response does not appear to be mixture of the small (15-minute) patterned response and the unpatterned response because the peak is located at the same stimulus frequency as the 15-minute response and does not appear to be a combination of these two. In a comparison of the signal-to-noise ratios for subject LP, the largest ratio of 11:1 is found with the unpatterned stimulus. The next largest ratio, approximately 7:1, is found with the 15-minute stimulus. The smallest ratio of 5:1 is found with the 57-minute stimulus. Even though the peak temporal frequencies from the 15-minute and 57minute stimuli and the peak frequency from the patterned background noise

nearly coincide, the signal-to-noise ratios are large, indicating that the peaks represent the neural activity evoked by the stimulus and not from the uncorrelated background activity at the stimulus frequency (Tyler, et al, 1978).

The upper response curves in Figures 12A, 12B and 12C are the response curves for the fundamental components of the VER from the 15-minute, the 57-minute, and the unpatterned stimuli respectively for subject RR. The lower curves are the data for the fundamental corresponding background noise for subject RR. The upper curve in Figure 12A is produced by combining three presentations of the 15-minute stimulus. This curve appears to be nearly linear except at the initial stimulus frequency of 4 Hz. The relative magnitude of the response at 4 Hz is approximately 70 units. The lower data points are produced by the patterned background noise. The largest background amplitude occurs at the 20 Hz frequency with a relative magnitude of 45 units which is larger than the relative magnitude of the response curve at that frequency. At 4 Hz, the relative magnitude of the background noise is approximately 40 units. The signal-to-noise ratio at all stimulus frequencies is less than 2:1.

Figure 12B displays a curve produced by four combined presentations of the 57-minute stimulus. The lower data points are produced by a single recording session of the patterned background noise. The upper curve appears unimodal with a peak stimulus response at 9 Hz and a relative magnitude of approximately 90 units. The lower (noise) data points have several peaks of approximately the same magnitude which appear at 15, 20 and 23 Hz with relative magnitudes of approximately 50 units. The

maximum signal-to-noise ratio of slightly more than 3:1 occurs at 9 Hz. On either side of this range of frequencies, the signal-to-noise ratio decreases.

Subject RR's response curve to the unpatterned stimulus is shown as the upper curve in Figure 12C. It is produced by combining four presentations of the stimulus. The lower data points are produced by a single recording session of the unpatterned background noise. The upper curve appears unimodal but there appears to be a slight peak at the 4 Hz stimulus frequency. This peak may be due to an increase in the background noise at 4 Hz. The upper stimulus response curve shows the largest amplitude at 17 Hz with a relative magnitude of approximately 150 units. The lower data points appear to have several peaks with the largest peak at 4 Hz and a relative magnitude of 75 units. At 17 Hz, the relative magnitude of the lower data point is approximately 25 units, resulting in a signalto-noise ratio of 6:1. The signal-to-noise ratio appears to decrease on either side of the 17 Hz stimulus frequency, particularly from 4 Hz to 11 Hz. The small peak of the response curve located at 4 Hz may be attributed to a combination of the response to the stimulus combined with the background noise.

Subject RR's response curve to the 15-minute stimulus is nearly linear except at the initial 4 Hz stimulus frequency. There appears to be a slight increase in the relative magnitude of the response curve between 13 Hz and 15 Hz but there is also an increase in the relative magnitude of the background noise between those frequencies. The response curve to the 57-minute stimulus appears to be unrelated to the background noise for the stimulus frequencies in which the response peak is found. The

response curve to the unpatterned stimulus also appears to be unrelated to the background noise for the stimulus frequencies in which the response peak is found. However, in the lower stimulus frequency range, the stimulus response curve appears to be influenced by the background noise.

In a comparison of the data provided by subject RR for each stimulus, the data from the 15-minute stimulus appears to be confounded by background noise. The responses to the 57-minute and unpatterned stimuli peak at 9 Hz and 17 Hz respectively. The relative magnitude of the responses to these two stimuli are similar at approximately 90 units for the 57-minute stimulus and 150 units for the unpatterned stimulus. The largest signal-to-noise ratio of 6:1 is produced by the unpatterned stimulus. A signal-to-noise ratio of slightly more than 3:1 is produced by the 57-minute stimulus. When comparing RR's data for the 57-minute and unpatterned stimuli to Regan's data (1977, 1978), RR's data show the same type of peaking relationship. The 57-minute stimulus produces a peak in the higher temporal frequencies. However, Regan's data (1977, 1978) show a greater magnitude of response for the unpatterned stimulus than for the patterned stimulus. Subject RR's data does not show this difference in response magnitude.

The difference between the VER to contrast modulated stimuli and luminance modulated stimuli has been attributed to two types of detection channels in the visual system. The channel which responds to spatial stimuli has been referred to as either the X-type (Enroth-Cugell and Robson, 1966) or sustained type (Cleland, et al, 1971). The sustained type responds better to slow moving, sharply focused, high spatial frequency targets. The channel which responds to luminance changes is

called either the Y-type (Enroth-Cugell and Robson, 1966) or transient type (Cleland, et al, 1971). The transient type responds better to large, fast moving, low spatial frequency targets. This tendency for high spatial frequency responses to occur at low temporal frequencies while the low spatial frequency responses occur at high temporal frequencies had been referred to as spatiotemporal reciprocity by Tyler, et al (1978).

Regan (1977, 1978) has presented a simular notion referred to as temporal tuning where high spatial frequency and low spatial frequency stimuli such as small check and large check stimuli demonstrated a selectivity to different temporal frequencies for an optimal response. Typically, the largest responses to small checks are found at 5 to 9 Hz whereas large check stimuli (greater than 40 minutes) produce the largest responses between 15 and 21 Hz (Regan, 1981). However, Regan (1978) also demonstrated that the response curve elicited by the large check stimuli can be bimodal with a slightly smaller peak in the same range as the small check stimuli. Unpatterned stimuli were found to produce peaks in the same range as the large check stimulus (Regan and Richards, 1973, and Regan, 1978). Regan (1977, 1978) also made the point that the magnitude of the response to unpatterned stimuli is larger than the magnitude of the response to the patterned stimuli. However, small check stimuli produce a larger response than large check stimuli. Large check stimuli give responses which, according to Regan (1977, 1978), are a mixture of patterned responses and unpatterned responses.

Table 1 presents a comparison of responses to each stimulus from each subject. Comparisons are made in four categories: the shape of the stimulus response curve (CS), the temporal stimulus frequency at which the

peak or the largest response to the stimulus is found (SF), the relative magnitude of the peak (Rel Mag), and the signal-to-noise ratio at the peak stimulus response (S/N).

The greatest difference in the shape of the response curves is produced with the 15-minute stimulus. The response curve is unimodal from subject RM, bimodal from subject LP and nearly linear from subject RR. The response curves to the 57-minute and unpatterned stimuli are unimodal for all subjects.

As seen in Table 1, the notion of spatiotemporal reciprocity (Tyler, Apkarian and Nakayama, 1928) is found in the stimulus frequency responses to the 15-minute and 57-minute stimuli for subject RM. The 15-minute stimulus produced a peak at a temporal frequency of 10 Hz while the 57-minute stimulus produced the peak at the higher temporal frequency of 17 Hz. The peak response of LP to both the 15-minute and 57-minute stimuli are produced at 7 Hz. Regan (1977, 1978) found that the small (15-minute) check stimuli typically produced a peak at a lower temporal frequency (7 Hz) than the large (40 or more minute) check stimuli. However, Regan (1978) does make the observation that his large check produced two peaks, one of which was located at the same temporal frequency (7 Hz) at which the small check stimulus peaked.

Subject RR's responses may adhere to the notion of spatiotemporal reciprocity but the low signal-to-noise ratio to the 15-minute stimulus prohibits any firm conclusion. The peak from the 57-minute stimulus, however, was found to be within the expected range of 5-9 Hz.

Each subject's response to the unpatterned stimulus peaked within the 15-21 Hz range as found by Regan (1978). The peak response from RM

was at 15 Hz, LP's was at 18 Hz, and RR's response peaked at 17 Hz.

The magnitudes of RM's and LP's peak response to the patterned stimuli were larger for the 15-minute stimulus than for the 57-minute stimulus and their peak response to the unpatterned stimuli was larger than that for the 15-minute stimulus. Regan (1977, 1978) also showed that the response magnitude was larger for the unpatterned stimulus than for either of the check patterned stimuli. For Regan (1977, 1978), the smaller checks (15 minute) produced larger response magnitudes than the larger checks (40 minutes or larger). Subject RR's responses did not follow this pattern. The smallest response was found for the 15-minute stimulus while the responses from the 57-minute and unpatterned stimuli had similar magnitudes.

The final category found in Table 1 is the signal-to-noise ratio. The signal-to-noise ratios in this table were the largest ratios found for each response curve from each stimulus for each subject. All of the signal-to-noise ratios were above 2:1 except for the responses from subject RR for the 15-minute stimulus. The largest values for each subject were found with the unpatterned stimulus. The next largest for subjects RM and LP were found with the 15-minute stimulus. The smallest ratios for subjects RM and LP were produced by the 57-minute stimulus. While RR produced his largest signal-to-noise ratio to the unpatterned stimulus, the 15-minute stimulus produced the smallest ratio and the 57-minute stimulus produced the second largest ratio. From these data, it appears that the responses to the unpatterned stimulus were the least affected by the background noise.

As part of the data analysis in this study, the phase difference

between the stimulus and the fundamental VER component as a function of stimulus frequency was considered. Spekreijse (1966) and Spekreijse, Estevez and Reits (1977) found that there was a more rapid increase in the phase lag for those stimulus frequencies below 20 Hz than for those above 20 Hz, resulting in a nearly linear response. However, in the study by van der Tweel and Verduyn Lunel (1965), using sinusoidally—modulated light, only two of their three subjects obtained linear responses. Their third subject's responses were markedly different in that there was a loss of linearality occurring in the temporal frequency range which produced the peak amplitude by the stimulus. Van der Tweel and Verduyn Lunel (1965) attributed this change to "inter-individual" differences, similar to the inter-subject differences found in this study.

The data of this study are plotted with the phase in radians shown on the Y-axis (ordinate) and the stimulus frequency on the X-axis (obscissa) as shown in Figures 13A, 13B, 13C, 14A, 14B, 14C, 15A, 15B and 15C.

Each figure contains the actual data points as well as a curve fit with three degrees of freedom. The figures with the number 13 are data from subject RM, while the figures with the number 14 are data from subject LP, and those figures with the number 15 are from subject RR. The letter A refers to the 15-minute stimulus, B to the 57-minute stimulus, and C to the unpatterned stimulus. Figure 16 was extrapolated from the data presented by Spekreijse, Estevez and Reits (1977). These data appear linear for the eight data points. The only data in this study that appear similar to Spekreijse, et al (1977), are seen in Figures 13C and 14C. These data points were produced by the unpatterned stimulus for

subjects RM and LP respectively. The remaining figures, except for Figure 14A, are nearly linear. Possibly these relationships would have been more linear if only eight data points were used or possibly Spekreijse, et al's (1977) data would have produced a less linear relationship if more data points were taken. Figure 14A was produced by the data points from the 15-minute stimulus for subject LP. These data display the most abrupt change in the series, similar to van der Tweel and Verduyn's (1965) study. These are the same data used in Figure 11A which displayed the only bimodal curve in this series.

Purpose Revisted

The data presented in this study are intended to show the relationship between temporal and spatial frequency in the VER. Table 1 displays an overview of the data used in comparing the responses from each of the three stimuli for each of the three subjects. It was determined that the unpatterned stimulus produced a unimodal response curve which has a peak in the higher temporal frequencies (15-18 Hz) and results in the largest signal-to-noise ratios. It was also determined that the 15-minute stimulus produced a response curve which has a peak in the lowest temporal frequencies (4-10 Hz) and the largest peak for two (RR and LP) out of the three subjects. It was found that the 57-minute check produced a peak in the middle (7-17 Hz) temporal frequency range in all three subjects. The data from subject RM demonstrates spatiotemporal reciprocity (Tyler, Apkarian and Nakayama, 1978) while the data from subject LP is more similar to the data of Regan (1977, 1978), where the small check and large check stimuli elicited responses at the same temporal frequency.

The data from this study reinforces the fact that no one particular notion fully explains the complexities of the VER. Some of the data presented here support different notions or even parts of different notions. One of the difficulties presented by the literature is the fact that many of our ideas about evoked potentials are derived from a relatively small population of observers. Van der Tweel and Verduyn Lunel (1965) present data from three observers, Regan and Richards (1973) from two observers, Spekreijse, Estevez and Reits (1977) from one observer, Regan (1977, 1978) from one observer, and, finally, Tyler, Apkarian and Nakayama (1978) present data from four observers (one of whom provided most of the data).

Further investigations involving larger numbers of subjects need to be initiated. A large variety of subjects may more fairly define the range of VER data. Even the small sample of this study repeatedly bears testament to its idiosyncratic nature and, in this author's opinion, for now the words of Regan (1977) should be taken to heart: "If there is a simpler way of doing your experiment, it is foolishness to use evoked potential recording."

TABLE 1

RR	S/N Ratio	Below 2:1	3:1	6:1
	Rel Mag	70	96	150
	SF	4Hz	2H2	17Hz
	8	Nearly linear	Unimodal	Unimodal
LP	S/N Ratio	7:1	5:1	11:1
	Rel Mag	240	170	500
	SF	7Hz,	7HZ	17Hz
	S .	Bimodal	Unimodal	Unimodal
RM	S/N Ratio	7:1	4:1	13:1
	Rel Mag	240	175	450
	Ӄ	10Hz	тинг	15Hz
	প্ত	Unimodal 10Hz	Unimoda1	Uninodal 15Hz
	- Programme Annual Prog	15-minute check	57-minute check	Unpatterned

= Stimulus frequency which is the stimulus frequency which had the largest response = Relative magnitude which is the number of units measured at the largest response S/N Ratio = The signal-to-noise ratio at the stimulus frequency with the largest response = The curve shape which is the type curvature of the stimulus response curve Rel Mag શ ₹<u>₹</u>

REFERENCES

- Adrian, E.D., and Matthews, B.H.C. (1934) The Berger rhythm; potential changes from the occipital lobes of man. <u>Brain</u> 57: 355-385.
- Arden, G.B., Bodis-Wollner, I., Halliday, A.M., Jeffreys, A., Kulikowski, J.J., Spekreijse, H., and Regan, D. (1977) Methodology of patterned visual stimulation, in Desmedt, J.E. (Ed.): <u>Visual Evoked Potentials</u> in <u>Man</u>: <u>New Developments</u>. Oxford, Clarendon Press, pp. 3-15.
- Behrman, J., Nissim, S., and Arden, G.B. (1972) A clinical method for obtaining pattern visual evoked responses, in Arden, G.B. (Ed.):

 The Visual System: Neurophysiology, Biophysics, and Their Clinical Applications, Vol. 24, Advances in Experimental Medicine and Biology.

 New York, Plenum Press, pp. 199-206.
- Berger, H. (1929) Ueker das Elektrenkephalogramm des Mehschen. I. <u>Arch.</u>
 Psychiat. <u>Nevenkr</u>. 87: 527-270.
- Berger, H. (1932) Uber das Elecktroenzephalogramm des Menssher. Arch.

 Psychiat. Nevenkr. 97: 6-26.
- Brazier, M.A.B. (1977) <u>Electrical Activity of the Nervous System.</u>
 Baltimore. The Williams and Wilkins Co., 4th Ed.
- Brietmeyer, B.G. (1975) Simple reaction time as a measure of the temporal response properties of transient and sustained channels. <u>Vision</u>

 <u>Res.</u> 15: 1151-1155.

- Brietmeyer, G.B., and Julesz, B. (1975) The role of on and off transients in determining the psychophysical spatial frequency response. <u>Vision</u>

 <u>Res.</u> 15: 411-415.
- Caton, R. (1875) The electric currents of the brain. <u>Rrit. Med. J.</u>
 2-278.
- Cleland, B.G., Dukin, M.W., and Levick, W.R. (1971) Sustained and transient neurons in the cat's retina and lateral geniculate nucleus. <u>J</u>.

 <u>Physiol</u>. 217: 473-496.
- Du Bois-Reymond, E. (1848) <u>Untersuchungen uber thieresche Electricitat</u>.

 Reimer, Berlin.
- Ellenberg, C., Shuttlesworth, D.E., and Palmer, E.A. (1977) Clinical pathophysiology of the cerebral visual system, in Burde, R.M., Karp, J.S. (Eds.): Clinical Neuroophthalmology: The Afferent Visual System. Vol. 17, No. 1, International Ophthal. Clinics. Boston, Little, Brown and Co., pp. 65-83.
- Enroth-Cugell, C., and Robson, J.G. (1966) The contrast sensitivity of retinal ganglion cells of the cat. J. Physiol. 187: 517-522.
- Halliday, A.M., McDonald, W.I., and Mushin, J. (1972) Delayed visual evoked response in optic neuritis. <u>Lancet 1: 982-985</u>.
 - 1.1g, G.F.A. (1974) The visual evoked response. Adv. Ophthalmol. 28: 2-28.
- Hartner, M.R., and White, C.T. (1968) Effects of contour sharpness and

- check size on visually evoked cortical potentials. <u>Vision Res</u>. 8: 701-711.
- Hoffman, K.P., Stone, J., and Sherman, S.M. (1972) Relay of receptive field properties in dorsal lateral geniculare nucleus of the cat.

 J. Neurophysiol. 35: 518-531.
- Ikeda, I., and Wright, M.J. (1972) Differential effects of refractive errors and receptive field organization of central and peripheral ganglion cells. <u>Vision Res.</u> 12: 1465-1476.
- Ikeda, I., and Wright, M.J. (1974) Evidence for "sustained" and "transient" neurons in the cat's visual cortex. <u>Vision Res</u>. 14: 133-136.
- Kamp, A., Sem-Jacobson, C.W., Storm van Leeuwen, W., and van der Tweel, L.H. (1960) Cortical responses to modulated light in the human.

 <u>Acta Physiol. Scand.</u> 48: 1-12.

AND REPORTED TO DO DO DE LES ESTADOS CONTRACTOR DE LA CON

- Keesey, U.T. (1972) Flicker and pattern detection: A comparison of thresholds. <u>J. Opt. Soc. Am.</u> 62: 446-448.
- Kulikowski, J.J., and Tolhurst, D.J. (1973) Psychophysical evidence for sustained and transient detectors of human vision. <u>J. Physiol</u>. 232: 149-162.
- Levi, D.M., and Walters, J.W. (1977) Visual evoked responses in strabismic and anisometropic amblyopia: Effects of check size and retinal locus. Amer. J. Optom. and Physiol. Optics 577: 691-698.
- Levi, D.M., and Harwerth, R.S. (1968) A sensory mechanism for amblyopia:

 Electrophysical studies. Amer. J. Optom. and Physiol. Optics 55: 163-171.

- MacKay, D.M., and Jeffreys, D.A. (1973) Visually evoked potentials and visual perception in man, in Jung, R. (Ed.): <u>Handbook of Sensory</u>

 <u>Physiology</u>, <u>Vol. 7/3B Central Visual Information</u>. Berlin,

 Springer-Verlag, pp. 647-678.
- Millodot, M., and Riggs, R.A. (1970) Refraction determined electrophysiologically. <u>Arch Ophthalmol</u>. 84: 272-278.
- Milner, B.A., Regan, D., and Heron, J.R. (1972) Theorectical models of the generation of study-state evoked potentials, their relation to neuroanatomy and their relevance to certain clinical problems, in Arden, G.B. (Ed.): The Visual System: Neurophysiology, Biophysics, and Their Clinical Applications, Vol. 24, Advances in Experimental Medicine and Biology. New York, Plenum Press, pp. 157-169.
- Ochs, S. (1965) <u>Elements of Neurophysiology</u>. New York, John Wiley and Sons, Inc.
- Padmos, P., Haaijman, J.J., and Spekreijse, H. (1973) Visual evoked cortical potential to patterned stimuli in monkey and man.

 <u>Electroenceph</u>. <u>Clin</u>. <u>Neurophysiol</u>. 35: 153-163.
- Perry, N.W., and Childers, D.E. (1969) <u>The Human Visual Evoked Response</u>. Springfield, Charles C. Thomas.
- Prawdicz-Neminski, W.N. (1925) Zur Kenntnis der elekrischen und der Inntervotionsvorange in den funktionnellen Elementen und Gweken des tierischen Organismus, Elektrocerebrogramm der Saugetiere.

 Pflug. Arch. Ge 3 Physiol. 209: 362-382.

- Regan, D. (1966) Same characteristics of average steady-state and transient responses evoked by modulated light. <u>Electroenceph</u>.

 <u>Clin. Neurophysiol</u>. 20: 238-249.
- Regan, D. (1968) Chromatic adaptation and steady-state evoked potentials.

 <u>Vision Res.</u> 8: 149-158.
- Regan, D. (1970) Evoked potential and psychophysical correlates of changes in stimulus color and intensity. <u>Vision Res</u>. 10: 163-178.
- Regan, D. (1972a) <u>Evoked Potentials in Psychology</u>, <u>Sensory Physiology</u>, and <u>Clinical Medicine</u>. London, Chapman and Hall.
- Regan, D. (1972b) Cortical evoked potentials, in Nicholson, J.P. (Ed.):

 <u>Interdisciplinary Investigation of the Brain</u>. New York, Plenum

 Press, pp. 177-192.
- Regan, D. (1977) Steady-state evoked potentials. <u>J. Opt. Soc. Am.</u> 67: 1475-1489.
- Regan, D. (1978) Assessment of visual acuity by evoked potential recording: ambiguity caused by temporal dependence of spatial frequency selectivity. <u>Vision Res</u>. 18: 439-443.
- Regan, D. (1979) Electrical responses evoked from the human brain.

 <u>Sci. Amer.</u> 741: 134-146.
- Regan, D. (1981) Speedy evoked potential methods for assessing vision in normal and amblyopic eyes: Pros and cons. <u>Vision Res</u>. 20: 265-269.

- Regan, D., and Heron, J.R. (1969) Clinical investigation of lesions of the visual pathway: a new objective technique. <u>J. Neurol.</u>

 Neurosurg. Psychiat. 32: 479-483.
- Regan, D., and Richards, W. (1971) Independence of evoked potentials and apparent size. <u>Vision Res</u>. 11: 679-684.
- Regan, D., and Richard, W. (1973) Brightness and contrast and evoked potentials. <u>J. Opt. Soc. Am.</u> 63: 606-611.
- Ruddock, K.H. (1968) Control of the time pattern of the stimulus, in Crawford, B.H., Granger, G.W., and Weale, R.A. (Eds.): <u>Techniques</u>

 of <u>Photostimulation in Biology</u>. New York, John Wiley and Sons, Inc., pp. 109-143.
- Sokol, S. (1976) Visually evoked potentials: theory, techniques, and clinical applications. <u>Surv. Ophthalmol</u>. 21: 18-44.
- Spekreijse, H. (1966) Analysis of EEG Responses in Man Evoked by Sine

 Wave Modulated Light. The Hague, Junk.

- Spekreijse, H., Estevez, O., and Reits, D. (1977) Visual evoked potentials and the physiological analysis of visual process in man, in Desmedt, J.E. (Ed.): <u>Visual Evoked Potentials in Man</u>: <u>New Developments</u>. Oxford, Clarendon Press, pp. 3-15.
- Spekreijse, H., van der Tweel, L.H., and Zuideman, T. (1973) Contrast evoked responses in man. <u>Vision Res</u>. 13: 1577-1601.

- Tolhurst, D.J. (1973) Separate channels for the analysis of the shape and the movement of a moving visual stimulus. <u>J. Physiol</u>. 231: 385-402.
- Tolhurst, D.J. (1975) Sustained and transient channels in human vision.

 <u>Vision Res.</u> 15: 1151-1155.
- Tyler, C.W., Apkarian, P., and Nakayama, K. (1978) Multiple spatial-frequency tuning of electrical responses from the human visual cortex. Exp. Brain Res. 33: 535-550.
- Tyler, C.W., Apkarian, P., Levi, D.M., and Nakayama, K. (1979) apid assessment of visual function: an electronic sweep technique for the pattern visual evoked potential. <u>Invest</u>. <u>Ophthalmol</u>. <u>Visual Sci</u>. 18: 703-713.
- Van der Tweel, L.H., and Spekreijse, H. (1968) Visual evoked responses.

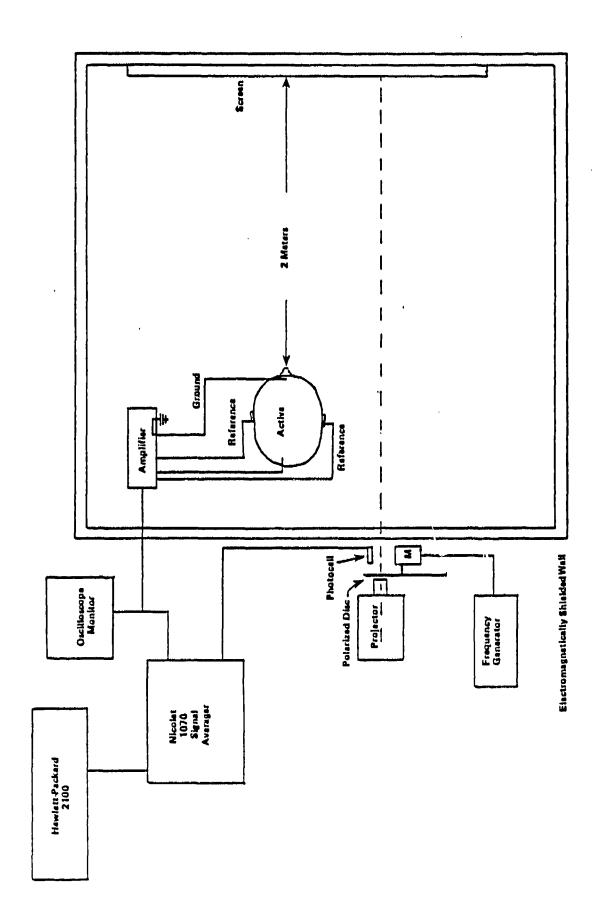
 The Clinical Value of Electroretinography. ISCERG Symp. Ghent,

 1966, pp. 83-94.
- Van der Tweel, L.H., and Verduyn Lunel, H.F.E. (1965) Human responses to sinusoidally modulated light. <u>Electrocept</u>. <u>Clin</u>. <u>Neurophysiol</u>. 18: 587-598.

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Walters, J.W., Yolton, R.L., and Gohl, P.L. (1976) Construction of simple vectographic slides for VER stimuli. <u>J. Optom. and Physiol.</u>

Optics 53: 191-193.



Organization of the recording apparatus used in this study. Figure 1.

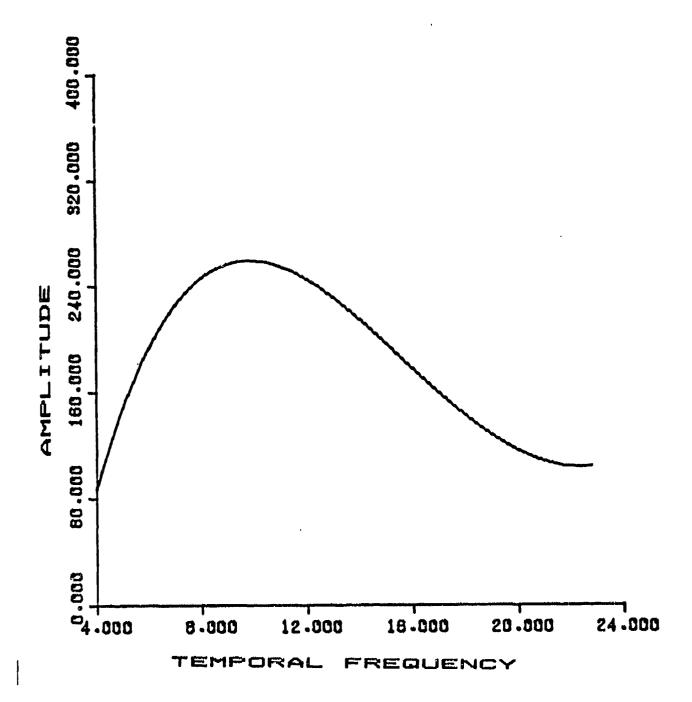


Figure 2A. The response curve for the fundamental component of the VER for five combined presentations to subject RM (RMYØ, RMØC, RMØM, RMØU, and RMDA) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .3747x^3 - 12.6295x^2 + 152.4572x - 343.544$$

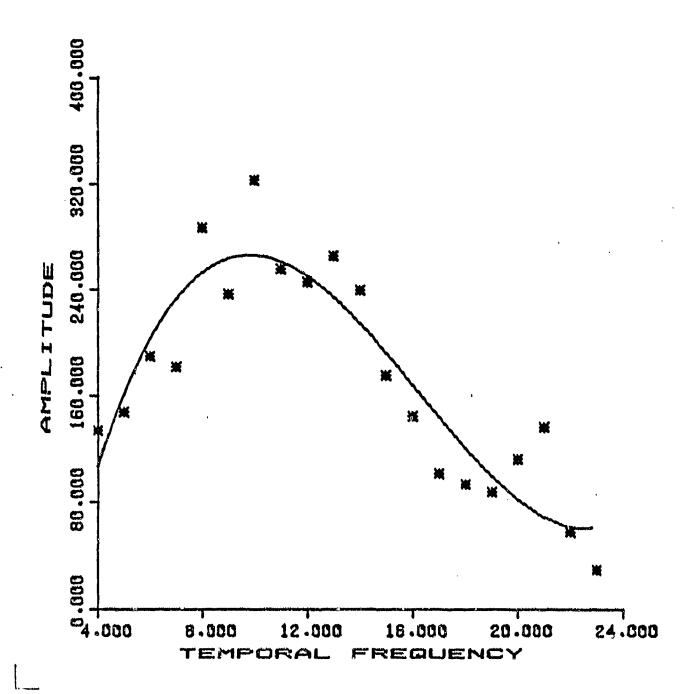


Figure 2B. The response curve for the fundamental component of the VER for a single presentation to subject RM (RMDA) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .1447x^3 - 12.6295x^2 + 121.0685x - 250.792$$

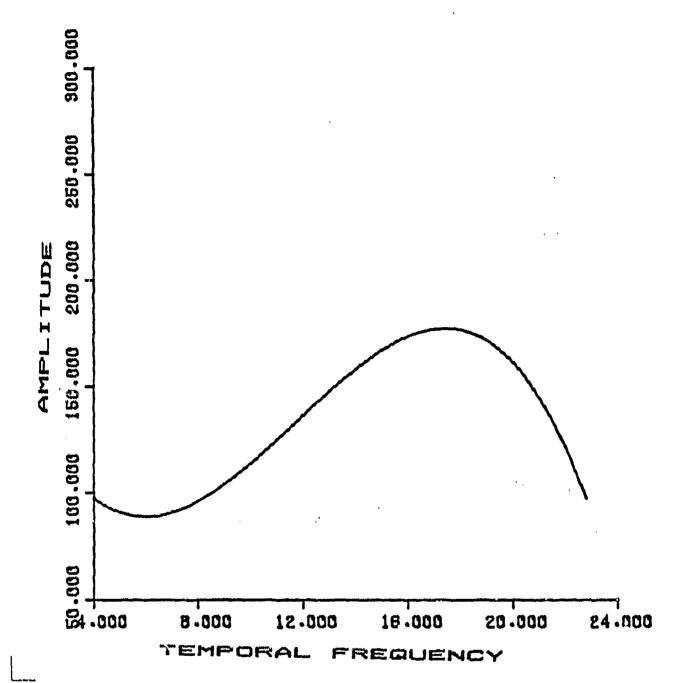


Figure 3A. The response curve for the fundamental component of the VER for five combined presentations to subject RM (RMØA, RMØE, RMØO, RMØW, and RMEA) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.1053x^3 + 3.9425x^2 - 35.5912x + 183.6381$$

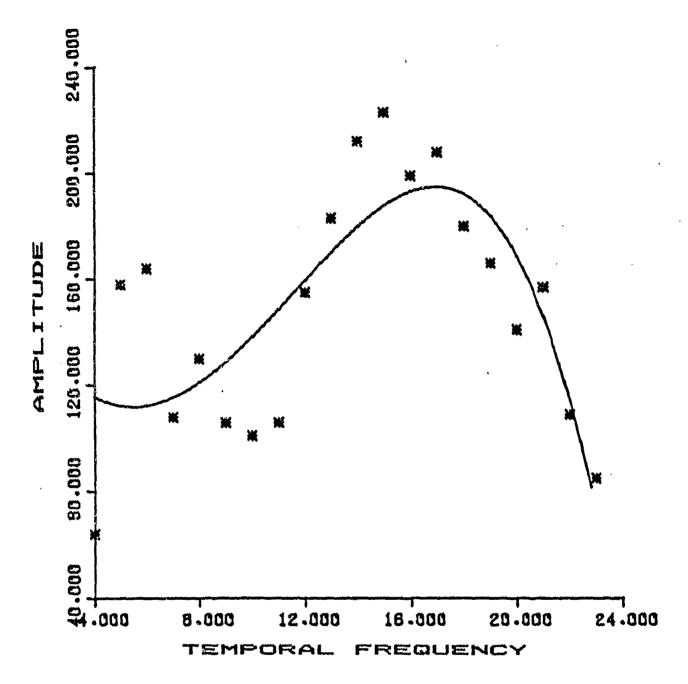


Figure 3B. The response curve for the fundamental component of the VER from a single presentation to subject RM (RMØA) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.0007x^3 + 2.0202x^2 - 20.4195x + 165.4450$$

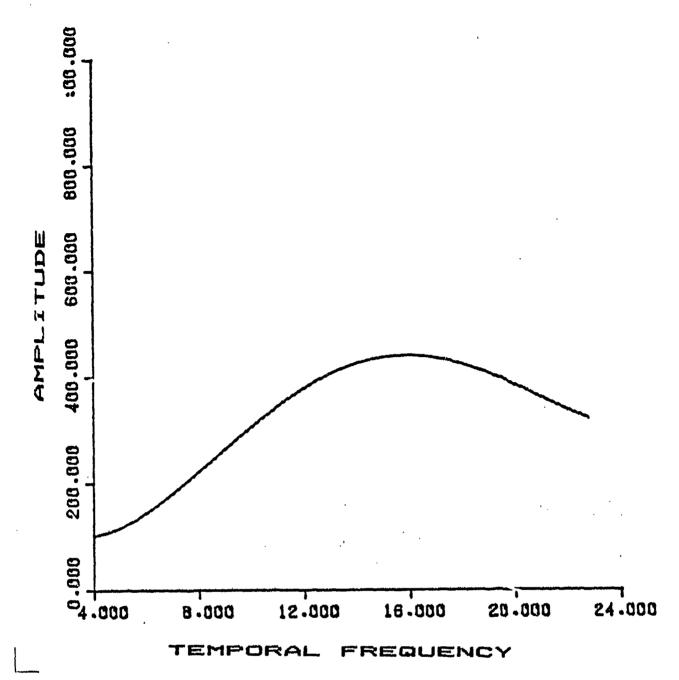


Figure 4A. The response curve for the fundamental component of the VER from a combination of six presentations to subject RM (RMWW, RMWG, RMWG, RMWG, RMWG, RMWG, RMWG, and RMFA) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -1.0933x^3 + 20.0573x^2 - 106.407x + 273.1473$$

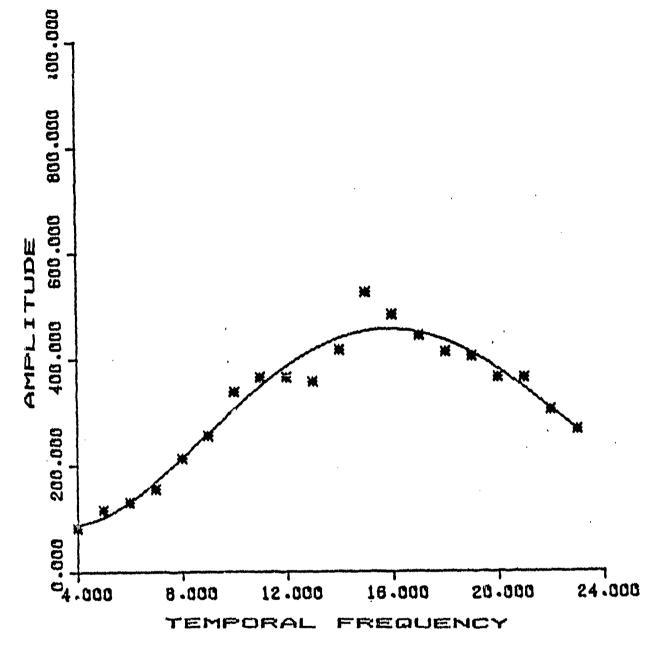
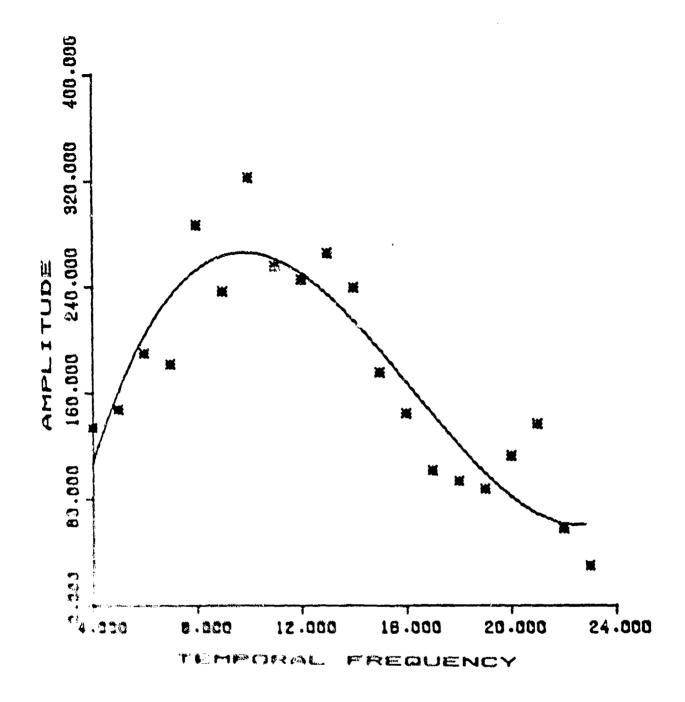


Figure 4B. The response curve for the fundamental component of the VER for a single presentation to subject RM (RMWI) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -1.1305x^3 + 21.3911x^2 - 116.556x + 280.5491$$



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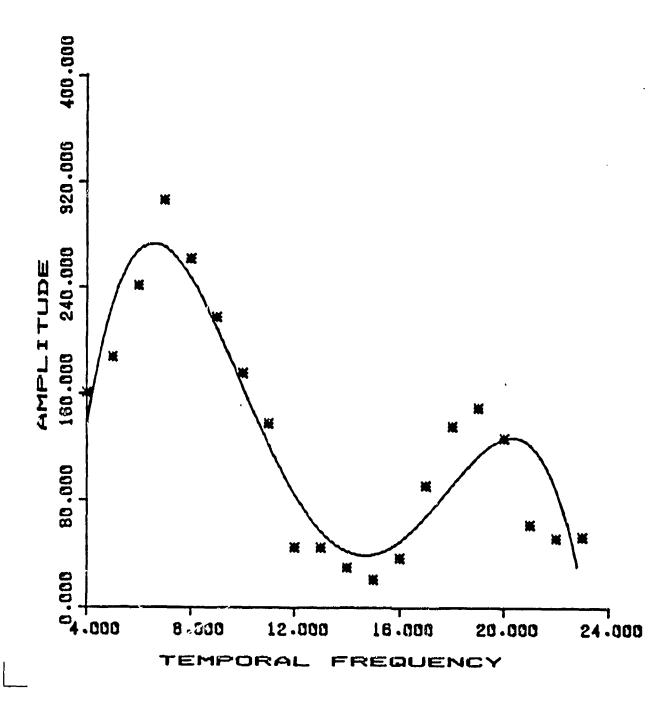


Figure 5B. The response curve for the fundamental component of the VER for a single presentation to subject LP (LPZØ) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$\gamma = .37804x^3 - 72.0054x^2 + 533.489x - 1071.51$$

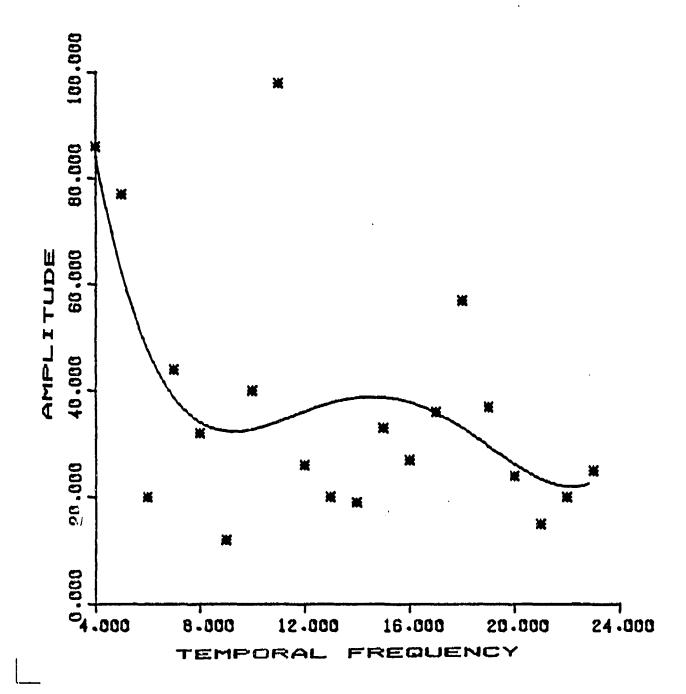


Figure 5C. The response curve for the fundamental component of the VER for a single presentation to subject RR (RRØM) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.3931x^3 + 3.4972x^2 - 75.5056x + 277.999$$

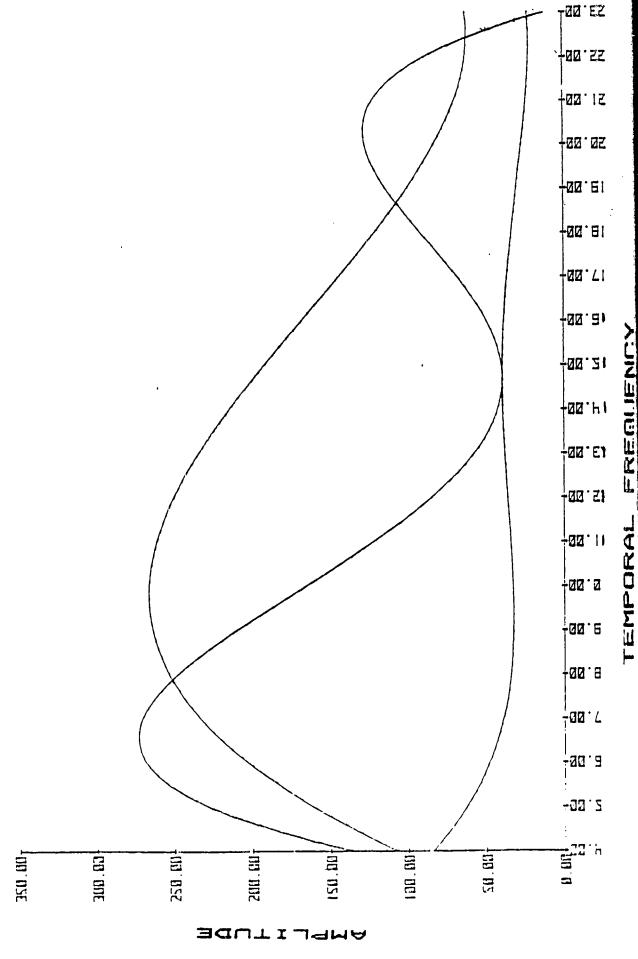


Figure 5D. Combination of Figures 5A, 5B, and 5C.

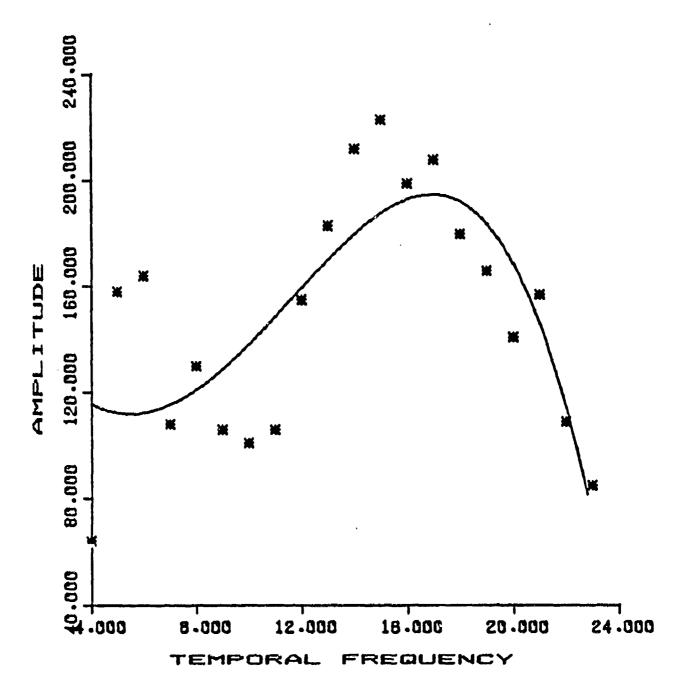


Figure 6A. The response curve for the fundamental component of the VER for a single presentation to subject RM (RMWA) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.0007x^3 + 2.0202x^2 - 20.4195x + 165.4450$$

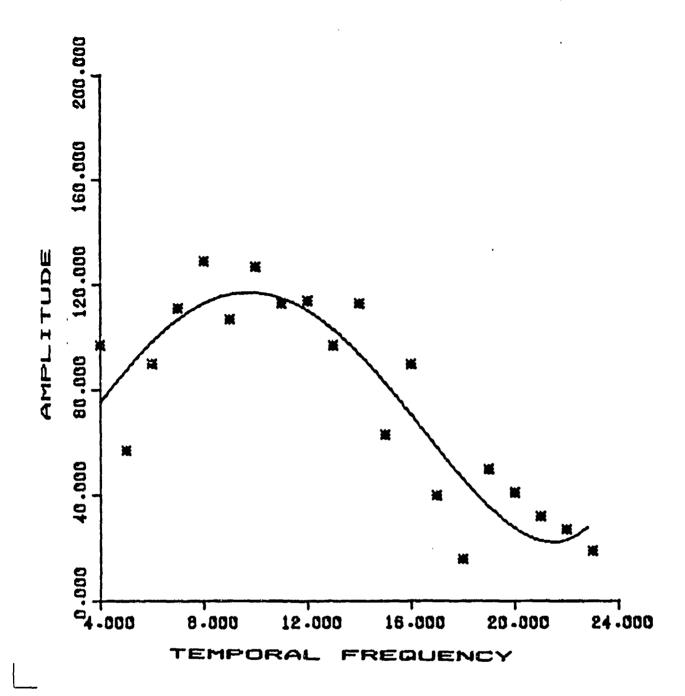


Figure 6C. The response curve for the fundamental component of the VER for a single presentation to subject RR (RRSØ) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.1842x^3 + 1.2281x^2 + 10.6877 + 22.3075$$

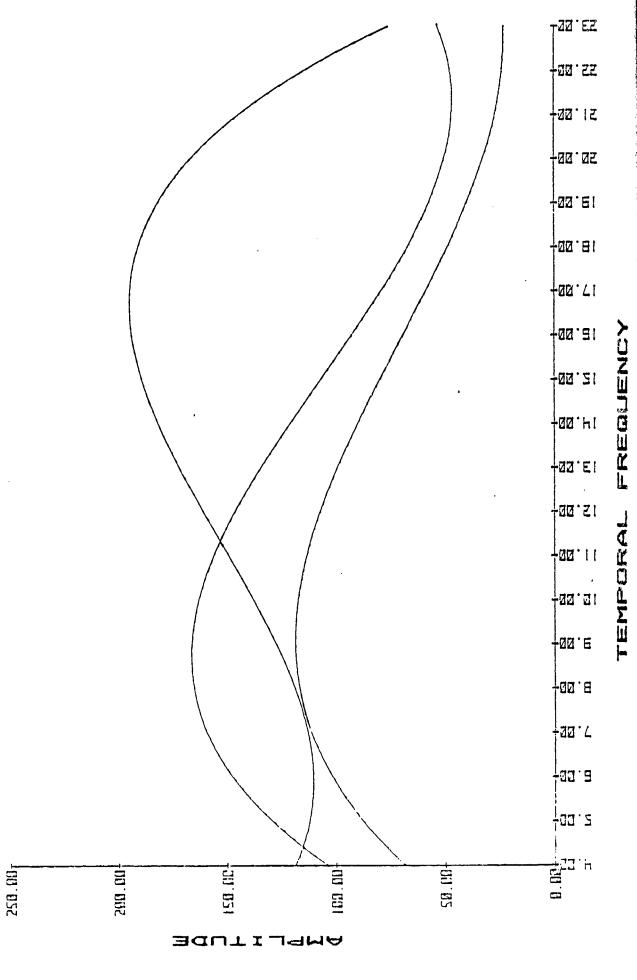


Figure 6D. Combination of Figures 6A, 6B, and 6C.

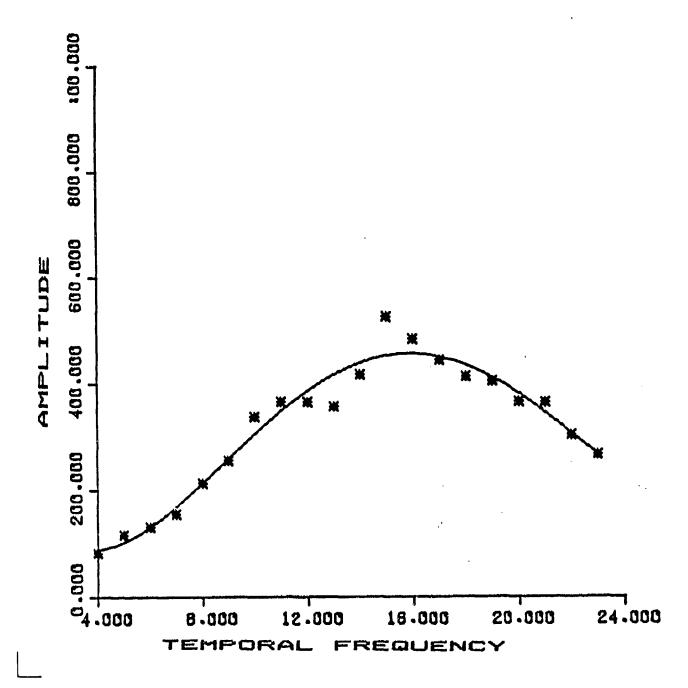


Figure 7A. The response curve for the fundamental component of the VER for a single presentation to subject RM (RMØI) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -1.1305x^3 - 21.3911x^2 - 116.5560x + 280.5491$$

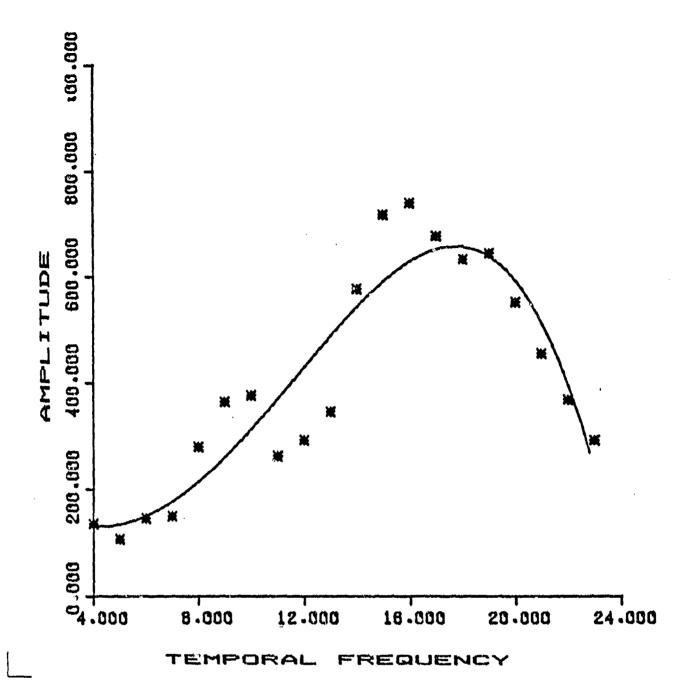


Figure 7B. The response curve for the fundamental component of the VER for a single presentation to subject LP (LPTØ) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .0071x^3 + 6.8095x^2 - 59.5138x + 258.6053$$

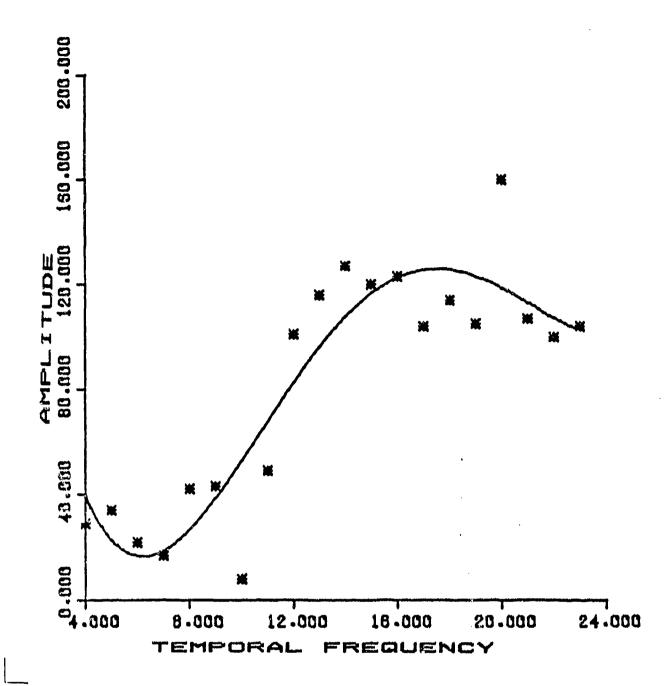


Figure 7C. The response curve for the fundamental component of the VER for a single presentation to subject RR (RRWW) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .5895x^3 + 12.5922x^2 - 97.0847x + 261.4221$$

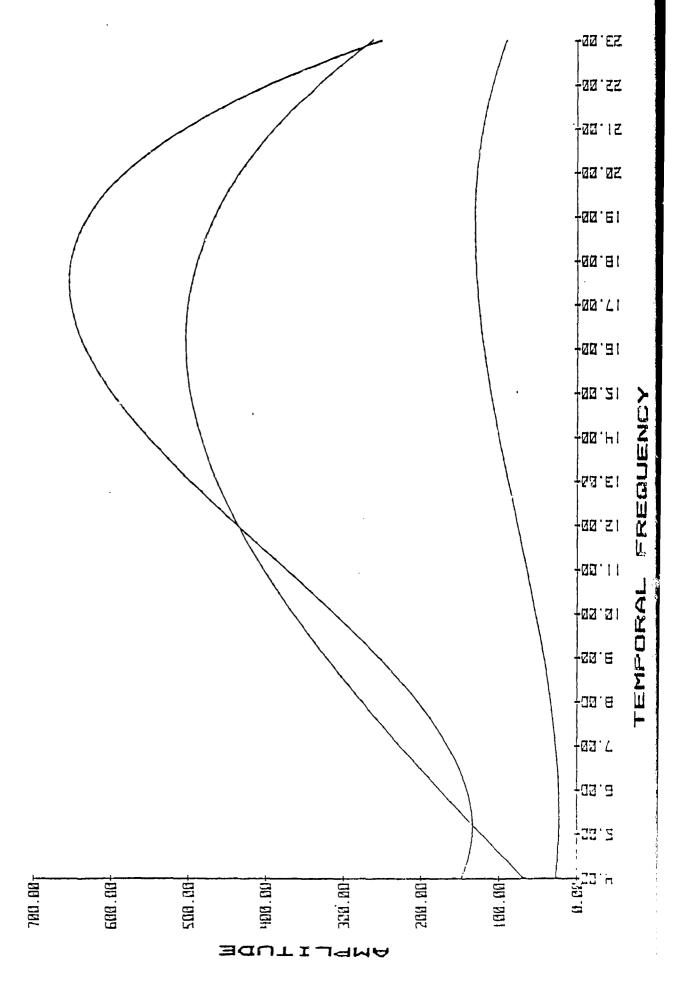


Figure 7D. Combination of Figures 7A, 7B, and 7C.

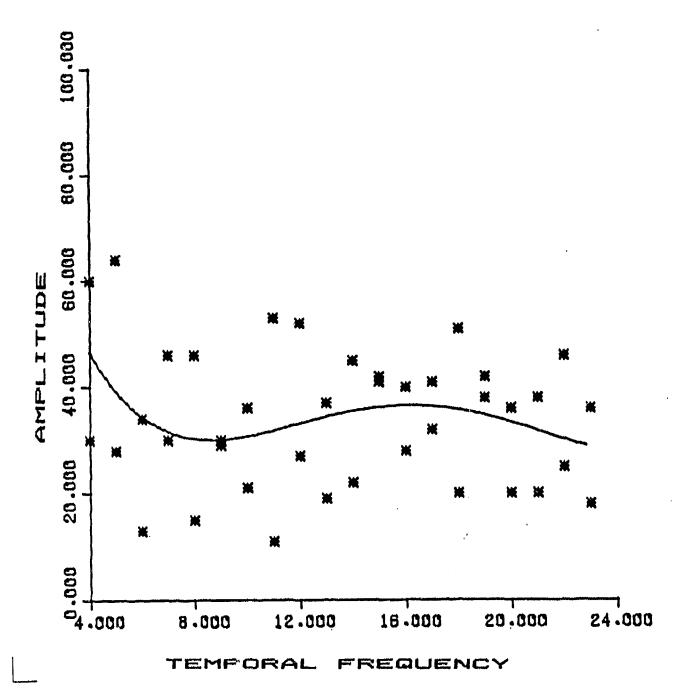


Figure 8A. The response curve for the fundamental component of the VER from two presentations to subject RM (RMMQ and RMMX) with the patterned background noise. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with

four degrees of freedam.

$$y = -.1239x^3 + 2.8236x^2 - 25.8911x + 112.3798$$

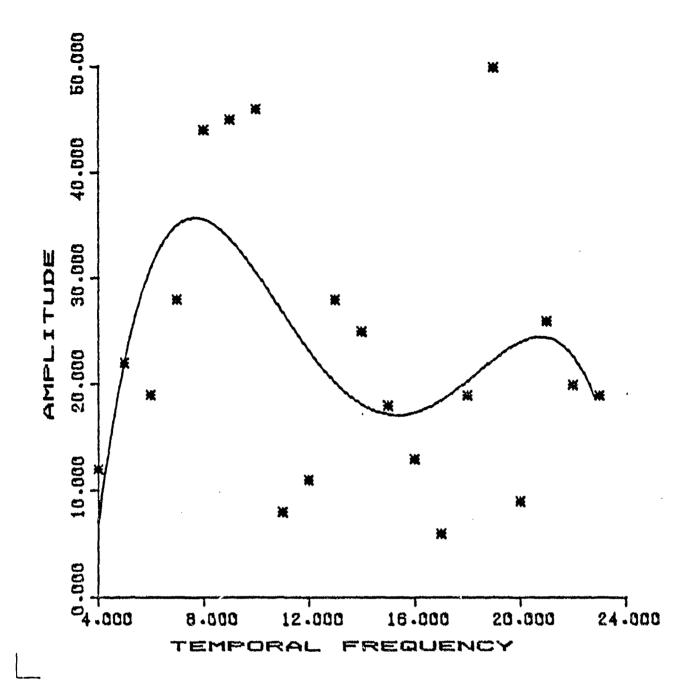


Figure 8B. The response curve for the fundamental component of the VER for a single presentation to subject LP (LPØN) with the patterned background noise. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .3909x^3 - 7.9765x^2 + 65.4728x - 150.4660$$

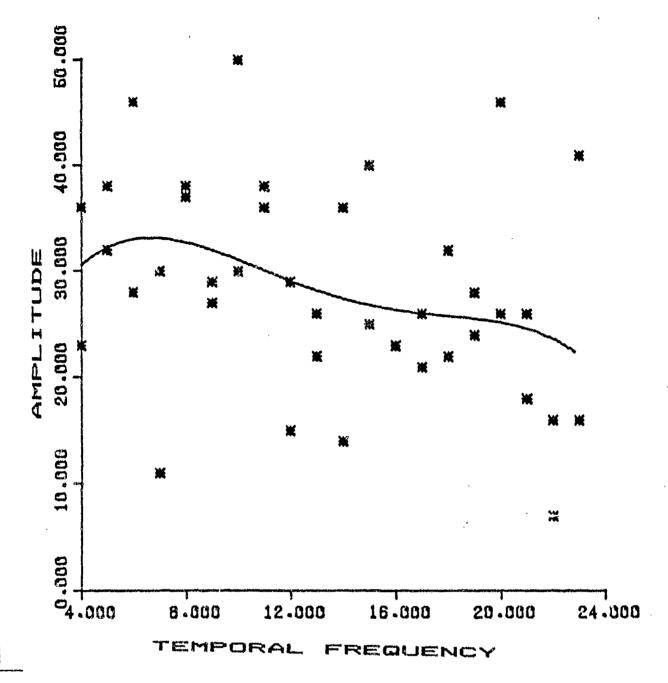


Figure 8C. The response curve for the fundamental component of the VER for two presentations for subject RR (RRØE and RRØO) with the patterned background noise. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .0576x^3 - 1.1628x^2 + 8.9955x + 9.7533$$

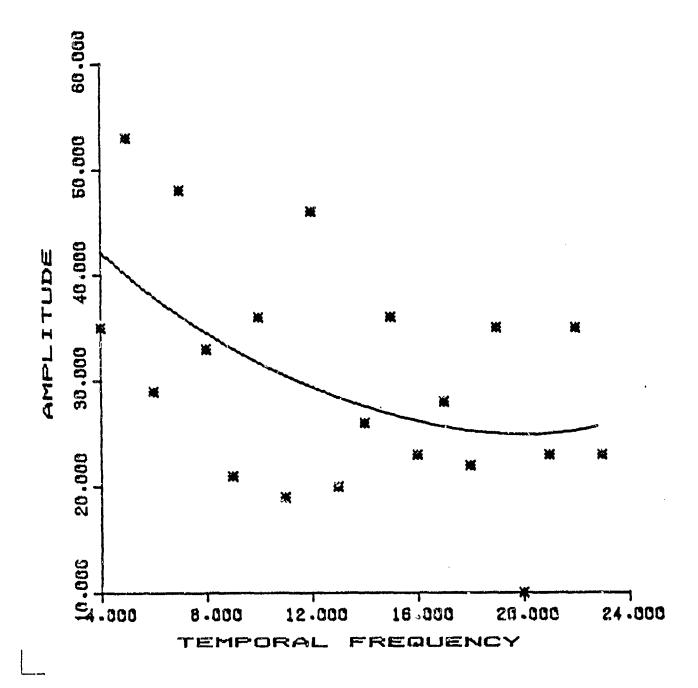


Figure 9A. The response curve for the fundamental component of the VER for a single presentation to subject RM (RMAA) with the unpatterned background noise as a stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.0072x^3 + .1994x^2 - 3.6353x + 53.9390$$

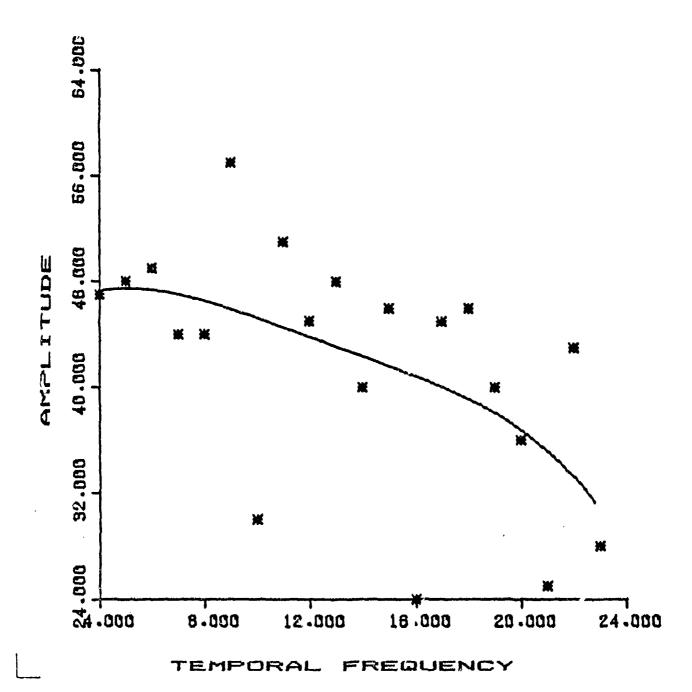


Figure 98. The response curve for the fundamental component of the VER for a single presentation to subject LP (LPØP) with the unpatterned background noise as a stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental examponent of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$\gamma = .0220x^3 + .4149x^2 + 2.7580x - 41.6054$$

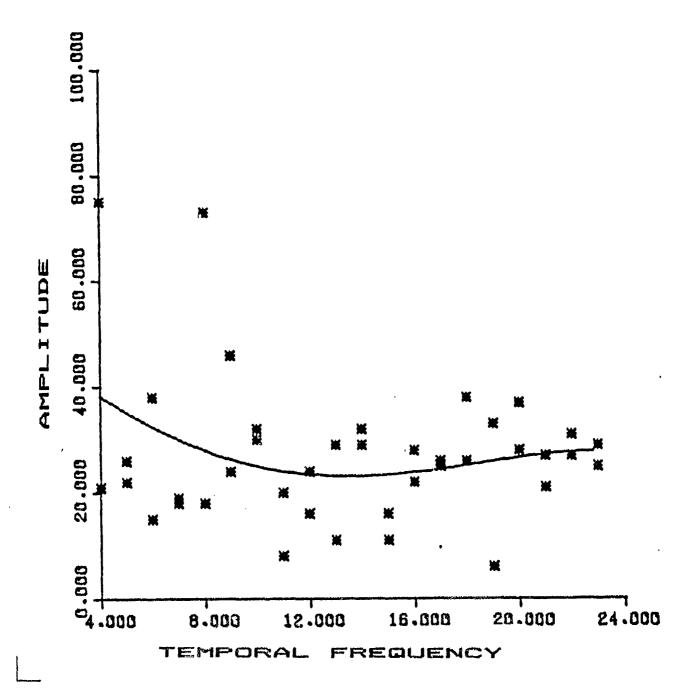


Figure 9C. The response curve for the fundamental component of the VER for two presentations to subject RR (RRØI and RRAA) with the unpatterned background noise as a stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .0091x^3 + .0735x^2 - 4.1360x + 53.2215$$

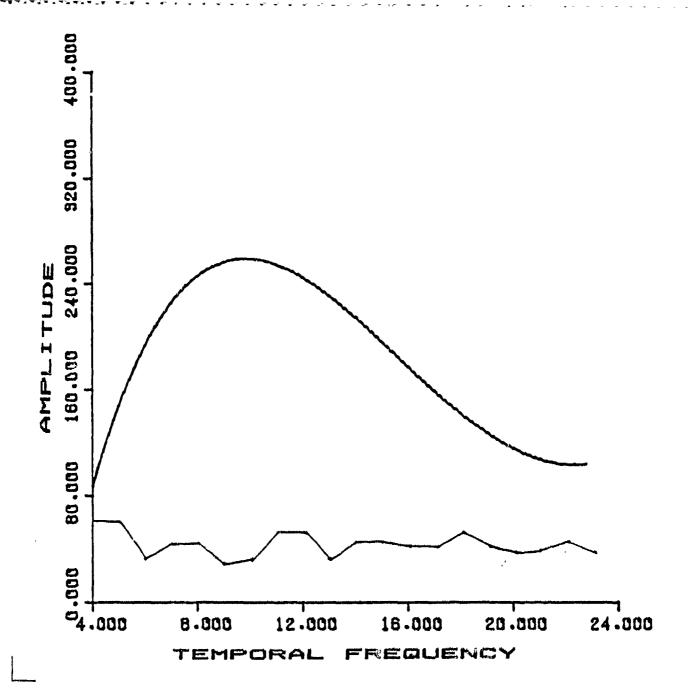


Figure 10A. The response curve for the fundamental component of the VER for five combined presentations to subject RM (RMYØ, RMØC, RMØM, RMØU, and RMDA) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VFR. The curve was fit using a polynomial regression with four degrees of freedom.

 $y = .3747x^3 - 12.6295x^2 + 152.4572x - 343.544$ The lower data points represent the background noise.

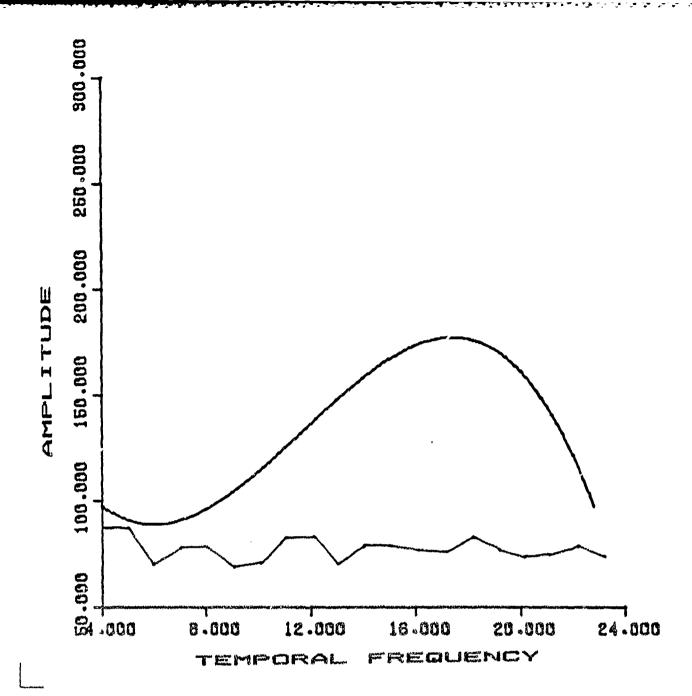


Figure 10B. The response curve for the fundamental component of the VER for five combined presentations to subject RM (RMMA, RMME, RMMO, RMMW, and RMEA) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.1053x^3 + 3.9425x^2 - 35.5912x + 183.6381$$

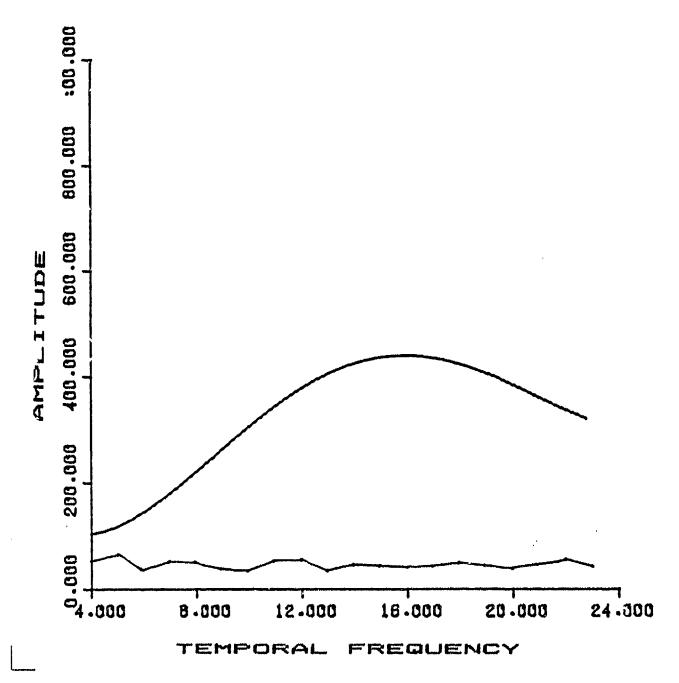


Figure 10C. The response curve for the fundamental component of the VER for six combined presentations to subject RM (RMWØ, RMØG, RMØI, RMWK, RMØS, and RMFA) with the unpatterned stimulus. the x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -1.0933x^3 + 20.0573x^2 - 106.5560x + 273.1473$$

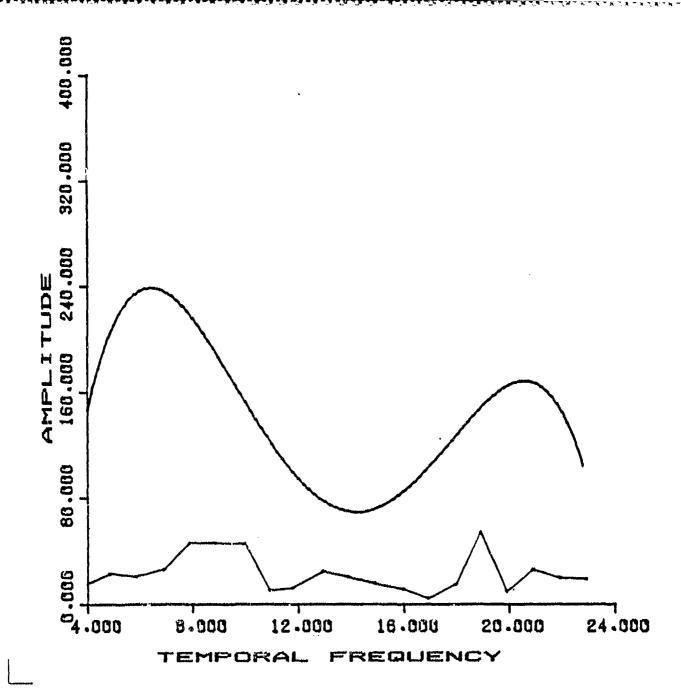


Figure 11A. The response curve for the fundamental component for the VER for four combined presentations to subject LP (LPØB, LPØD, LPZØ, and LPNØ) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = 2.8894x^3 - 54.2895x^2 - 395.7388x - 739.022$$

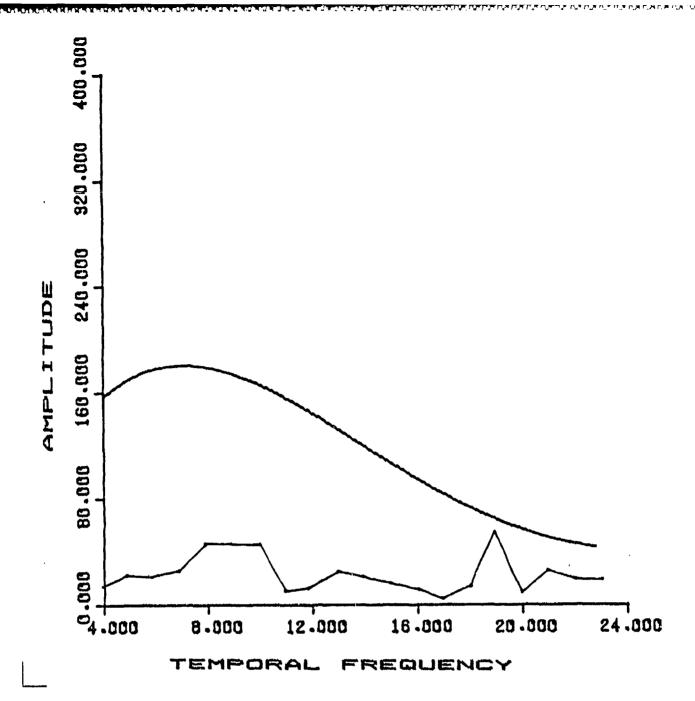


Figure 11B. The response curve for the fundamental component of the VER for five combined presentations to subject LP (LPPØ, LPVØ, LPXØ, LPXØ, LPØJ, and LPØL) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .2111x^3 - 5.8366x^2 + 54.4187x + 19.6811$$

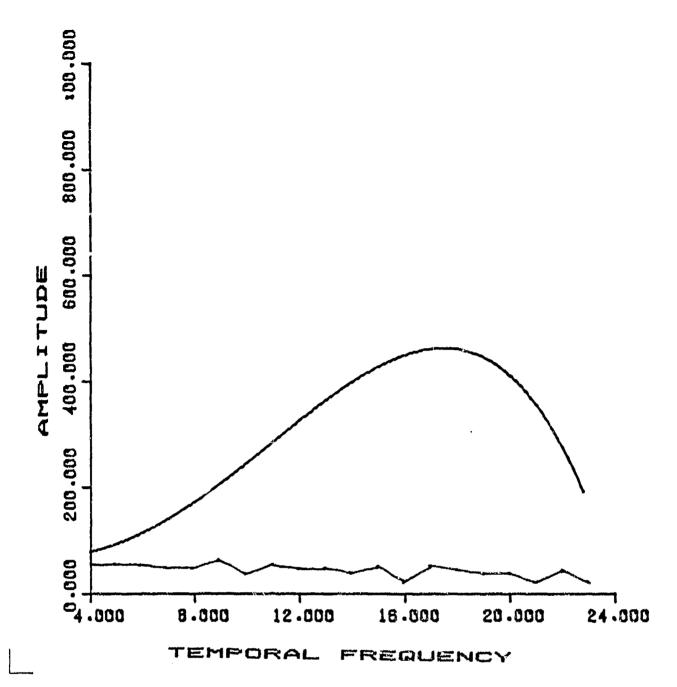


Figure 11C. The response curve for the fundamental component of the VER for five combined presentations to subject LP (LPEØ, LPØF, LPØF, LPØF, LPØF, LPØF, LPØF, LPØF, LPØF, LPØF, and LPTØ) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

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$$y = .0675x^3 + 3.1828x^2 - 14.9686x + 84.9571$$

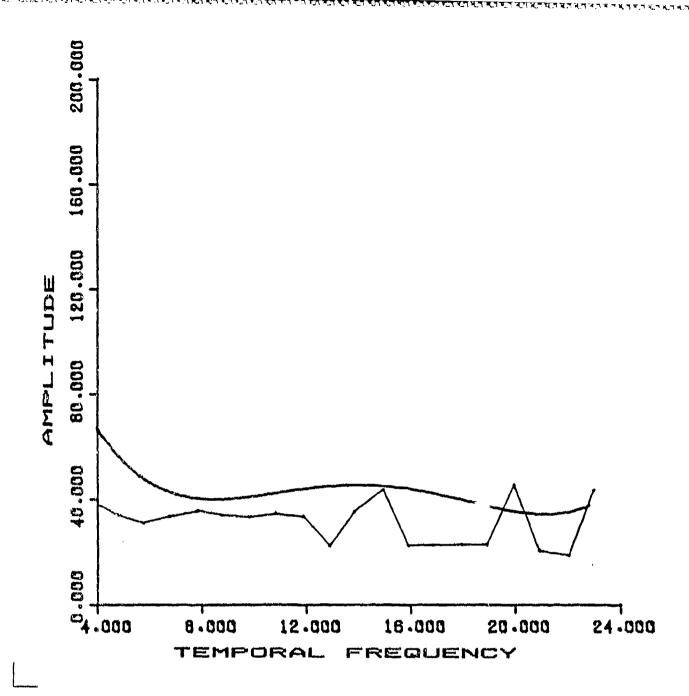
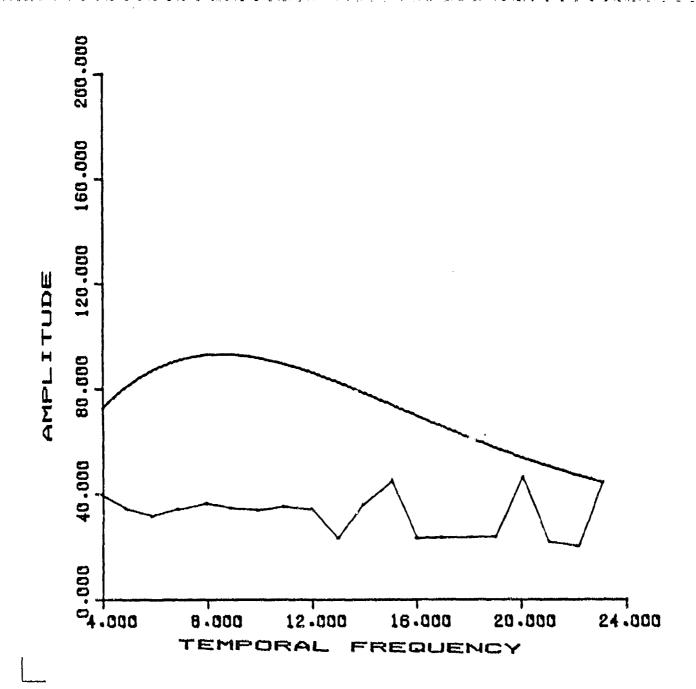


Figure 12A. The response curve for the fundamental component of the VER for three combined presentations to subject RR (RRUØ, RRØK, and RRØM) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.2906x^3 + 5.9284x^2 - 50.047x + 189.5445$$



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Figure 12B. The response curve for the fundamental component of the VER for four combined presentations to subject RR (RRMØ, RRSØ, RRØC, and RRØE) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = .0917x^3 - 2.5825x^2 + 26.9147x + .8586$$

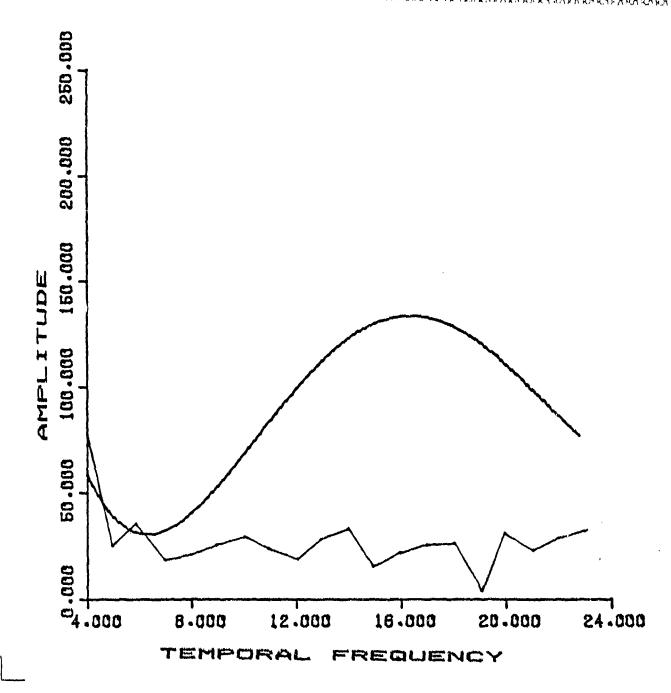


Figure 12C. This is the response curve for the fundamental component of the VER for four presentations to subject RR (RRCØ, RRWØ, RRYØ, and RRØA) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the relative magnitude of the fundamental component of the VER. The curve was fit using a polynomial regression with four degrees of freedom.

$$y = -.7072x^3 - 14.9137x^2 - 114.870x + 321.7287$$

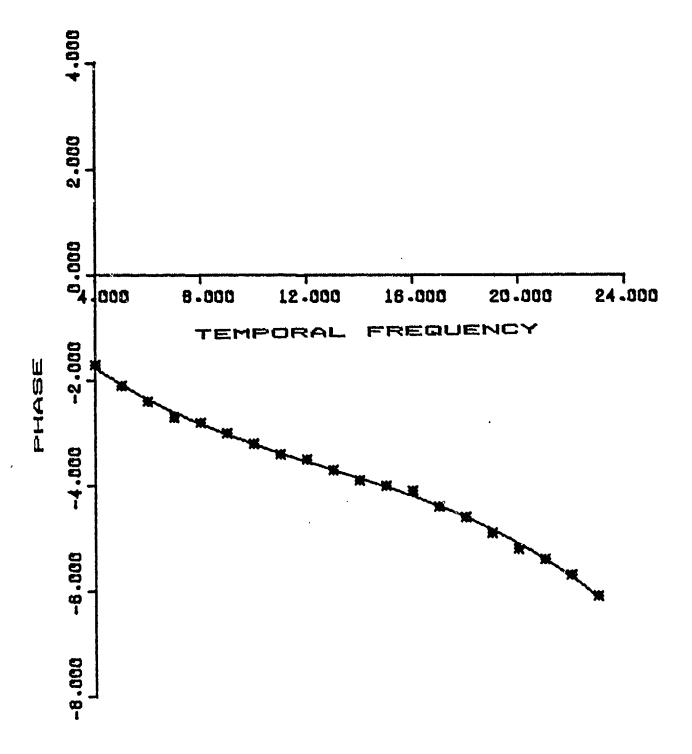


Figure 13A. The phase difference for the fundamental component of the VER for a single presentation to subject RM (RMDA) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = .0294x^2 - .5323x - .5890$$

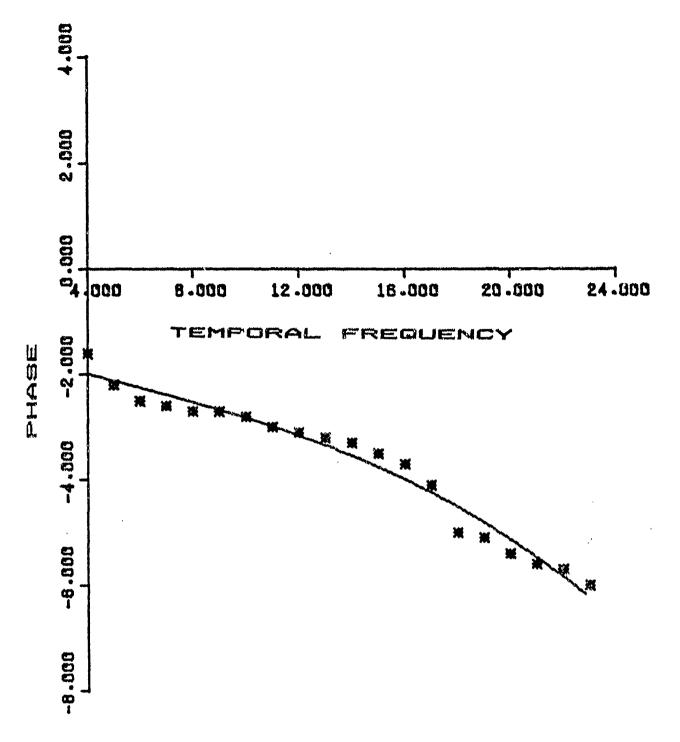


Figure 13B. The phase difference for the fundamental component of the VER for a single presentation to subject RM (RMMA) with 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = .0032x^2 - .1418x - 1.4560$$

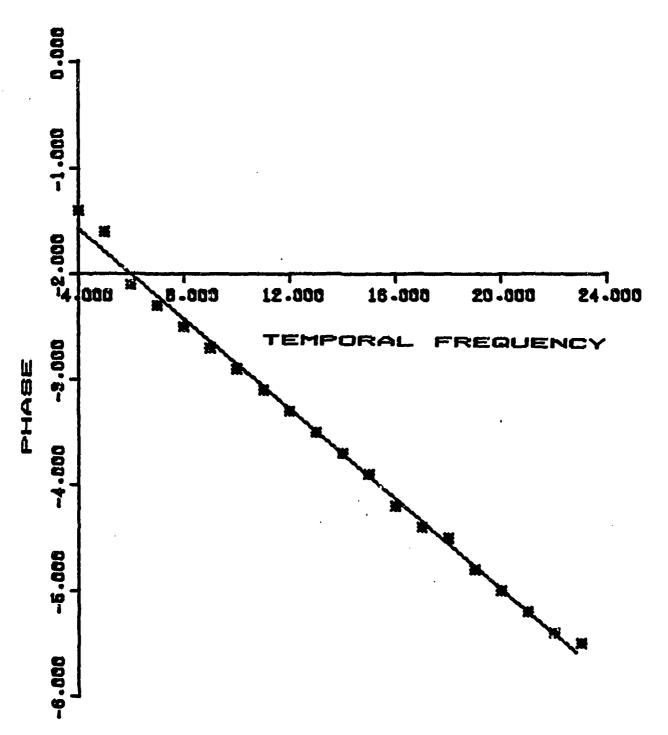
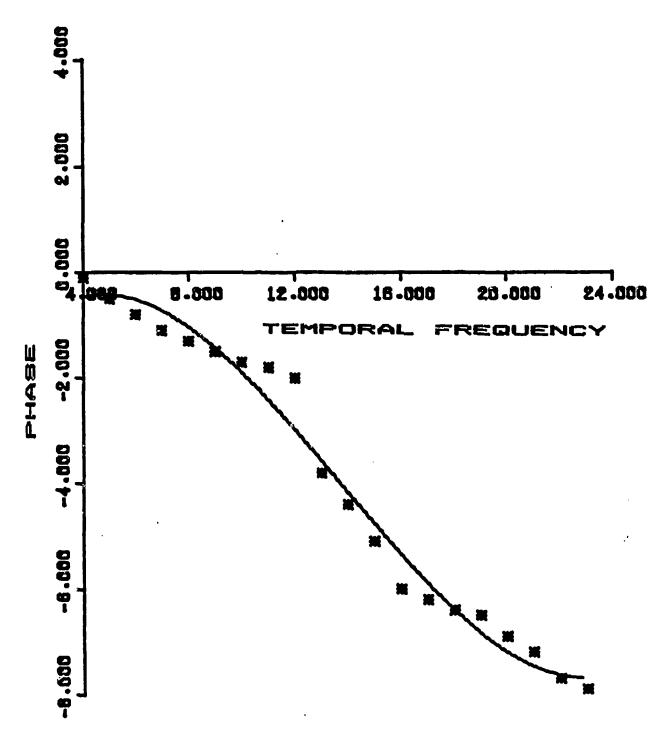


Figure 13C. The phase difference for the fundamental component of the VER for a single presentation to subject RM (RMWI) of the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = .2105x^2 - .2132x - .7214$$



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Figure 14A. The phase for the fundamental component of the VER for a single presentation to subject LP (IPZØ) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = -.1015x^2 + .7983x - 2.1826$$

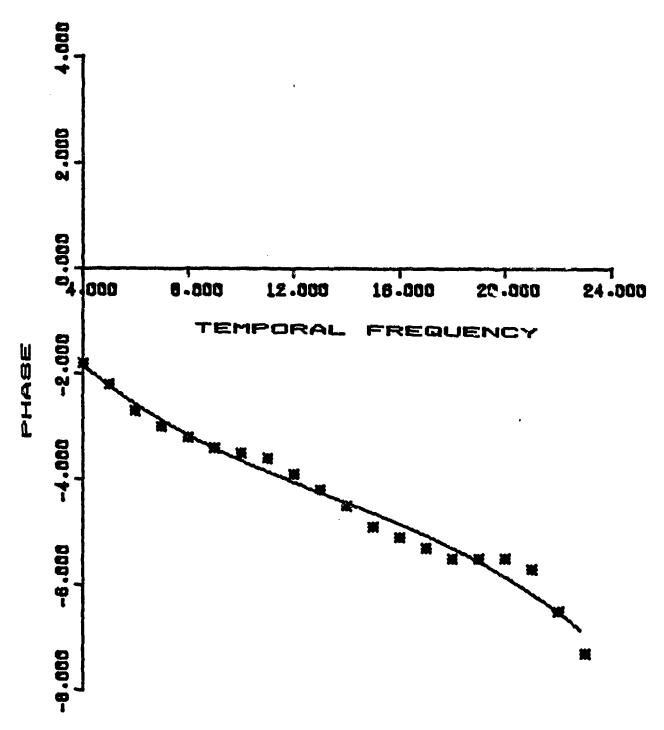


Figure 14B. The phase difference for the fundamental component of the VER for a single presentation to subject LP (LPXW) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

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$$y = .032x^2 - .6325x + .2148$$

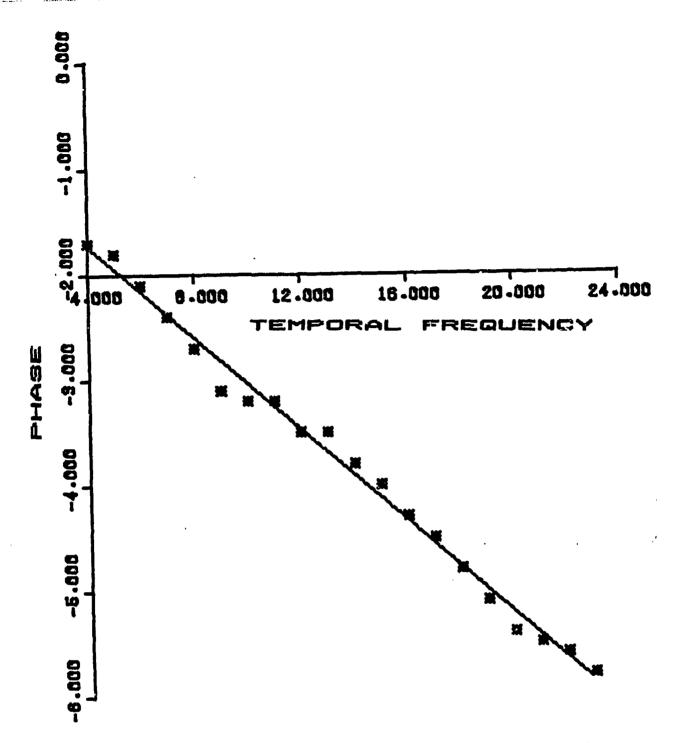


Figure 14C. The phase difference for the fundamental component of the VER for a single presentation to subject LP (LPTW) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

r = -.2185x - .8503

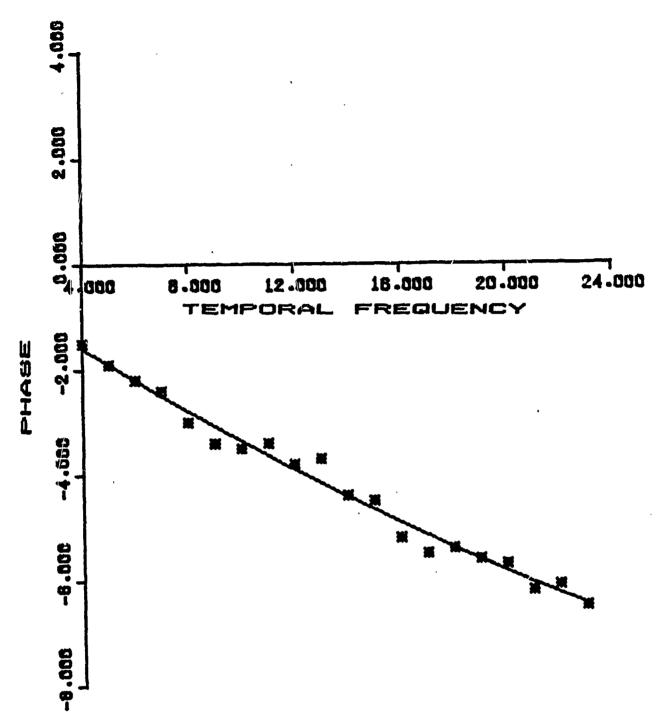


Figure 15A. The phase difference for the fundamental component of the VER for a single presentation to subject RR (RRØM) with the 15-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = .0029x^2 - .3366x - .2865$$

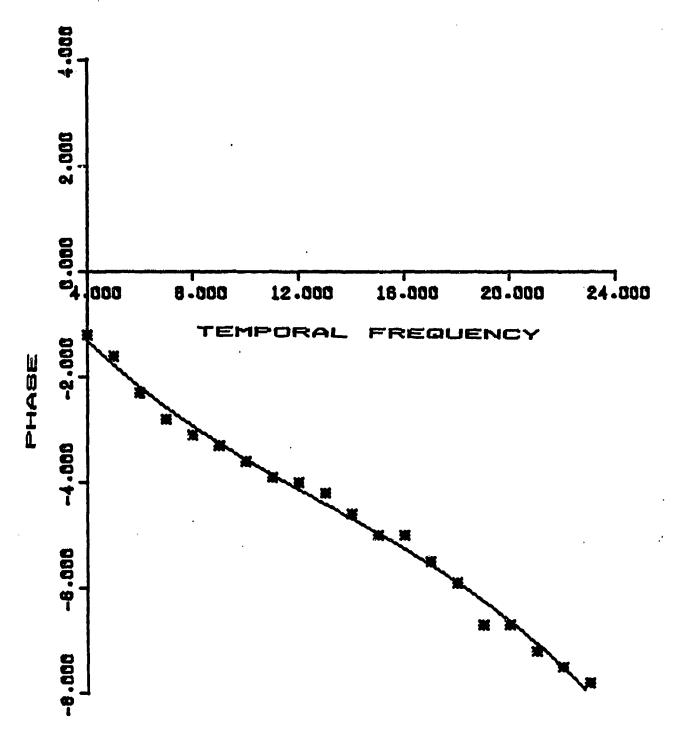


Figure 15B. The phase difference for the fundamental component of the VER for a single presentation to subject RR (RRSØ) with the 57-minute stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = .0337x^2 - .7141x + 1.0641$$

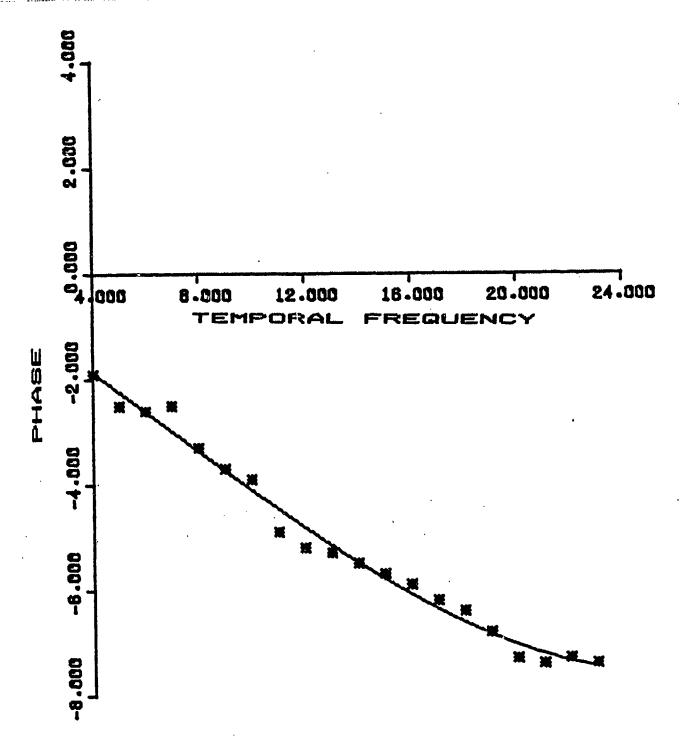
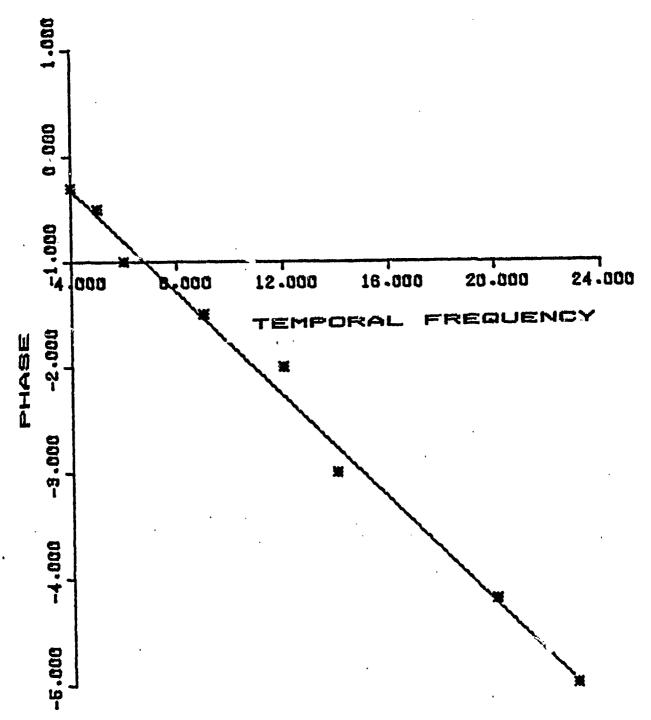


Figure 15C. The phase difference for the fundamental component of the VER for a single presentation to subject RR (RRWØ) with the unpatterned stimulus. The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = -.0074x^2 - .3216x - .4714$$



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Figure 16. The phase difference for the fundamental component of the VER for a single presentation extrapolated from Spekreijse, Esteves and Reits (1977). The x-axis represents the temporal frequency of the stimulus and the y-axis represents the phase in radians. The curve was fit using a polynomial regression with three degrees of freedom.

$$y = -.2451x + .5614$$

APPENDIX A

Date: 5-9-78

UNPATTERNED

	•						
RM	Hz	f ₁	f ₂	f ₃	øı	ø ₂	ø ₃
KØ	23	49314	76872	33894	275	-1.591	-1.730
Kl	22	27323	17109	46709	092	-1.633	-1.171
K2	21	65293	22274	15090	-1.794	-1.451	941
кз	20	101199	23609	58572	-1.528	-1.439	-1.813
K4	19	94442	41741	46869	-1.415	-1.650	-1.855
K5	18	125561	39929	24222	-1.470	-1.444	-1.633
К6	17	111835	56576	36245	-1.271	-1.152	-1.349
K7	16	76364	27612	51215	-1.495	-1.275	-1445
K8	15	11250	8170	35812	695	-1.686	-1.617
K9	14	41924	34724	41047	642	-1.644	-1.561
LØ	13	220556	92964	29450	-1.007	-1.243	-1.593
딦	12	106945	53385	30897	-1.967	925	-1.514
L2	11	116188 145314	45142 79591	37642	013	-1.854	-1.584
L3 L4	10 9	69030	79391 57968	20413 10699	-1.654	-1.524	-1.598
L5	8	208665	195413	87230	-1.603 -1.162	-1.413 730	-1.673
1.6	7	100481	15877	13850	-1.102	730 244	-1.305 -1.517
L7	6	103098	54008	27011	-1.117	081	-1.755
L8	5	36589	74527	7688	853	-1.720	-1.396
L9	4	17563	46779	28825	-1.131	-1.364	-1.603
				20000		2.001	2.005
				SMALL	CHECKS		
MØ	23	2880	29335	26042	-1.688	-1.712	-1.233
ML	22	19465	28182	34049	-1.719	-1.494	-1.418
M2	21	19518	28940	36834	-1.882	-1.369	-1.284
Mβ	20	16487	30156	46558	-1.612	-1.491	-1.953
M4	19	36438	14194	135085	-1.275	-1.688	-1.345
M5	18	60515	13499	45013	-1.625	-1.642	-1.876
M6	17	9405	10238	35322	-1.533	-1.100	-1.323
M7	16	15508	25673	32109	-1.554	-1.943	-1.239
M8	15	105566	38275	21450	-1.574	329	-1.912
M9	14	32106	3005	10881	-1.091	426	-1.464
NØ	13	124845	21038	24856	911	-1.004	-1.437
N1	12	46138	13047	22726	796	-1.697	-1.448
N2	11	13062	38895	20559	-1.167	-1.844	-1.659
из	10	67041	29858	30530	-1.727	-1.271	-1.590
N4	9	1338	17083	18047	-1.127	-1.608	-1.545
NS	8	43465	42594	19409	-1.967	-1.338	-1.837
N6	7	58566	24622	4683	-1.675	-1.725	863
N7	6	49566	29071 27999	41086 48791	-1.506	-1,350	-1.616
М8 6И	5 4	44626 46877	27999 31526	26599	-1.307 -1.243	-1.462 -1.014	-1.359 -1.292

Date: 5-9-78

LARGE CHECKS

RM	Hz	f ₁	f_2	£3	ø _l	ø ₂	ø ₃
00/	23	51162	31327	23236	-1.704	-1.754	-1.318
Ol	22	89331	57869	67569	-1.594	-1.423	-1.619
02	21	86313	2853 9	36022	-1.459	-1.538	-1.218
03	20	79217	32084	224738	-1.688	-1.451	-1.898
04	19	41456	48196	99142	-1.189	-1.385	-1.451
05	18	51.776	44354	32596	-1.094	-1.323	-1.678
06	17	54180	29632	8593	-1.143	-1.511	-1.473
07	16	101099	35442	71790	-1,532	-1.360	-1.492
08	15	95988	46278	18982	-1.246	-1.328	-1.800
09	14	8058	25396	37074	078	-1.501	-1.234
PØ	13	28011	36735	35025	-1.849	-1.729	-1.669
Pl	12	131374	41141	56054	-1.109	-1.434	-1.871
P2	11	25374	57539	44343	-1.968	-1.519	-1.518
P3	īC	39987	37649	37189	-1.743	-1.604	-1.395
P4	9	47187	44916	43624	~1.532	-1.525	-1.439
P5	8	45918	22765	25459	-1.617	-1.605	-1.532
P6	7	84339	25914	28750	-1.504	-1.352	-1.531
P7	6	54553	21615	27902	-1.594	-1.407	-1.421
P8	5	26382	38470	26333	-1.404	-1.489	-1.431
p9	4	14188	23413	28744	-1.822	-1.097	-1.404

Date: 5-26-78

LARGE CHECKS

RM	Hz	f ₁	f ₂	f ₃	ø _l	ø ₂	ø ₃
RØ	4	22081	7207	19132	-1.309	-1.615	-1.465
Rl	5	34664	19884	8102	-1.296	-1.668	-1.996
R2	6	32207	376 9	23354	-1.625	-1.09 9	-1.363
R3	7	12853	13678	12725	-1.813	-1.782	-1.563
R4	8	39403	13517	14481	-1.871	513	-1.497
R5	9	20306	11540	11651	-1.519	-1.459	-1.476
R6	10	30669	18979	15311	-1.964	-1.716	-1.353
R7	11	48718	29813	10441	499	-1.440	-1.212
R8	12	15638	19675	10439	166	-1.598	-1.792
. R9	13	24652	26999	12042	-1.476	-1.492	-1.743
SØ Sl	14 15	20209 51859	9746 9180	19673 17281	130	310 041	303 -1.693
S2	16	56766	14574	11934	567 951	-1.066	-1.093 -1.249
52 53	17	79265	38575	20445	-1.322	-1.638	-1.663
53 S4	18	98705	40361	55233	-1.481	-1.495	-1.736
S 5	19	72658	47921	121339	-1.445	-1.415	-1.653
56 56	20	64029	37094	218938	-1.463	-1.428	278
5 7	21	50321	60201	133970	-1.641	-1.652	950
S8	22	45195	54598	25327	-1.770	-1.488	-1.855
S9	23	35646	41121	45420	-1.821	-1.657	-1.139
				SMALI	· CHECKS		
	4	28093	26777			-1.485	-1.700
TØ	4 5	28093 40871	26777 18536	14394	-1.259	-1.485 -1.656	-1.700 -1.361
Tl	5	40871	18536	14394 25633	-1.259 -1.416	-1.656	-1.361
				14394 25633 19849	-1.259		
T1 T2	5 6 7	40871 70407	18536 25788	14394 25633	-1.259 -1.416 -1.633	-1.656 -1.632	-1.361 -1.552
T1 T2 T3	5 6	40871 70407 18097	18536 25788 31674	14394 25633 19849 13288	-1.259 -1.416 -1.633 -1.914	-1.656 -1.632 -1.486	-1.361 -1.552 -1.413
T1 T2 T3 T4	5 6 7 8	40871 70407 18097 45762	18536 25788 31674 18373	14394 25633 19849 13288 27461	-1.259 -1.416 -1.633 -1.914 002	-1.656 -1.632 -1.486 -1.392	-1.361 -1.552 -1.413 -1.634
T1 T2 T3 T4 T5 T6	5 6 7 8 9 10	40871 70407 18097 45762 13874 19914 58679	18536 25788 31674 18373 20992 27366 51952	14394 25633 19849 13288 27461 22265 27908 17861	-1.259 -1.416 -1.633 -1.914 002 -1.523 -1.643 -1.133	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650
T1 T2 T3 T4 T5 T6 T7 T8	5 6 7 8 9 10 11 12	40871 70407 18097 45762 13874 19914 58679 22090	18536 25788 31674 18373 20992 27366 51952 38182	14394 25633 19849 13288 27461 22265 27908 17861 19762	-1.259 -1.416 -1.633 -1.914 002 -1.523 -1.643 -1.133 -1.141	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577 875	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461
T1 T2 T3 T4 T5 T6 T7 T8	5 6 7 8 9 10 11 12 13	40871 70407 18097 45762 13874 19914 58679 22090 7776	18536 25788 31674 18373 20992 27366 51952 38182 9500	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577 875 -1.909	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553
T1 T3 T4 T5 T6 T7 T8 T9 U0	5 6 7 8 9 10 11 12 13 14	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577 875 -1.909 788	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666
T1 T3 T4 T5 T6 T7 T9 U1	5 6 7 8 9 10 11 12 13 14 15	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577 875 -1.909 788 -1.281	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801
T1 T3 T4 T5 T6 T7 T9 U1 U1 U1 U1 U1	5 6 7 8 9 10 11 12 13 14 15 16	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577 875 -1.909 788 -1.281 -1.261	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388
T1 T3 T4 T5 T6 T7 8 T9 W U U U U U U U U U U U U U U U U U U	5 6 7 8 9 10 11 12 13 14 15 16 17	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133 27708	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336 18225	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775 12249	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499 -1.712	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577875 -1.909788 -1.281 -1.261 -1.443	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388 -1.750
T1 T3 T4 T5 T6 T7 T8 T9 W U U U U U U U U U U U U U U U U U U U	5 6 7 8 9 10 11 12 13 14 15 16 17 18	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133 27708 31760	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336 18225 32697	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775 12249 39793	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499 -1.712 -1.888	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577875 -1.909788 -1.281 -1.261 -1.443 -1.687	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388 -1.750 -1.800
T1 T3 T4 T5 T6 T7 8 P W U U U U U U U U U U U U U U U U U U	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133 27708 31760 34270	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336 18225 32697 22648	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775 12249 39793 137018	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499 -1.712 -1.888 -1.323	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577875 -1.909788 -1.281 -1.261 -1.443 -1.687 -1.427	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388 -1.750 -1.800 -1.575
T1 T3 T4 T5 T6 T8 T9 W1 U2 U3 4 U5 U6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133 27708 31760 34270 27770	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336 18225 32697 22648 27431	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775 12249 39793 137018 163877	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499 -1.712 -1.888 -1.323 -1.568	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577875 -1.909788 -1.281 -1.261 -1.443 -1.687 -1.427 -1.537	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388 -1.750 -1.800 -1.575
T1 T3 T4 T5 T6 T8 T9 W U1 U U3 U4 U5 U5 U7	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133 27708 31760 34270 27770 20834	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336 18225 32697 22648 27431 38766	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775 12249 39793 137018 163877 177623	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499 -1.712 -1.888 -1.323 -1.568 -1.962	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577875 -1.909788 -1.281 -1.261 -1.443 -1.687 -1.537 -1.637	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388 -1.750 -1.800 -1.575 -249 -834
T1 T3 T4 T5 T6 T7 8 P9 U1 U2 U3 4 U5 U6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	40871 70407 18097 45762 13874 19914 58679 22090 7776 17376 25822 37133 27708 31760 34270 27770	18536 25788 31674 18373 20992 27366 51952 38182 9500 11526 11154 10336 18225 32697 22648 27431	14394 25633 19849 13288 27461 22265 27908 17861 19762 15743 30240 6695 21775 12249 39793 137018 163877	-1.259 -1.416 -1.633 -1.914002 -1.523 -1.643 -1.133 -1.141 -1.227 -1.396 -1.349 -1.499 -1.712 -1.888 -1.323 -1.568	-1.656 -1.632 -1.486 -1.392 -1.503 -1.532 -1.577875 -1.909788 -1.281 -1.261 -1.443 -1.687 -1.427 -1.537	-1.361 -1.552 -1.413 -1.634 -1.377 -1.634 -1.650 -1.461 -1.553 -1.666 -1.801 -1.388 -1.750 -1.800 -1.575

23 22 21 20 19	290742 367690 387957 394476	93466 71085 58200 90853	105004 73556 51869	-1.504 -1.357 -1.172	-1.346 -1.129 -1.535	-1.569 -1.204
21 20	387957	58200				
20			27002	⇒ L = J. / Z.		1 /(0)
	371410		350401			-1.493
73	400004		150491	-1.011	-1.377	-1.522
	402224	85334	87054	799	-1.094	-1.523
18	429374	68399	35744	644	586	-1.248
17	443186	104059	6113	477	209	228
16	513841	146828	93580	314	-1.876	-1.627
						-1.323
						-1.33
						642
12	479640	165953		-1.252	-1.860	-1.979
11	340330	275322	117845	-1.065	-1.208	-1.514
10	311103	313873	95635	896	735	~ . 902
9	250999	353705	96203	695	320	399
8	241317	385988	163244	519	-1.783	-1.58
7	193206	256407				686
						-1.43
						24
4	74415	119649	74825	-1.527	-1.994	-1.435
			SMALL	CHECKS	,	
23	A1899	57134	50987	- 710	-1 263	-1.346
						-1.427
						255
						979
						32
						-1.66
						-1.299
						765
						292
						011
						-1.593
						-1.165
						338
						-1.760
						-1.119
						513
						-1.96
6	177365	190544			095	-1.31
5	195257	209917	91702	-1.924	-1.721	78
4	147719	153652	47504	-1.518	-1.276	096
			A-4			
	15 14 13 12 11 10 9 8 7 6 5 4 23 22 21 20 19 18 17 16 15 14 13 12 11 0 9 8 7 6 5	15 561213 14 595897 13 574911 12 479640 11 340330 10 311103 9 250999 8 241317 7 193206 6 215326 5 155837 4 74415 23 41899 22 70210 21 46979 20 94575 19 114267 18 153602 17 146775 16 228479 15 272845 14 305709 13 232712 12 285406 11 237832 10 225792 9 264436 8 275585 7 256806 6 177365 5 195257	15 561213 190204 14 595897 197234 13 574911 161990 12 479640 165953 11 340330 275322 10 311103 313873 9 250999 353705 8 241317 385988 7 193206 256407 6 215326 161211 5 155837 102806 4 74415 119649 23 41899 57134 22 70210 48301 21 46979 32374 20 94575 48488 19 114267 40474 18 153602 35523 17 146775 59636 16 228479 97177 15 272845 77800 14 305709 84707 13 232712 124464 12 285406 139777 11 237832 180924 10 225792 159016 9 264436 160136 8 275585 184517 7 256806 188447 6 177365 190544 5 195257 209917	15 561213 190204 61785 14 595897 197234 41412 13 574911 161990 16313 12 479640 165953 68612 11 340330 275322 117845 10 311103 313873 95635 9 250999 353705 96203 8 241317 385988 163244 7 193206 256407 78936 6 215326 161211 30201 5 155837 102806 77982 4 74415 119649 74825 SMALI 23 41899 57134 50987 22 70210 48301 33611 21 46979 32374 25884 20 94575 48488 197664 19 114267 40474 28107 18 153602 35523 39647 17 146775 59636 21188 16 228479 97177 70921 15 272845 77800 52229 14 305709 84707 47528 13 232712 124464 20178 12 285406 139777 19644 11 237832 180924 38606 10 225792 159016 41891 9 264436 160136 59123 8 275585 184517 41789 7 256806 188447 62208 177365 190544 92625 5 195257 209917 91702 4 147719 153652 47504	15 561213 190204 61785087 14 595897 197234 41412 -1.773 13 574911 161990 16313 -1.539 12 479640 165953 68612 -1.252 11 340330 275322 117845 -1.065 10 311103 313873 95635896 9 250999 353705 96203695 8 241317 385988 163244519 7 193206 256407 78936340 6 215326 161211 30201069 5 155837 102806 77982 -1.686 4 74415 119649 74825 -1.527 SMALL CHECKS 23 41899 57134 50987710 22 70210 48301 33611896 21 46979 32374 25884782 20 94575 48488 197664632 19 114267 40474 28107613 18 153602 35523 39647543 17 146775 59636 21188307 16 228479 97177 70921139 15 272845 77800 52229 -1.9567 14 305709 84707 47528 -1.785 13 232712 124464 20178 -1.559 12 285406 139777 19644 -1.370 11 237832 180924 38606 -1.238 10 225792 159016 41891 -1.049 9 264436 160136 59123926 8 275585 184517 4178977.4 7 256806 188447 62208431 6 177365 190544 92625220 5 195257 209917 91702 -1.924 4 147719 153652 47504 -1.518	15 561213 190204 61785087 -1.631 14 595897 197234 41412 -1.773 -1.217 13 574911 161990 16313 -1.539687 12 479640 165953 68612 -1.252 -1.860 11 340330 275322 117845 -1.065 -1.208 10 311103 313873 95635896735 9 250999 353705 96203695320 8 241317 385988 163244519 -1.783 7 193206 256407 78936340 -1.147 6 215326 161211 30201069641 5 155837 102806 77982 -1.686219 4 74415 119649 74825 -1.527 -1.994 SMALL CHECKS 23 41899 57134 50987710 -1.263 22 70210 48301 33611896801 21 46979 32374 25884782641 20 94575 48488 197664632522 19 114267 40474 28107613266 18 153602 35523 39647543 -1.993 17 146775 59636 21188307 -1.844 16 228479 97177 70921139 -1.474 15 272845 77800 52229 -1.957 -1.128 14 305709 84707 47528 -1.785917 13 232712 124464 20178 -1.559621 12 285406 139777 19644 -1.370177 11 237832 180924 38606 -1.238 -1.923 10 225792 159016 41891 -1.049 -1.571 9 264436 160136 59123926 -1.319 8 275585 184517 41789774938 7 256806 188447 62208431547 6 177365 190544 92625220095 5 195257 209917 91702 -1.924 -1.721 4 147719 153652 47504 -1.518 -1.276

Date: 6-21-78

LARGE CHECKS

RM	HZ	f ₁	f ₂	f ₃	\emptyset_1	ø ₂	ø ₃
ØA	23	84575	59182	8103	-1.086	-1.722	034
1A	22	109139	27212	4039	719	-1.495	-1.300
2A	21	157537	44445	25192	614	-1.251	-1.395
3 A	20	140783	58281	119012	471	-1.244	-1.737
44	19	166112	75277	50914	132	-1.160	514
5A	18	179852	62346	40902	059	759	079
6A	17	207979	35868	0422	173	944	078
7A	16	199006	57967	20153	-1.770	694	-1.231
8A	15	222555	54733	20193	-1.599	120	-1.258
9A	14	211523	41862	8373	-1.313	-1.675	-1.752
ØB	13	183212	27881	56950	-1.247	-1.392	435
ĺB	12	155186	6464	28414	-1.128	097	-1.975
2B	11	105677	19862	35511	-1.010	-1.412	-1.819
3B	10	101394	46922	52323	874	-1.384	-1.227
4B	9	106165	87678	64278	788	-1.151	615
5B	8	129805	118099	43256	723	877	111
6B	7	108364	146605	62576	633	369	-1.690
7B	6	164119	161374	88028	580	014	-1.138
8B	5	158190	148705	69831	268	-1.493	101
9B	4	64270	154049	5128	-1.648	998	394

Date: 8-4-78

RM	Hz	f ₁	f ₂	£3	Øı	ø ₂	ø ₃
9C	4	79219	74444	61655	-1.521	-1.467	-1.501
1C	5	127 9 56	234381	100865	055	-1.69 6	847
2C	6	214219	163202	116346	513	045	-1.439
3C	7	220098	155404	99333	736	607	-1.849
4C	8	273004	124316	39852	880	-1.038	771
5C	9	325244	129271	78763	-1.053	-1.360	-1.331
6C	10	303389	138999	60931	-1.230	-1.601	-1.681
7C	11	317619	77908	10586	-1.389	-1.872	-1.442
8C	12	281470	64287	45440	-1.565	282	-1.326
9C	13	263371	58459	54088	-1.658	-1.002	-1.493
ØD	14	272675	75350	28417	-1.848	-1.166	-1.813
ъ	15	187485	59988	34615	-1.895	-1.393	-1.331
210	16	275267	113679	29146	266	-1.581	-1.417
310	17	173512	62451	39013	393	-1.651	-1.497
4D	18	93578	25210	80500	822	-1.736	-1.647
5D	19	253796	20086	53361	939	-1.042	897
6D	20	280134	50753	739395	-1.140	1.242	401
70	21	288153	46304	39849	-1.299	-1.387	158
810	22	196266	33224	40879	-1.582	-1.348	-1.379
9D	23	166549	57038	15808	-1.832	-1.361	-1.671
				LARGE	CHECKS		
9E	4	81557	85956	63801	-1.207	938	-1.623
1E		65025	150340	35745	-1.721	-1.455	046
2E	5 6	91661	139685	70650	262	-1.744	996
3E	7	60749	39743	99858	643	291	-1.461
4E	8	60583	41999	41172	838	847	-1.888
5F	9	55232	87126	28573	-1.140	-1.286	559
6±:	10	82454	42590	74640	-1.008	-1.497	-1.225
7E	ii	99548	41664	71659	971	-1.626	-1.569
8E	12	124028	50248	75529	-1.159	-1.511	-1.932
9E	13	118059	25572	3393	-1.244	-1.595	-1.084
ØF	14	149084	53584	24507	-1.337	-1.590	-1.343
1F	15	182915	49879	36106	-1.463	-1.799	-1.404
2F	16	175684	04640	59027	-1.596	107	-1.454
	17	169974	18044	62804	-1.910	448	-1.779
4F	18	174203	33145	57875	041	994	-1.887
5F	19	142473	69527	53553	249	-1.162	901
6F	20	148148	69344	523096	260	-1.355	-1.714
7F	21	148934	92179	24821	551	-1.550	402
8F	22	72297	65610	34494	847	-1.655	-1.536
9F	23	95775	64022	12059	-1.058	-1.689	100

Date: 8-4-78

RM	Hz	f ₁	f ₂	f ₃	\emptyset_1	ø ₂	ø ₃
9G	4	96051	182770	75411	-1.526	-1.874	-1.510
1G	5	155062	128647	54081	-1.633	338	212
2G	6	217777	142886	59936	-1.933	919	-1.493
3G	7	203568	155693	30689	241	-1.230	-1.080
4G	8	350765	288364	123492	493	-1.725	-1.455
5G	9	268116	224055	73764	774	275	255
6G	10	349489	223565	94033	996	804	-1.107
7G	11	360347	252280	102086	-1.187	-1.258	-1.621
8G	12	409183	174219	52159	-1.364	-1.692	131
9G	13	358593	100439	39321	-1.519	302	749
ØH	14	373352	114387	51757	-1.698	-1.003	-1.287
1H	15	480568	148093	48183	-1.951	-1.491	-1.500
211	16	472982	135203	31832	126	-1.704	-1.672
3H	17	452878	124990	8732	303	-1.994	-1.666
4H	18	443128	85495	11608	507	361	-1.667
5H	19	450859	67727	73626	780	952	-1.221
6H	20	447994	40682	453504	-1.013	-1.216	286
7H	21	457094	21521	31995	-1.195	940	-1.853
8 H	22	379692	65761	39239	-1.351	961	-1.529
9H	23	425839	88878	12933	-1.501	-1.302	-1.373

Date:	8-11-78	UNPATTERNED

RM	Hz	f _l	f ₂	£3	ø ₁	ø ₂	ø ₃
91	23	266740	85813	37497	-1.574	-1.251	-1.561
1I	22	304068	55366	44541	-1.432	-·1.220	-1.522
2I	21	365230	24352	41646	-1.250	-1.325	-1.481
3I	20	366062	64930	183910	-1.010	-1.198	-1.692
4 I	19	404901	70840	37056	868	989	-1.302
5I	18	414395	84309	43653	578	496	-1.495
6I	17	444551	103181	31917	435	178	-1.649
7I	16	484091	136431	33677	~ .258	-1.817	-1.600
8I	15	526027	186915	37741	-1.951	-1.452	-1.518
9I	14	418214	132591	61777	-1.731	-1.067	-1.452
Ø	13	356868	122780	47582	-1.522	357	-1.259
Ŋ	12	366121	201530	27920	-1.395	-1.797	456
27 37	11 10	365617 338349	285686 217273	107720	-1.175	-1.369 981	-1.768
30 47	9	255565	205049	107042 57056	075 792	961 465	-1.259 409
5J	8	213362	219486	70044	792 583	-1.860	-1.640
<u>ಹ</u>	7	154405	139071	46561	333	-1.404	-1.491
∞ 7J	6	130569	75992	37791	165	980	-1.291
ಖ	5	116090	47498	4153	-1.647	681	-1.310
9J	4	82413	149140	61781	-1.412	-1.911	-1.587
		· • * * * * * * * * * * * * * * * * * * 	·	TINIDA	רואואאינייי		
				UNPA	TTERNED	•	
ØK	4	74815	138804	UNPA 61110	TTERNED -1.437	-1.870	-1.582
JK ØK	5	74815 138464	138804 59743			-1.870 431	-1.582 582
	5 6			61110	-1.437		
1K	5 6 7	138464	59743 99422 175053	61110 47802 48268 57874	-1.437 -1.646 -1.981 298	431	582
1K 2K 3K 4K	5 6 7 8	138464 163257 199308 181601	59743 99422 175053 261599	61110 47802 48268 57874 78286	-1.437 -1.646 -1.981 298 624	431 983 -1.342 -1.800	582 -1.400 -1.266 -1.588
1K 2K 3K 4K 5K	5 6 7 8 9	138464 163257 199308 181601 212338	59743 99422 175053 261599 213431	61110 47802 48268 57874 78286 57269	-1.437 -1.646 -1.981 298 624 735	431 983 -1.342 -1.800 370	582 -1.400 -1.266 -1.588 390
1K 2K 3K 4K 5K 6K	5 6 7 8 9	138464 163257 199308 181601 212338 267448	59743 99422 175053 261599 213431 217940	61110 47802 48268 57874 78286 57269 108895	-1.437 -1.646 -1.981 298 624 735 988	431 983 -1.342 -1.800 370 864	582 -1.400 -1.266 -1.588 390 -1.216
1K 2K 3K 4K 5K 6K 7K	5 6 7 8 9 10	138464 163257 199308 181601 212338 267448 298926	59743 99422 175053 261599 213431 217940 303076	61110 47802 48268 57874 78286 57269 108895 96841	-1.437 -1.646 -1.981 298 624 735 988 -1.165	431 983 -1.342 -1.800 370 864 -1.280	582 -1.400 -1.266 -1.588 390 -1.216 -1.708
1K 2K 3K 4K 5K 6K 7K 8K	5 6 7 8 9 10 11 12	138464 163257 199308 181601 212338 267448 298926 305461	59743 99422 175053 261599 213431 217940 303076 200402	61110 47802 48268 57874 78286 57269 108895 96841 26175	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305	431 983 -1.342 -1.800 370 864 -1.280 -1.704	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127
1K 2K 3K 4K 5K 6K 7K 8K 9K	5 6 7 8 9 10 11 12 13	138464 163257 199308 181601 212338 267448 298926 305461 330621	59743 99422 175053 261599 213431 217940 303076 200402 99083	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078
12 25 45 55 67 85 95 £1	5 6 7 8 9 10 11 12 13 14	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434
1X X X X X X X X X X X X X X X X X X X	5 6 7 8 9 10 11 12 13 14 15	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424
12.23.43.56.76.86.56.17.21.21.21.21.21.21.21.21.21.21.21.21.21.	5 6 7 8 9 10 11 12 13 14 15 16	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424 -1.626
以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及	5 6 7 8 9 10 11 12 13 14 15 16	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607 423166	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055 60981	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276 25029	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264 500	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896 146	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424 -1.626 -1.755
12 23 45 56 75 85 95 LL	5 6 7 8 9 10 11 12 13 14 15 16 17 18	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607 423166 410411	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055 60981 49866	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276 25029 18926	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264 500 745	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896 146 675	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424 -1.626 -1.755 -1.396
以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及以及	5 6 7 8 9 10 11 12 13 14 15 16 17 18	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607 423166 410411 342359	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055 60981 49866 33295	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276 25029 18926 14796	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264 500 745 905	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896 146 675 881	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424 -1.626 -1.755 -1.396 958
以	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607 423166 410411 342359 312239	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055 60981 49866 33295 18722	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276 25029 18926 14796 196835	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264 500 745 905 -1.108	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896 146 675 881 -1.201	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424 -1.626 -1.755 -1.396 958 -1.305
以及	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607 423166 410411 342359 312239 319898	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055 60981 49866 33295 18722 37616	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276 25029 18926 14796 196835 51515	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264 500 745 905 -1.108 -1.273	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896 146 675 881 -1.201 -1.152	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.424 -1.626 -1.755 -1.396 958 -1.305 -1.501
以	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	138464 163257 199308 181601 212338 267448 298926 305461 330621 511016 455821 460607 423166 410411 342359 312239	59743 99422 175053 261599 213431 217940 303076 200402 99083 109519 168936 111055 60981 49866 33295 18722	61110 47802 48268 57874 78286 57269 108895 96841 26175 34956 37484 39300 34276 25029 18926 14796 196835	-1.437 -1.646 -1.981 298 624 735 988 -1.165 -1.305 -1.521 -1.687 -1.971 264 500 745 905 -1.108	431 983 -1.342 -1.800 370 864 -1.280 -1.704 300 987 -1.492 -1.896 146 675 881 -1.201	582 -1.400 -1.266 -1.588 390 -1.216 -1.708 127 -1.078 -1.434 -1.424 -1.626 -1.755 -1.396 958 -1.305

Date: 8-16-78

	M	1	43835	103890	75998	-1.745	-1.432	-1.855
ű		ij	80557	165792	41312	-1.952	-1.622	876
	M	6	121680	150780	10'737	502	071	-1.384
	M	7	184938	132914	90415	720	587	-1.729
	M	, 8	239298	142368	37488	868	-1.001	545
	M	9	295307	168712	77467	-1.107	-1.315	-1.356
	M	10	290314	186049	57828	-1.285	-1.653	-1.669
	M M	11	274521	118556	15990	-1.431	-1.055	-1.855
		12	242738	64929	60275	-1.431	414	-1.297
	M							
	M No	13	209210	52363	60360	-1.733	-1.071	-1.556
Ø		14	168674	56324	29766 13506	-1.757	-1.477	-1.671
	N	15	226887	66830	13596	017	-1.298	-1.355
	N	16	144530	68767	40491	105	-1.514	-1.360
	N	17	168437	63534	50397	354	-1.664	-1.443
4		18	158094	40568	50394	571	-1.817	-1.385
5		19	111373	13475	26994	-1.182	-1.583	-1.627
6		20	157374	16206	209031	-1.124	-1.365	048
	N	21	67286	19211	28749	-1.454	-1.193	-1.380
8		22	157021	26546	28535	-1.453	-1.391	-1.474
9	N	23	64140	64491	27437	-1.826	-1.433	-1.707
_					LARGE	CHECKS		
ø	Ó	4	68901	56766	63341	-1.515	877	-1.658
	.0	5	61032	91947	30720	-1.793	-1.320	-1.802
	0	6	92892	81385	21314	236	-1.747	-1.075
3	O	7	83971	37691	43161	320	-1.943	-1.570
4	0	8	67586	34224	55455	690	-1.132	-1.781
5	0	9	56407	18451	14599	785	-1.482	-1.578
6	0	10	111126	17212	41087	939	-1.490	-1.324
7	0	11	107833	35584	84212	-1.008	-1.366	-1.558
	0	12	115213	41735	36772	-1.149	-1.427	-1.808
	0	13	100933	47403	15638	-1.245	-1.542	-1.271
	Þ	14	163538	47787	17423	-1.407	-1.501	-1.054
	P	15	180564	36474	46052	-1.513	-1.777	-1.329
	P	16	151598	57073	62901	-1.642	-1.862	-1.296
	P	17	143092	30528	30094	-1.698	923	-1.452
4	P	18	137637	43309	10570	-1.956	-1.114	733
	P	19	148971	49074	26286	034	-1.328	738
	P	20	108984	75184	420455	224	-1.500	320
6		21	98470	44172	35338	359	-1.583	-1.685
6 7	P			00001	20012	483	-1.733	-1.677
6 7	P P	22 23	100113	22801	29912	405	- 4	

Date: 8-16-78 PATTERNED BACKGROUND - EYES OPEN

RM	Hz	fl	f ₂	f ₃	ø _l	ø ₂	ø ₃
ØQ	4	29633	21214	1913	-1.461	-1.515	177
1Q	5	28188	12342	28822	-1.700	-1.450	-1.429
2Q	6	12665	40913	31115	376	-1.207	-1.350
3Q	7	30435	33882	30160	-1.392	-1.596	-1.507
4Q	8	15449	19391	26642	-1.661	-1.525	-1.440
5Q	9	30183	38671	13782	-1.199	-1.418	861
6Q	10	21246	21409	18743	-1.471	-1.314	-1.460
7Q	11	11497	22471	24418	-1.468	-1.507	-1.442
8Q	12	26688	19085	25260	-1.558	-1.804	-1.574
9Q	13	18574	13613	20535	-1.753	-1.537	-1.339
ØR	14	22168	16693	32247	-1.638	-1.523	-1.502
1R	15	40526	6356	22384	-1.521	-1.877	-1.588
2R	16	28430	21562	19345	-1.475	-1.612	-1.500
3R	17	32435	17946	13584	-1.608	-1.459	-1.504
4R	18	20376	30150	28253	-1.789	-1.558	-1.504
5R	19	38121	39547	27965	-1.398	-1.540	-1.554
6R	20	20325	20060	193090	-1.671	-1.522	-1.848
7R	21	20096	1.8259	15393	-1.573	-1.389	-1.262
8R	22	25244	26062	25356	-1.574	-1.723	-1.430
9R	23	18162	23369	.8688	-1.745 .	-1.444	895
				UNPA	TTERNED	,	·
øs		60731	109598	· · · · · · · · · · · · · · · · · · ·		-1.882	-1.504
øs 1s	4 5	60731 109842	109598 104685	35488	-1.548	-1.882 252	-1.504 022
15	5	109842	104685	35488 34228	-1.548 -1.552	252	022
1S 2S	5 6	109842 152838	104685 95569	35488 34228 48903	-1.548 -1.552 -1.920	252 -1.007	022 -1.417
1S 2S 3S	5 6 7	109842 152838 181441	104685 95569 106528	35488 34228 48903 3041	-1.548 -1.552 -1.920 197	252 -1.007 -1.378	022 -1.417 419
1s 2s 3s 4s	5 6 7 8	109842 152838 181441 202574	104685 95569 106528 196239	35488 34228 48903 3041 68022	-1.548 -1.552 -1.920 197 535	252 -1.007 -1.378 -1.740	022 -1.417 419 -1.363
15 25 35 45 55	5 6 7 8 9	109842 152838 181441 202574 218527	104685 95569 106528 196239 200441	35488 34228 48903 3041 68022 64309	-1.548 -1.552 -1.920 197 535 729	252 -1.007 -1.378 -1.740 330	022 -1.417 419 -1.363 295
15 25 35 45 55 65	5 6 7 8 9	109842 152838 181441 202574 218527 249279	104685 95569 106528 196239 200441 225566	35488 34228 48903 3041 68022 64309 97167	-1.548 -1.552 -1.920 197 535 729 923	252 -1.007 -1.378 -1.740 330 818	022 -1.417 419 -1.363 295 -1.116
15 25 35 45 55 65 75	5 6 7 8 9 10	109842 152838 181441 202574 218527 249279 314018	104685 95569 106528 196239 200441 225566 290334	35488 34228 48903 3041 68022 64309 97167 89714	-1.548 -1.552 -1.920 197 535 729 923 -1.132	252 -1.007 -1.378 -1.740 330 818 -1.267	022 -1.417 419 -1.363 295 -1.116 -1.641
15 25 35 45 55 65 75 85	5 6 7 8 9 10 11 12	109842 152838 181441 202574 218527 249279 314018 287306	104685 95569 106528 196239 200441 225566 290334 186928	35488 34228 48903 3041 68022 64309 97167 89714 34126	-1.548 -1.552 -1.920 197 535 729 923 -1.132 -1.284	252 -1.007 -1.378 -1.740 330 818 -1.267 -1.720	022 -1.417 419 -1.363 295 -1.116 -1.641 207
15 25 35 45 55 65 75 85 95	5 6 7 8 9 10 11 12 13	109842 152838 181441 202574 218527 249279 314018 287306 308026	104685 95569 106528 196239 200441 225566 290334 186928 92638	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794	-1.548 -1.552 -1.920 197 535 729 923 -1.132 -1.284 -1.494	252 -1.007 -1.378 -1.740 330 818 -1.267 -1.720 279	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064
15 25 35 45 55 65 75 85 95	5 6 7 8 9 10 11 12 13 14	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312	-1.548 -1.552 -1.920 197 535 729 923 -1.132 -1.284 -1.494 -1.636	252 -1.007 -1.378 -1.740 330 818 -1.267 -1.720 279 717	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506
15 25 35 45 55 65 75 85 95	5 6 7 8 9 10 11 12 13	109842 152838 181441 202574 218527 249279 314018 287306 308026	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 26608	-1.548 -1.552 -1.920 197 535 729 923 -1.132 -1.284 -1.494 -1.636 -1.951	252 -1.007 -1.378 -1.740330818 -1.267 -1.720279717 -1.368	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064
15 25 35 45 55 65 75 85 95 11 21	5 6 7 8 9 10 11 12 13 14 15 16	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632 371256 384420	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347 78688	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 26608 27990	-1.548 -1.552 -1.920197535729923 -1.132 -1.284 -1.494 -1.636 -1.951158	252 -1.007 -1.378 -1.740330818 -1.267 -1.720279717 -1.368 -1.741	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506 -1.563 -1.544
15 25 35 45 55 65 75 85 95 17 27 37	5 6 7 8 9 10 11 12 13 14 15 16	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632 371256 384420 370070	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347 78688 77350	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 26608	-1.548 -1.552 -1.920197535729923 -1.132 -1.284 -1.494 -1.636 -1.951158352	252 -1.007 -1.378 -1.740 330 818 -1.267 -1.720 279 717 -1.368 -1.741 -1.957	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506 -1.563 -1.544 -1.843
15 25 35 45 55 65 75 85 95 71 17 27 47	5 6 7 8 9 10 11 12 13 14 15 16 17	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632 371256 384420 370070 382613	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347 78688 77350 36463	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 25608 27990 15872 23722	-1.548 -1.552 -1.920197535729923 -1.132 -1.284 -1.494 -1.636 -1.951158352659	252 -1.007 -1.378 -1.740330818 -1.267 -1.720279717 -1.368 -1.741 -1.957535	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506 -1.563 -1.544 -1.843 303
15 25 35 45 55 65 75 85 95 71 21 21 31 45 57	5 6 7 8 9 10 11 12 13 14 15 16 17	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632 371256 384420 370070 382613 311844	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347 78688 77350 36463 18376	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 25608 27990 15872 23722 35934	-1.548 -1.552 -1.920197535729923 -1.132 -1.284 -1.494 -1.636 -1.951158352659803	252 -1.007 -1.378 -1.740330818 -1.267 -1.720279717 -1.368 -1.741 -1.957535883	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506 -1.563 -1.544 -1.843 303 -1.062
15 25 35 45 55 65 75 85 95 11 21 31 47 51 67	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632 371256 384420 370070 382613 311844 312378	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347 78688 77350 36463 18376 24930	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 25608 27990 15872 23722 35934 388487	-1.548 -1.552 -1.920197535729923 -1.132 -1.284 -1.494 -1.636 -1.951158352659803950	252 -1.007 -1.378 -1.740330818 -1.267 -1.720279717 -1.368 -1.741 -1.957535883 -1.281	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506 -1.563 -1.544 -1.843 303 -1.062 920
15 25 35 45 55 65 75 85 95 71 21 21 31 45 57	5 6 7 8 9 10 11 12 13 14 15 16 17	109842 152838 181441 202574 218527 249279 314018 287306 308026 318632 371256 384420 370070 382613 311844	104685 95569 106528 196239 200441 225566 290334 186928 92638 96021 74347 78688 77350 36463 18376	35488 34228 48903 3041 68022 64309 97167 89714 34126 26794 27312 25608 27990 15872 23722 35934	-1.548 -1.552 -1.920197535729923 -1.132 -1.284 -1.494 -1.636 -1.951158352659803	252 -1.007 -1.378 -1.740330818 -1.267 -1.720279717 -1.368 -1.741 -1.957535883	022 -1.417 419 -1.363 295 -1.116 -1.641 207 -1.064 -1.506 -1.563 -1.544 -1.843 303 -1.062

THE THE PERSON STREET STREET STREET, S

23 22 21 20 19 18 17 16 15 14	121605 74372 86338 109907 78553 47520 67665	88165 67507 50425 6576 34019	f ₃ 61965 45006 20573 405425	-1.808 -1.538 -1.433	-1.410 -1.306 -1.202	-1.544 -1.479
22 21 20 19 18 17 16 15	74372 86338 109907 78553 47520 67665	67507 50425 6576 34019	45006 20573	-1.538 -1.433	-1.306	-1.479
21 20 19 18 17 16 15	86338 109907 78553 47520 67665	50425 6576 34019	20573	-1.433		
20 19 18 17 16 15	109907 78553 47520 67665	6576 3 4 019			-1.202	
19 18 17 16 15	78553 47520 67665	34019	405425		~ - ~ ~ ~	-1.98
19 18 17 16 15	47520 67665			-1.231	401	-1.12
17 16 15 14	67665	こつづに 4	11210	-1.026	-1.927	-1.43
17 16 15 14	67665	53754	37919	575	-1.856	-1.556
16 15 14		71862	55741	278	-1.704	-1.52
15 14	130481	86496	50534	211	-1.463	-1.378
14	112055	98973	25381	-1.959	-1.300	-1.40
	129864	42592	28578	-1.740	-1.119	-1.643
13	242350	52721	54340	-1.710	-1.059	-1.58
12	173534	30798	58426	-1.576	545	-1.43
11	233826	86380	17033	-1.410	014	-1.67
10	248554	110749	40999	-1.272	-1.732	-1.66
9	203555	144927	67590	-1.184	-1.372	-1.33
8	184184	115677	20642	950	-1.159	-1.21
7	149361	83451	42473	697	789	-1.90
					- 222	-1.56
						99
						06
·*	214070			-11/0/	-4.047	
			LARGE	CHECKS		
23	166586	43582	24764	885	-1.721	-1.669
						-1.589
						-1.60
						-1.34
						-1.17
						-1.25
						-1.68
						-1.51
						-1.,38
						-1.31
						-1.32
						-1.81
						-1.62
						-1.28
						84
						-1.76
						-1.52
						94
						-1.94
						-1.420
-	3.300	⊎ (\	1,107		4.000	
			A-11			
	23 22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7 6 5 4	6 192211 5 157800 4 114893 23 166586 22 169577 21 156963 20 141313 19 158213 18 166793 17 160073 16 187922 15 207314 14 152921 13 93879 12 71043 11 81952 10 91541 9 105715 8 109680 7 78408 6 105987 5 117210	6 192211 136093 5 157800 181954 4 114893 129500 23 166586 43582 22 169577 25652 21 156963 46918 20 141313 68111 19 158213 64647 18 166793 50124 17 160073 26632 16 187922 38319 15 207314 51223 14 152921 50587 13 93879 34590 12 71043 50176 11 81952 36605 10 91541 42326 9 105715 42219 8 109680 38757 7 78408 27233 6 105987 106361 5 117210 100664	6 192211 136093 89714 5 157800 181954 69997 4 114893 129500 21569 LARGE 23 166586 43582 24764 22 169577 25652 52170 21 156963 46918 40638 20 141313 68111 286687 19 158213 64647 23533 18 166793 50124 7772 17 160073 26632 34798 16 187922 38319 55595 15 207314 51223 40933 14 152921 50587 23543 13 93879 34590 16365 12 71043 50176 18056 11 81952 36605 65984 10 91541 42326 64613 9 105715 42219 43352 8 109680 38757 69845 7 78408 27233 75088 6 105987 106361 36866 5 117210 100664 33812	6 192211 136093 89714496 5 157800 181954 69997 -1.965 4 114893 129500 21569 -1.767 LARGE CHECKS 23 166586 43582 24764885 22 169577 25652 52170595 21 156963 46918 40638331 20 141313 68111 286687106 19 158213 64647 23533 -1.999 18 166793 50124 7772 -1.996 17 160073 26632 34798 -1.796 18 187922 38319 55595 -1.617 15 207314 51223 40933 -1.513 14 152921 50587 23543 -1.324 13 93879 34590 16365 -1.212 12 71043 50176 18056 -1.297 11 81952 36605 65984 -1.165 10 91541 42326 64613 -1.125 9 105715 42219 43352870 8 109680 38757 69845664 7 78408 27233 75088548 6 105987 106361 36866170 5 117210 100664 33812 -1.867 4 54506 87671 47401 -1.355	6 192211 136093 89714496222 5 157800 181954 69997 -1.965 -1.747 4 114893 129500 21569 -1.767 -1.324 LARGE CHECKS 23 166586 43582 24764885 -1.721 22 169577 25652 52170595 -1.773 21 156963 46918 40638331 -1.528 20 141313 68111 286687106 -1.479 19 158213 64647 23533 -1.999 -1.308 18 166793 50124 7772 -1.996 -1.145 17 160073 26632 34798 -1.796857 16 187922 38319 55595 -1.61.7079 15 207314 51223 40933 -1.513 -1.712 14 152921 50587 23543 -1.324 -1.500 13 93879 34590 16365 -1.212 -1.583 12 71043 50176 18056 -1.212 -1.583 12 71043 50176 18056 -1.297 -1.366 11 81952 36605 65984 -1.165 -1.445 10 91541 42326 64613 -1.125 -1.438 9 105715 42219 43352870 -1.422 8 109680 38757 69845664852 7 78408 27233 75088548200 6 105987 106361 36866170 -1.891 5 117210 100664 33812 -1.867 -1.414 4 54506 87671 47401 -1.355 -1.060

Date: 8-31-78 PATTERNED BACKGROUND - EYES OPEN

RM	Hz	fl	£2	f ₃	ø ₁	ø ₂	Ø3
øх	23	35530	40407	44913	-1.423	-1.501	-1.485
lX	22	46261	46807	43822	-1.445	-1.493	-1.476
2X	21	38015	42435	45956	-1.489	-1.505	-1.507
3X	20	35835	42081	54856	-1.397	-1.508	-1.262
4X	19	42246	42567	42906	-1.472	-1.495	-1.490
5X	18	50678	45969	45879	-1.501	-1.467	-1.497
6X	17	40787	37131	40785	-1.449	-1.515	-1.481
7X	16	40210	42511	41185	-1.615	-1.501	-1.511
8X	15	42217	39528	42160	-1.537	-1.491	-1.490
9X	14	44826	40870	40844	-1.506	-1.536	-1.488
ØZ	13	37361	28755	41523	-1.499	-1.469	-1.477
12	12	51981	40185	38896	-1.460	-1.496	-1.467
22	11	53210	40374	38499	-1.488	-1.490	-1.476
3 Z	10	35573	42772	38895	-1.555	-1.473	-1.490
4Z	9	28952	36549	35182	-1.618	-1.460	-1.479
5Z	8	45868	36067	40192	-1.437	-1.465	-1.437
62	7	45872	36790	29346	-1.417	-1.430	-1.417
7 Z	.6	34237	32511	35898	-1.423	-1.490	-1.450
^-		A 49 MM	37605	35369	-1.562	-1.390	-1.477
8Z	·5	64166	3/003	プラン()		-1	
8Z 9Z	· 5	59517	53610	52250	892	-1.488	-1.589
		59517	53610	52250		-1.488	
92	(59517	53610	52250	892 - EYES OP	-1.488	
9Z 	4	5951.7 UNP	53610 ATTERNED E 29371	52250 ACKGROUND	892	-1.488 EN -1.510	-1.451
9Z AA AB	4 5	59517 UNP. 34952	53610 ATTERNED F	52250 PACKGROUND 35525 62955	892 - EYES OP	-1.488 EN	-1.589
AA AB AC	4 5 6	59517 UNP. 34952 52894	53610 ATTERNED E 29371 43563 42253	52250 PACKGROUND 35525 62955 32008	892 - EYES OP -1.386 255	-1.488 EN -1.510 -1.660	-1.589 -1.451 -1.619
AA AB AC AD	4 5 6 7	34952 52894 29377 47929	53610 ATTERNED E 29371 43563 42253 38553	52250 ACKGROUND 35525 62955 32008 26630	892 - EYES OP -1.386 255 -1.785 -1.604	-1.488 -1.510 -1.660 -1.551 -1.451	-1.451 -1.619 -1.494 -1.551
AA AB AC AD AE	4 5 6	34952 52894 29377	53610 ATTERNED E 29371 43563 42253 38553 33693	52250 ACKGROUND 35525 62955 32008 26630 33325	892 - EYES OP -1.386 255 -1.785	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491	-1.589 -1.451 -1.619 -1.494
AA AB AC AD AE AF	4 5 6 7 8 9	34952 52894 29377 47929 32730 21148	53610 ATTERNED E 29371 43563 42253 38553	35525 62955 32008 26630 33325 29525	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.496	-1.451 -1.619 -1.494 -1.551 -1.465 -1.513
AA AB AC AD AE AF AG	4 5 6 7 8 9	34952 52894 29377 47929 32730 21148 36294	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194	35525 62955 32008 26630 33325 29525 31776	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.496 -1.471	-1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485
9Z AA AB AC AD AF AG AH	4 5 6 7 8 9	34952 52894 29377 47929 32730 21148	53610 ATTERNED E 29371 43563 42253 38553 33693 36955	35525 62955 32008 26630 33325 29525	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.496	-1.451 -1.619 -1.494 -1.551 -1.465 -1.513
AA AB AC AD AE AF AG AH AI	4 5 6 7 8 9 10 11 12	34952 52894 29377 47929 32730 21148 36294 19160 45726	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809	35525 62955 32008 26630 33325 29525 31776 30755 31470	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.496 -1.471 -1.476 -1.555	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.468 -1.497
9Z AA AB AC AD AF AG AH	4 5 6 7 8 9 10	34952 52894 29377 47929 32730 21148 36294 19160	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753	35525 62955 32008 26630 33325 29525 31776 30755	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.496 -1.471 -1.476	-1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468
AA AB AC AD AE AF AG AH AI AJ	4 5 6 7 8 9 10 11 12 13	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730	52250 ACKGROUND 35525 62955 32008 26630 33325 29525 31776 30755 31470 30862	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.476 -1.555 -1.498	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468 -1.497 -1.500
9Z AA AB AC AD AE AF AG AH AI AI AK AL	4 5 6 7 8 9 10 11 12 13 14	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086	52250 ACKGROUND 35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.476 -1.555 -1.478 -1.483	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468 -1.497 -1.500 -1.444
9Z AA AB AC AD AF AG AH AI AI AK	4 5 6 7 8 9 10 11 12 13 14 15	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985 35789	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086 27751	52250 35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444 30479 27403	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479 -1.561	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.476 -1.555 -1.478 -1.483 -1.482	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468 -1.497 -1.500 -1.444 -1.489
9Z AA AB AC AAE AF AC AH AI AK AM AN	4 5 6 7 8 9 10 11 12 13 14 15 16 17	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985 35789 22707	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086 27751 25518 26410	35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444 30479 27403 31580	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479 -1.561 -1.464 -1.499	-1.488 -1.510 -1.660 -1.551 -1.451 -1.496 -1.471 -1.476 -1.555 -1.498 -1.483 -1.482 -1.514 -1.471	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468 -1.497 -1.500 -1.444 -1.489 -1.499
9Z AA AB AC AC AH AI AN AN AN AO	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985 35789 22707 28260 21942	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086 27751 25518 26410 29884	35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444 30479 27403 31580 27102	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479 -1.561 -1.464 -1.499 -1.416	-1.488 -1.510 -1.660 -1.551 -1.451 -1.496 -1.471 -1.476 -1.555 -1.498 -1.483 -1.482 -1.514 -1.471 -1.469	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468 -1.497 -1.500 -1.444 -1.489 -1.459 -1.513
9Z AA AB AC AD AF AG AH AI AK AM AN AO AP	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985 35789 22707 28260 21942 34990	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086 27751 25518 26410 29884 28785	52250 35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444 30479 27403 31580 27102 28932	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479 -1.561 -1.464 -1.499 -1.416 -1.497	-1.488 -1.510 -1.660 -1.551 -1.451 -1.496 -1.471 -1.476 -1.555 -1.498 -1.483 -1.482 -1.514 -1.469 -1.506	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.468 -1.497 -1.500 -1.444 -1.489 -1.459 -1.513 -1.502
9Z AABACAAEAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985 35789 22707 28260 21942 34990 9711	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086 27751 25518 26410 29884 28785 30032	52250 35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444 30479 27403 31580 27102 28932 29007	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479 -1.561 -1.464 -1.499 -1.416 -1.497 -1.595	-1.488 -1.510 -1.660 -1.551 -1.451 -1.491 -1.476 -1.555 -1.488 -1.483 -1.482 -1.514 -1.469 -1.506 -1.490	-1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.485 -1.468 -1.497 -1.500 -1.444 -1.489 -1.459 -1.513 -1.502 -1.770
9Z AA AB AC AD AF AG AH AI AK AM AN AO AP	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	34952 52894 29377 47929 32730 21148 36294 19160 45726 19709 25985 35789 22707 28260 21942 34990	53610 ATTERNED E 29371 43563 42253 38553 33693 36955 35194 30753 32809 29730 31086 27751 25518 26410 29884 28785	52250 35525 62955 32008 26630 33325 29525 31776 30755 31470 30862 29444 30479 27403 31580 27102 28932	892 - EYES OP -1.386255 -1.785 -1.604 -1.484 -1.432 -1.633 -1.377 -1.550 -1.413 -1.479 -1.561 -1.464 -1.499 -1.416 -1.497	-1.488 -1.510 -1.660 -1.551 -1.451 -1.496 -1.471 -1.476 -1.555 -1.498 -1.483 -1.482 -1.514 -1.469 -1.506	-1.589 -1.451 -1.619 -1.494 -1.551 -1.465 -1.513 -1.468 -1.497 -1.500 -1.444 -1.489 -1.459 -1.513 -1.502

Date: 9-14-78

SMALL CHECKS

RM	Hz	f _l	£2	£3	ø ₁	ø ₂	ø ₃
DA	23	30134	103886	15331	168	395	-1.764
DB	22	58281	91688	37415	-1.721	-1.225	-1.425
∞	21	137194	96265	36880	-1.431	932	-1.941
DD	20	112960	21176	129387	-1.216	328	-1.059
DE DF	19 18	87534 94038	37076 90860	11088 53818	906	023 -1.729	525
DG	17	101472	71525	26370	637 495	-1.729 -1.803	-1.757 -1.704
DH	16	144799	86986	34329	107	-1.437	-1.575
DI	15	175756	72331	27099	303	-1.356	-1.190
Ŋ	14	236911	45324	13215	-1.917	-1.206	-1.188
DK	13	266368	26471	68465	-1.794	-1.220	-1.526
DL	12	24573.4	26694	55342	-1.580	463	-1.397
DM	11	256050	84806	13036	-1.403	-1.946	-1.506
DN	10	322668	103436	50314	-1.255	-1.604	-1.681
∞	9	236530	80196	63382	-1.059	-1.316	-1.468
ΣP	8	286747	100321	54313	892	-1.138	-1.028
DQ	7	182134 189751	108187 101149	51290 102525	729	~ .870	020
DR DS	6 5	147708	101149	56884	540 188	206 -1.717	-1.522 -1.123
DI	4.	133902	140296	48430	-1.780	-1.349	192
		20000	T 10234.	40400	2.00	-1.0.15	- 1452
		·		LARGE	CHECKS		
EA	4	89909	80535	LARGE 43579	CHECKS -1.570	968	-1.616
EB	5	121594	109368	43579 19141	-1.570 031	-1.414	-1.801
EB EC	5 6	121594 141195	109368 97176	43579 19141 45317	-1.570 031 258	-1.414 -1.704	-1.801 -1.189
	5 6 7	121594 141195 145586	109368 97176 31832	43579 19141 45317 55668	-1.570 031 258 412	-1.414 -1.704 -1.905	-1.801 -1.189 -1.456
888	5 6 7 8	121594 141195 145586 180448	109368 97176 31832 18711	43579 19141 45317 55668 36637	-1.570 031 258 412 614	-1.414 -1.704 -1.905 -1.726	-1.801 -1.189 -1.456 -1.713
贸易包围管	5 6 7 8 9	121594 141195 145586 180448 103228	109368 97176 31832 18711 55984	43579 19141 45317 55668 36637 7905	-1.570 031 258 412 614 684	-1.414 -1.704 -1.905 -1.726 -1.542	-1.801 -1.189 -1.456 -1.713 704
出品品品品品	5 6 7 8 9	121594 141195 145586 180448 103228 122625	109368 97176 31832 18711 55984 46725	43579 19141 45317 55668 36637 7905 70088	-1.570 031 258 412 614 684 927	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432	-1.801 -1.189 -1.456 -1.713 704 -1.381
贸易员国营贸图	5 6 7 8 9 1	121594 141195 145586 180448 103228 122625 153007	109368 97176 31832 18711 55984 46725 36747	43579 19141 45317 55668 36637 7905 70088 76597	-1.570 031 258 412 614 684 927 -1.042	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704
图各色角色器出出	5 6 7 8 9 1 11 12	121594 141195 145586 180448 103228 122625 153007 94012	109368 97176 31832 18711 55984 46725 36747 29974	43579 19141 45317 55668 36637 7905 70088 76597 32978	-1.570 031 258 412 614 684 927 -1.042 -1.152	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818
日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日	5 6 7 8 9 1 11 12 13	121594 141195 145586 180448 103228 122625 153007 94012 141957	109368 97176 31832 18711 55984 46725 36747 29974 45370	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094	-1.570 031 258 412 614 684 927 -1.042 -1.152 -1.083	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.380
图各色角色器出出	5 6 7 8 9 1 11 12	121594 141195 145586 180448 103228 122625 153007 94012	109368 97176 31832 18711 55984 46725 36747 29974	43579 19141 45317 55668 36637 7905 70088 76597 32978	-1.570 031 258 412 614 684 927 -1.042 -1.152	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818
异巴耳耳耳耳 目号	5 6 7 8 9 1 11 12 13 14	121594 141195 145586 180448 103228 122625 153007 94012 41957	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864	-1.570 031 258 412 614 684 927 -1.042 -1.152 -1.083 -1.304	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.380 -1.531
足叉甲甲甲甲异异异甲甲甲甲	5 6 7 8 9 1 11 12 13 14 15 16 17	121594 141195 145586 180448 103228 122625 153007 94012 41957 110433 244416 226250 250121	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357 33482 36366 52817	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864 50824 15915 11390	-1.570 031 258 412 614 684 927 -1.042 -1.152 -1.083 -1.304 -1.507 -1.628 -1.732	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744 -1.891 333 -1.026	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.380 -1.531 -1.565 -1.596 -1.181
罗里里里里里里里里里里	5 6 7 8 9 1 11 12 13 14 15 16 17 18	121594 141195 145586 180448 103228 122625 153007 94012 41957 110433 244416 226250 250121 207702	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357 33482 36366 52817 69148	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864 50824 15915 11390 15061	-1.570 031 258 412 614 684 927 -1.042 -1.152 -1.083 -1.304 -1.507 -1.628 -1.732 -1.932	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744 -1.891 333 -1.026 -1.177	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.565 -1.596 -1.181 -1.889
用皮里里用用用用用用用用	5 6 7 8 9 1 11 12 13 14 15 16 17 18 19	121594 141195 145586 180448 103228 122625 153007 94012 41957 :10433 244416 226250 250121 207702 205080	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357 33482 36366 52817 69148 81425	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864 50824 15915 11390 15061 55861	-1.570031258412614684927 -1.042 -1.152 -1.083 -1.304 -1.507 -1.628 -1.732 -1.932074	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744 -1.891 333 -1.026 -1.177 -1.446	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.531 -1.565 -1.596 -1.181 -1.889 -1.030
日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日	5 6 7 8 9 1 12 13 14 15 16 17 18 19 20	121594 141195 145586 180448 103228 122625 153007 94012 41957 10433 244416 226250 250121 207702 205080 174884	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357 33482 36366 52817 69148 81425 47570	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864 50824 15915 11390 15061 55861 132157	-1.570031258412614684927 -1.042 -1.152 -1.083 -1.304 -1.507 -1.628 -1.732 -1.932074333	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744 -1.891 333 -1.026 -1.177 -1.446 -1.512	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.380 -1.531 -1.565 -1.596 -1.181 -1.889 -1.030 -1.093
男男母母母母母母母母母母母母母母母	5 6 7 8 9 1 11 12 13 14 15 16 17 18 19 20 21	121594 141195 145586 180448 103228 122625 153007 94012 41957 10433 244416 226250 250121 207702 205080 174884 143664	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357 33482 36366 52817 69148 81425 47570 49404	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864 50824 15915 11390 15061 55861 132157 19286	-1.570031258412614684927 -1.042 -1.152 -1.083 -1.304 -1.507 -1.628 -1.732 -1.932074333470	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744 -1.891 333 -1.026 -1.177 -1.446 -1.512 -1.784	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.380 -1.531 -1.565 -1.596 -1.181 -1.889 -1.030 -1.030 -1.093 -1.706
日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日日	5 6 7 8 9 1 12 13 14 15 16 17 18 19 20	121594 141195 145586 180448 103228 122625 153007 94012 41957 10433 244416 226250 250121 207702 205080 174884	109368 97176 31832 18711 55984 46725 36747 29974 45370 74357 33482 36366 52817 69148 81425 47570	43579 19141 45317 55668 36637 7905 70088 76597 32978 35094 43864 50824 15915 11390 15061 55861 132157	-1.570031258412614684927 -1.042 -1.152 -1.083 -1.304 -1.507 -1.628 -1.732 -1.932074333	-1.414 -1.704 -1.905 -1.726 -1.542 -1.432 -1.498 -1.765 -1.262 -1.744 -1.891 333 -1.026 -1.177 -1.446 -1.512	-1.801 -1.189 -1.456 -1.713 704 -1.381 -1.704 -1.818 -1.380 -1.531 -1.565 -1.596 -1.181 -1.889 -1.030 -1.093

Date: 9-14-78

RM	Hz	£1	f ₂	f ₃	ø ₁	ø ₂	ø ₃
FA	4	122575	144727	55657	-1.427	-1.914	-1.404
FB	5	158618	114089	2 1226	-1.649	477	157
FC	6	208357	94381	73769	-1.881	-1.055	-1.521
FD	7	244780	116685	18773	213	-1.349	793
FE	8	283733	246805	118101	500	-1.767	-1.566
FF	9	350083	338773	113002	717	404	445
FG	10	413025	362998	155729	86 9	953	-1.237
FH	11	498239	367107	103402	-1.108	-1.449	-1.77.9
FI	12	500809	228243	12652	-1.353	-1.918	-1.902
FU	13	570219	127126	10645	-1.577	477	-1.374
FK	14	556212	121545	32754	-1.813	-1.020	-1.306
FL	15	502330	108417	52048	091	-1.485	-1.394
FM	16	412415	50601	55844	363	-1.731	-1.630
FN	17	332988	28141	36477	575	-1.723	-1.494
FO	18	415005	25592	33649	743	-1.256	-1.414
FP	19	387773	41634	29119	966	-1.430	-1.368
FQ	20	273755	26867	38160	-1.221	-1.120	-1.025
FR	21 .	362347	39399	17893	-1.273	894	-1.540
FS	22	340031	59648	58516	-1.439	-1.034	-1.565
FT	23	313637	106679	42155	-1.534	-1.248	-1.568

Date: 5-31-78

LP	Hz	fl	\mathtt{f}_2	f ₃	\emptyset_1	\emptyset_2	ø ₃
ЕØ	4	37234	24206	32494	-1.041	-1.609	-1.578
E1	5	47534	10500	26747	744	-1.443	-1.385
E2	6 7	139245	35804	31396	-1.139	047	-1.236
E3		93444	14499	29558	-1.351	-1.003	-1.608
E4	8	101167	41004	17661	-1.570	973	-1.491
.75	9	128282	65333	12921	-1.879	-1.281	-1.684
E6	10	143257	41974	21322	-1.907	-1.615	-1.349 .
E7	11	114161	39952	11280	392	022	-1.413
E8	12	115733	27450	13182	402	-1.143	-1.357
E9	13	187374	11864	16139	630	-1.117	-1.762
FØ	14	56364	23088	14105	604	-1.542	-1.541
F1	15	139396	11866	15525	869	234	-1.386
F2	16	167895	4905	18409	-1.261	-1.581	-1.552
F3	17	232804	19337	15280	-1.576	-1.484	1.443
F4	18	258061	12860	22720	-1.718	-1.716	-1.638
F5	19	137577	54625	58691	-1.935	-1.527	-1.588
F6	20	229668	16905	73863	019	-1.683	-1.631
F7	21	129302	18883	2449	513	-1.488	-1.837
F8	22	122944	16978	13761	498	-1.445	-1.847
F9	23	136294	14997	7538	748	-1.404	-1.014
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-,,				SMALL	CHECKS		
	4	45707	11219			-1.535	-1.718
GØ G1	4 5	45707 47273	11219 31154	10893	-1.343	-1.535 -1.768	-1.718 -1.732
Gl	5	47273	31154	10893 12013	-1.343 -1.641	-1.768	-1.732
G1 G2	5 6	47273 79605	31154 6694	10893 12013 11032	-1.343 -1.641 -1.916	-1.768 -1.424	-1.732 -1.336
G1 G2 G3	5 6 7	47273 79605 71173	31154 6694 12871	10893 12013 11032 12160	-1.343 -1.641 -1.916 093	-1.768 -1.424 -1.523	-1.732 -1.336 -1.256
G1 G2 G3 G4	5 6 7 8	47273 79605 71173 38888	31154 6694 12871 6340	10893 12013 11032 12160 10470	-1.343 -1.641 -1.916 093 409	-1.768 -1.424 -1.523 -1.487	-1.732 -1.336 -1.256 -1.538
G1 G2 G3 G4 G5	5 6 7 8 9	47273 79605 71173 38888 24046	31154 6694 12871 6340 5825	10893 12013 11032 12160 10470 20532	-1.343 -1.641 -1.916 093 409 305	-1.768 -1.424 -1.523 -1.487 426	-1.732 -1.336 -1.256 -1.538 -1.254
G1 G2 G3 G4 G5 G6	5 6 7 8 9 10	47273 79605 71173 38888 24046 11773	31154 6694 12871 6340 5825 18163	10893 12013 11032 12160 10470 20532 11919	-1.343 -1.641 -1.916 093 409 305 971	-1.768 -1.424 -1.523 -1.487 426 276	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503
G1 G2 G3 G4 G5 G6	5 6 7 8 9 10 11	47273 79605 71173 38888 24046 11773 87984	31154 6694 12871 6340 5825	10893 12013 11032 12160 10470 20532 11919 11144	-1.343 -1.641 -1.916 093 409 305 971 -1.485	-1.768 -1.424 -1.523 -1.487 426 276 -1.735	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639
G1 G2 G3 G4 G5 G6 G7 G8	5 6 7 8 9 10	47273 79605 71173 38888 24046 11773 87984 47391	31154 6694 12871 6340 5825 18163 36425	10893 12013 11032 12160 10470 20532 11919 11144 21461	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603	-1.768 -1.424 -1.523 -1.487 426 276 -1.735 -1.150	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503
G1 G2 G3 G4 G5 G6 G7 G8 G9	5 6 7 8 9 10 11 12 13	47273 79605 71173 38888 24046 11773 87984 47391 24979	31154 6694 12871 6340 5825 18163 36425 48425 10840	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752	-1.343 -1.641 -1.916 093 409 305 971 -1.485	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600
G1 G2 G3 G5 G6 G7 G8 G9	5 6 7 8 9 10 11 12 13	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656
G1 G2 G3 G4 G5 G6 G7 G8 G9 HM	5 6 7 8 9 10 11 12 13 14 15	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623	-1.768 -1.424 -1.523 -1.487 426 276 -1.735 -1.150 -1.223 -1.616 -1.118	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334
G1 G2 G3 G5 G6 G7 G8 G9	5 6 7 8 9 10 11 12 13	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656
G1 G2 G3 G5 G6 G7 G8 G9 H1 H1 H2 H3	5 6 7 8 9 10 11 12 13 14 15 16 17	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491 7445 19744	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193 15057 30650	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449 15441 29853	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623 069 -1.407	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547 -1.436	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334 -1.496 -1.521
G1 G2 G3 G4 G5 G6 G7 G8 G9 H1 H1	5 6 7 8 9 10 11 12 13 14 15 16 17 18	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491 7445 19744 21299	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193 15057 30650 29254	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449 15441 29853 39739	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623 069 -1.407 893	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547 -1.436 -1.586	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334 -1.496 -1.521 -1.380
G1 G2 G3 G5 G6 G7 G8 G9 H1 H2 H3 H4	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491 7445 19744 21299 20747	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193 15057 30650 29254 16017	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449 15441 29853 39739 65644	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623 069 -1.407 893 -1.282	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547 -1.436 -1.586 -1.542	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334 -1.496 -1.521 -1.380 -1.315
G1 G2 G3 G5 G6 G7 G8 G9 H1 H1 H4 H5	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491 7445 19744 21299	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193 15057 30650 29254	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449 15441 29853 39739 65644 84642	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623 069 -1.407 893 -1.282 -1.606	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547 -1.436 -1.586 -1.542 -1.429	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334 -1.496 -1.521 -1.380 -1.315 -1.714
G1 G2 G3 G5 G6 G7 G9 H1 H2 H4 H5 H6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491 7445 19744 21299 20747 35132	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193 15057 30650 29254 16017 29711	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449 15441 29853 39739 65644	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623 069 -1.407 893 -1.282 -1.606 -1.425	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547 -1.436 -1.586 -1.586 -1.542 -1.429 -1.471	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334 -1.496 -1.521 -1.380 -1.315
G1 G2 G3 G4 G5 G6 G7 G8 G9 H1 H12 H4 H4 H4 H6 H7	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	47273 79605 71173 38888 24046 11773 87984 47391 24979 20579 30491 7445 19744 21299 20747 35132 38380	31154 6694 12871 6340 5825 18163 36425 48425 10840 13243 16193 15057 30650 29254 16017 29711 47409	10893 12013 11032 12160 10470 20532 11919 11144 21461 18752 28279 6449 15441 29853 39739 65644 84642 30371	-1.343 -1.641 -1.916 093 409 305 971 -1.485 -1.603 046 -1.797 -1.623 069 -1.407 893 -1.282 -1.606	-1.768 -1.424 -1.523 -1.487426276 -1.735 -1.150 -1.223 -1.616 -1.118 -1.547 -1.436 -1.586 -1.542 -1.429	-1.732 -1.336 -1.256 -1.538 -1.254 -1.503 -1.639 -1.109 -1.600 -1.656 -1.334 -1.496 -1.521 -1.380 -1.315 -1.714 -1.26

Date: 6-12-78

LP	Hz	fl	f ₂	f ₃	Ø ₁	ø ₂	ø ₃
JØ	4	103899	62015	68259	-1.614	-1.711	-1.549
Jl	5 6	99524	28836	50410	-1.806	-1.930	-1.322
J2	6	145320	59873	39693	042	476	557
J3	7	116313	2006 9 6	76434	443	-1.134	-1.346
J4	8	178903	25 9 0^	5 744 0	714	-1.762	-1.815
J5	9	232748	30265	46732	-1.021	392	898
J6	10	308225	242585	75570	-1.110	973	-1.481
J7	11	300509	181419	23484	-1.331	-1.440	-1.925
J8	12	441313	85210	56482	-1.467	-1.862	-1.252
J9	13	£16151	26863	· 87831	-1.647	695	-1.495
ΚØ	14	589101	93283	39621	-1.926	-1.262	-1.593
Kl.	15	544584	89181	37470	229	-1.562	-1.488
K2	16	497985	16899	59849	464	-1.633	-1.362
K3	17	500802	37496	57726	745	-1.304	-1.535
K4	18	487886	66551	36408	-1.020	-1.409	838
K5	19	474365	32849	35534	-1.263	-1.651	401
K6	20	433545	53490	235584	-1.436	-1.441	930
K7	21	340261	34112	135495	-1.591	-1.291	-1.440
K8	22	295135	78265	48976	-1.751	-1.475	-1.350
К9	23	227940	73295	46767	-1.893	-1.608	-1.586
				UNIPA	TTERNED		
LØ	24	137409	53491	72993	022	-1.599	-1.550
ĽĴ.	25	114132	26675	48798	263	-1.928	-1.284
1.2	26	82446	93815	74040	513	982	-1.682
L3	27	92344	60530	49560	776	-1.499	-1.355
L4	28	107635	59664	54446	-1.035	-1.084	-1.616
1.5	29	97273	83696	52778	-1.217	-1.588	-1.488
L6	30	100030	798429	54690	-1.348	-1.573	-1.455
L7	31	120094	50932	41785	-1.543	-1.064	-1.575
L8	32	74932	108493	47749	-1.483	-1.362	-1.453
L9	33	80431	96866	7)348	-1.571	-1.674	-1.580
MØ	34	80168	73893	5 / 151	-1.622	-1.460	-1.397
M1	35	48802	40497	58414	-1.787	-1.329	-1.583
M2	36	126853	193087	43582	-1.333	147	-1.925
M3	37	33268	75407	65150	-1.188	-1.732	-1.677
M4	38	25328	38278	18047	-1.283	-1.833	-1.616
M5	39	44617	45289	29598	-1.243	-1.450	-1.361
M6	40	64935	50472	142953	-1.468	-1.498	-1.213
M7	41	77217	31050	13112	-1.425	-1.150	-1.340
M8	42	63925	50108	63540	-1.197	-1.749	-1.545
M9	43	33584	47979	55933	-1.550	-1.339	-1.547
בניו	7.0	3033.		30,00	1.00	2.000	4.01,

Date: 6-12-78

LP	Hz	f ₁	f ₂	£3	Ø ₁	ø ₂	ø ₃
NØ	4	151778	81985	50643	-1.845	-1.559	-1.584
N1		89558	101109	46230	571	-1.675	-1.381
N2	5 6 7 8	187651	79797	45776	808	-1.965	-1.790
ИЗ	7	201114	23304	90090	-1.136	319	-1.346
N4	8	264734	143049	53131	-1.311	998	-1.725
N5	9	194238	227457	38574	-1.503	-1.377	-1.185
N6	10	183392	247927	65030	-1.601	-1.791	-1.305
N7	11	202294	120888	72699	-1.893	235	-1.614
N8	12	56532	73889	45398	~1.982	754	-1.263
00 00	13 14	81410 33823	103421 97476	51832 33607	319 646	-1.142 -1.487	-1.513
01	15	56512	69339	36368	886 886	-1.487 -1.627	-1.643 -1.336
02	16	161797	49723	45681	-1.154	-1.710	-1.475
03	17	86292	17967	46021	-1.393	-1.321	-1.510
04	18	183217	36188	24617	-1.538	-1.435	-1.382
05	19	182883	65952	70791	-1.800	-1.516	-1.581
06	20	212479	55698	56238	138	-1.653	-1.500
07	21	171474	20715	82706	400	-1.764	-1.532
08	22	117725	41871	59552	624	-1.107	-1.554
09	23	167965	37748	62813	906	-1.321	-1.534
	····			LARGE	CHECKS		
PØ	4	318615	43806			-1.472	-1.329
PØ P1	4 5	318615 199316	43806 110133	LARGE 44892 33398	-1.853 -1.903	-1.472 -1.346	-1.329 -1.238
	5			44892	-1.853	-1.472 -1.346 013	
P1	5 6 7	199316 264345 229858	110133 93822 71376	44892 33398 56188 79355	-1.853 -1.903	-1.346	-1.238
P1 P2 P3 P4	5 6 7 8	199316 264345 229858 219557	110133 93822 71376 105345	44892 33398 56188 79355 20115	-1.853 -1.903 654 946 -1.174	-1.346 013 430 968	-1.238 954 -1.674 -1.818
P1 P2 P3 P4 P5	5 6 7 8 9	199316 264345 229858 219557 199429	110133 93822 71376 105345 145291	44892 33398 56188 79355 20115 35066	-1.853 -1.903 654 946 -1.174 -1.401	-1.346 013 430 968 -1.292	-1.238 954 -1.674 -1.818 -1.209
P1 P2 P3 P4 P5 P6	5 6 7 8 9	199316 264345 229858 219557 199429 195556	110133 93822 71376 105345 145291 128810	44892 33398 56188 79355 20115 35066 55017	-1.853 -1.903 654 946 -1.174 -1.401 -1.538	-1.346 013 430 968 -1.292 -1.604	-1.238 954 -1.674 -1.818 -1.209 -1.393
P1 P2 P3 P4 P5 P6 P7	5 6 7 8 9 10	199316 264345 229858 219557 199429 195556 171287	110133 93822 71376 105345 145291 128810 57240	44892 33398 56188 79355 20115 35066 55017 51076	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676	-1.346 013 430 968 -1.292 -1.604 -1.894	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564
P1 P2 P3 P4 P5 P6 P7 P8	5 6 7 8 9 10 11 12	199316 264345 229858 219557 199429 195556 171287 149360	110133 93822 71376 105345 145291 128810 57240 7988	44892 33398 56188 79355 20115 35060 55017 51076 34000	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738
P1 P2 P3 P4 P5 P6 P7 P8 P9	5 6 7 8 9 10 11 12 13	199316 264345 229858 219557 199429 195556 171287 149360 93657	110133 93822 71376 105345 145291 128810 57240 7988 48966	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329
P1 P2 P3 P4 P5 P6 P7 P8 P9 QØ	5 6 7 8 9 10 11 12 13	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269 623	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481
P1 P2 P3 P4 P5 P6 P7 P8 P9 Q1	5 6 7 8 9 10 11 12 13 14	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269 623 968	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370 -1.520	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531
P1 P2 P3 P4 P5 P6 P7 P8 P9 Q1 Q1 Q2	5 6 7 8 9 10 11 12 13 14 15 16	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121 144587	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873 31413	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834 34401	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269 623 968 -1.279	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370 -1.520 -1.525	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531 -1.579
P1 P2 P3 P4 P5 P6 P7 P8 P9 Q1 Q3	5 6 7 8 9 10 11 12 13 14	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269 623 968	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370 -1.520	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531
P1 P2 P3 P4 P5 P6 P7 P8 P9 Q1 Q1 Q2	5 6 7 8 9 10 11 12 13 14 15 16 17	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121 144587 154078	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873 31413 1878	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834 34401 21956	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269 623 968 -1.279 -1.522	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370 -1.520 -1.525 -1.508	-1.238 954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531 -1.579 -1.458
P1 P3 P4 P5 P6 P7 P8 P9 Q1 Q3 Q4	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121 144587 154078 114189	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873 31413 1878 46350 70891 74437	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834 34401 21956 37536	-1.853 -1.903 654 946 -1.174 -1.401 -1.538 -1.676 -1.909 269 623 968 -1.279 -1.522 -1.757	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370 -1.520 -1.525 -1.508 -1.243	-1.238954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531 -1.579 -1.458 -1.462
P1 P2 P3 P4 P5 P6 P7 P8 P9 Q1 Q2 Q3 Q4 Q5 Q7	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121 144587 154078 114189 50967 24674 9923	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873 31413 1878 46350 70891 74437 62899	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834 34401 21956 37536 56602 80718 56928	-1.853 -1.903654946 -1.174 -1.401 -1.538 -1.676 -1.909269623968 -1.279 -1.522 -1.757 -1.966083083358	-1.346 013 430 968 -1.292 -1.604 -1.802 -1.260 -1.370 -1.520 -1.525 -1.508 -1.5243 -1.419 -1.503 -1.731	-1.238954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531 -1.579 -1.458 -1.635 -1.635 -1.695 -1.632
P1 P2 P3 P4 P5 P6 P7 P8 P9 Q1 Q2 Q3 Q4 Q5 Q6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	199316 264345 229858 219557 199429 195556 171287 149360 93657 94710 116121 144587 154078 114189 50967 24674	110133 93822 71376 105345 145291 128810 57240 7988 48966 59895 57873 31413 1878 46350 70891 74437	44892 33398 56188 79355 20115 35066 55017 51076 34000 40850 53268 56834 34401 21956 37536 56602 80718	-1.853 -1.903654946 -1.174 -1.401 -1.538 -1.676 -1.909269623968 -1.279 -1.522 -1.757 -1.966083	-1.346 013 430 968 -1.292 -1.604 -1.894 -1.802 -1.260 -1.370 -1.520 -1.525 -1.508 -1.5243 -1.419 -1.503	-1.238954 -1.674 -1.818 -1.209 -1.393 -1.564 -1.738 -1.329 -1.481 -1.531 -1.579 -1.458 -1.462 -1.635 -1.695

Date: 6-26-78

LP	Hz	fl	f ₂	f ₃	ø _l	ø ₂	ø ₃
RØ	23	180437	116557	75773,	-1.724	-1.595	-1.572
R1	22	246468	118193	74242	-1.624	-1.555	-1.499
R2	21	365911	97121	111846	-1.522	-1.519	-1.452
R3 R4	20 19	442635 589839	70245 66340	102652 20538	-1.418 -1.186	-1.390 -1.121	883 -1.279
R5	18	576764	56689	32615	874	-1.402	-1.336
R6	17	662617	110921	174380	530	-1.692	-1.514
R7	16	710518	155174	35344	248	-1.590	-1.207
R8	15	637977	155321	32314	-1.913	-1.220	-1.881
R9	14	523643	35812	140217	-1.758	522	-1.609
sø	13	500817	121853	117849	-1.554	-1.929	-1.342
sl	12	283986	202657	27306	-1.490	-1.698	-1.327
S2	11	356226	268238	83566	-1.375	-1.335	-1.715
S3	70	439948	289099	130388	-1.247	942	-1.448
S4 S5	9 8	415400 284829	323836 371480	95945 82226	-1.082 764	373 -1.786	890 -1.808
55 56	7	172602	303563	136702	499	-1.78 -1.178	-1.227
57	6	161813	89114	71317	210	497	375
58	5	129517	43631	33691	-1.770	141	883
59	4	93609	62773	123924	-1.690	-1.841	-1.677
				UNPAT	TERNED		
TØ	4	135698	73817	UNPAT	TERNED -1.704	1.794	-1.573
Tl	5	106774	52706	112565 24443	-1.704 -1.820	-1.834	-1.016
Tl T2	5 6	106774 146397	52706 131001	112565 24443 73864	-1.704 -1.820 193	-1.834 572	-1.016 387
T1 T2 T3	5 6 7	106774 146397 149874	52706 131001 228198	112565 24443 73864 127499	-1.704 -1.820 193 476	-1.834 572 -1.210	-1.016 387 -1.381
T1 T2 T3 T4	5 6 7 8	106774 146397 149874 280083	52706 131001 228198 354536	112565 24443 73864 127499 87908	-1.704 -1.820 193 476 786	-1.834 572 -1.210 -1.775	-1.016 387 -1.381 -1.856
T1 T2 T3 T4 T5	5 6 7 8 9	106774 146397 149874 280083 365460	52706 131001 228198 354536 325557	112565 24443 73864 127499 87908 82164	-1.704 -1.820 193 476 786 -1.133	-1.834 572 -1.210 -1.775 330	-1.016 387 -1.381 -1.856 920
T1 T2 T3 T4 T5 T6	5 6 7 8 9	106774 146397 149874 280083 365460 377182	52706 131001 228198 354536 325557 278570	112565 24443 73864 127499 87908 82164 97772	-1.704 -1.820 193 476 786 -1.133 -1.262	-1.834 572 -1.210 -1.775 330 944	-1.016 387 -1.381 -1.856 920 -1.474
T1 T2 T3 T4 T5 T6	5 6 7 8 9 10	106774 146397 149874 280083 365460 377182 263522	52706 131001 228198 354536 325557 278570 242680	112565 24443 73864 127499 87908 82164 97772 48054	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288	-1.834 572 -1.210 -1.775 330 944 -1.376	-1.016 387 -1.381 -1.856 920 -1.474 -1.662
T1 T2 T3 T4 T5 T6	5 6 7 8 9	106774 146397 149874 280083 365460 377182	52706 131001 228198 354536 325557 278570	112565 24443 73864 127499 87908 82164 97772	-1.704 -1.820 193 476 786 -1.133 -1.262	-1.834 572 -1.210 -1.775 330 944	-1.016 387 -1.381 -1.856 920 -1.474
T1 T2 T3 T4 T5 T6 T7	5 6 7 8 9 10 11 12	106774 146397 149874 280083 365460 377182 263522 263522	52706 131001 228198 354536 325557 278570 242680 207900	112565 24443 73864 127499 87908 82164 97772 48054 17033	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783	-1.016 387 -1.381 -1.856 920 -1.474 -1.662 -1.040
T1 T2 T3 T4 T5 T6 T7 T8	5 6 7 8 9 10 11 12 13 14 15	106774 146397 149874 280083 365460 377182 263522 292257 346434	52706 131001 228198 354536 325557 278570 242680 207900 91049	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113	-1.016 387 -1.381 -1.856 920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865
T1 T2 T3 T4 T5 T6 T7 T8 T9 U1 U1 U2	5 6 7 8 9 10 11 12 13 14 15 16	106774 146397 149874 280083 365460 377182 263522 292257 346434 577728 718403 739840	52706 131001 228198 354536 325557 278570 242680 207900 91049 104133 140381 122369	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729	-1.016 387 -1.381 -1.856 920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281
T1 T2 T3 T4 T5 T6 T7 T8 T9 W1 U2 U3	5 6 7 8 9 10 11 12 13 14 15 16 17	106774 146397 149874 280083 365460 377182 263522 292257 346434 577728 718403 739840 677723	52706 131001 228198 354536 325557 278570 242680 207900 91049 104133 140381 122369 36252	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144 78059	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314 599	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729 363	-1.016 387 -1.381 -1.856 920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281 -1.490
T1 T2 T3 T4 T5 T6 T7 T8 T9 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1	5 6 7 8 9 10 11 12 13 14 15 16 17 18	106774 146397 149874 280083 365460 377182 263522 292257 346434 577728 718403 739840 677723 633971	52706 131001 228198 354536 325557 278570 242680 207900 91049 1041.33 140381 122369 36252 75230	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144 78059 43119	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314 599 828	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729 363 975	-1.016387 -1.381 -1.856920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281 -1.490 -1.513
T1 T2 T3 T4 T5 T6 T7 T8 T9 UU UU UU UU UU UU UU UU	5 6 7 8 9 10 11 12 13 14 15 16 17 18	106774 146397 149874 280083 365460 377182 263522 297257 346434 577728 718403 739840 677723 633971 644516	52706 131001 228198 354536 325557 278570 242680 207900 91049 104133 140381 122369 36252 75230 50067	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144 78059 43119 39126	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314 599 828 -1.154	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729 363 975 -1.315	-1.016 387 -1.381 -1.856 920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281 -1.490 -1.513 838
T1 T2 T4 T5 T6 T7 T7 T7 T9 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1 U1	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	106774 146397 149874 280083 365460 377182 26352 26352 263	52706 131001 228198 354536 325557 278570 242680 207900 91049 104133 140381 122369 36252 75230 50067 59823	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144 78059 43119 39126 152512	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314 599 828 -1.154 -1.402	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729 363 975 -1.315 -1.344	-1.016387 -1.381 -1.856920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281 -1.490 -1.513838789
T1 T2 T4 T5 T6 T7 T7 T9 W U U U U U U U U U U U U U U U U U U	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	106774 146397 149874 280083 365460 377182 263522 263522 267257 346434 577728 718403 739840 677723 633971 644516 552930 455723	52706 131001 228198 354536 325557 278570 242680 207900 91049 104133 140381 122369 36252 75230 50067 59823 80056	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144 78059 43119 39126 152512 48301	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314 599 828 -1.154 -1.402 -1.548	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729 363 975 -1.315 -1.344 -1.451	-1.016387 -1.381 -1.856920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281 -1.490 -1.513838789 -1.552
T1 T2 T3 T4 T5 T6 T7 T8 T9 U1 U2 U3 U5 U5 U6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	106774 146397 149874 280083 365460 377182 26352 26352 263	52706 131001 228198 354536 325557 278570 242680 207900 91049 104133 140381 122369 36252 75230 50067 59823	112565 24443 73864 127499 87908 82164 97772 48054 17033 84779 75649 41167 48144 78059 43119 39126 152512	-1.704 -1.820 193 476 786 -1.133 -1.262 -1.288 -1.533 -1.554 -1.803 086 314 599 828 -1.154 -1.402	-1.834 572 -1.210 -1.775 330 944 -1.376 -1.783 113 -1.083 -1.429 -1.729 363 975 -1.315 -1.344	-1.016387 -1.381 -1.856920 -1.474 -1.662 -1.040 -1.346 -1.754 -1.865 -1.281 -1.490 -1.513838789

Date: 8-1-78

LARGE CHECKS

LP	Hz	f ₁	f ₂	f ₃	Ø ₁	ø ₂	ø ₃
			<u> </u>	· 		<u></u>	
VØ	4	128522	73487	46143	-1.698	-1.368	-1.390
Vl	5	55933	115402	62949	240	-1.560	-1.438
V2	6	72484	90263	58791	789	-1.786	-1.233
V3	7	131379	22420	88244	-1.076	425	-1.572
V4	8	154241	85038	55464	-1.269	-1.162	-1.534
V 5	9	151265	116182	45609	-1.392	-1.401	-1.391
V6	10	157825	102956	56413	-1.476	-1.717	-1.443
V 7	11	146678	41034	60926	-1.654	-1.739	-1.533
v 8	12	127949	27099	36484	-1.942	-1.461	-1.519
V9	13	92958	41311	15691	085	-1.404	-1.627
11154	14	69370	64533	61427	523	-1.517	-1.564
W1	15	107495	57918	52623	944	-1.491	-1.577
W2	16	131602	54729	57651	-1.215	-1.614	-1.544
W3	17	140166	34311	44142	-1.387	-1.313	-1.627
W4	18	89403	45640	41793	-1.711	-1.432	-1.444
W5	19	48931	76826	81115	-1.776	-1.524	-1.529
W6	20	23491	49 209	227070	-1.637	-1.498	-1.628
W7	21	13545	24915	79910	-1.388	-1.504	-1.568
w8	22	52254	21790	54627	-1.437	-1.637	-1.505
W9	23	59281	26244	57387	-1.131	-1.177	-1.488
				LARGE	CEECKS		
xoó	4	126582	73557			-1.478	-1.410
xø xl	4 5	126582 60094	73557 108163	42777	-1.866	-1.478 -1.492	-1.410 -1.445
XI	5	60094	108163	42777 60813	-1.866 297	-1.492	-1.445
				42777	-1.866		
X1 X2	5 6 7	60094 143667	108163 67314	42777 60813 47385	-1.866 297 720	-1.492 -1.902	-1.445 -1.262
XI X2 X3	5 6	60094 143667 168651	108163 67314 27336	42777 60813 47385 54122	-1.866 297 720 -1.005	-1.492 -1.902 597	-1.445 -1.262 -1.601
X1. X2 X3 X4	5 6 7 8	60094 143667 168651 269520	108163 67314 27336 107076	42777 60813 47385 54122 47055	-1.866 297 720 -1.005 -1.232	-1.492 -1.902 597 -1.039	-1.445 -1.262 -1.601 -1.542
X1. X2 X3 X4 X5	5 6 7 8 9 10	60094 143667 168651 269520 155522	108163 67314 27336 107076 103228	42777 60813 47385 54122 47055 43768	-1.866 297 720 -1.005 -1.232 -1.416	-1.492 -1.902 597 -1.039 -1.474	-1.445 -1.262 -1.601 -1.542 -1.444
X1. X2 X3 X4 X5 X6	5 6 7 8 9	60094 143667 168651 269520 155522 143034	108163 67314 27336 107076 103228 81480	42777 60813 47385 54122 47055 43768 47446	-1.866 297 720 -1.005 -1.232 -1.416 -1.532	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459
X1 X2 X3 X4 X5 X6 X7	5 6 7 8 9 10	60094 143667 168651 269520 155522 143034 183980	108163 67314 27336 107076 103228 81480 17730	42777 60813 47385 54122 47055 43768 47446 53783	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532
X1 X2 X3 X4 X5 X6 X7 X8	5 6 7 8 9 10 11 12 13	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879	42777 60813 47385 54122 47055 43768 47446 53783 45438	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y0 Y1	5 6 7 8 9 10 11 12 13	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2	5 6 7 8 9 10 11 12 13 14 15 16	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091 46577 40449 48017	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553 904 -1.146	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3	5 6 7 8 9 10 11 12 13 14 15 16 17	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410 98670	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876 41422	42777 60813 47385 54122 47055 43768 47446 53785 45438 42091 46577 40449 48017 34786	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553 904 -1.146 -1.307	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594 -1.505	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532 -1.510
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3 Y4	5 6 7 8 9 10 11 12 13 14 15 16 17 18	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410 98670 94984	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876 41422 40940	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091 46577 40449 48017 34786 34338	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553 904 -1.146 -1.307 -1.566	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594 -1.505 -1.409	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532 -1.510 -1.381
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3 Y4 Y5	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410 98670 94984 78743	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876 41422 40940 66748	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091 46577 40449 48017 34786 34338 73280	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553 904 -1.146 -1.307 -1.566 -1.503	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594 -1.505 -1.409 -1.456	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532 -1.510 -1.381 -1.557
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3 Y4 Y5 Y6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410 98670 94984 78743 53314	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876 41422 40940 66748 58644	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091 46577 40449 48017 34786 34338 73280 197036	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553 904 -1.146 -1.307 -1.566 -1.503 -1.528	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594 -1.505 -1.409 -1.456 -1.614	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532 -1.510 -1.381 -1.557 -1.897
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3 Y4 Y5 Y6 Y7	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410 98670 94984 78743 53314 55658	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876 41422 40940 66748 58644 43085	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091 46577 40449 48017 34786 34338 73280 197036 62664	-1.866297720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925203553904 -1.146 -1.307 -1.566 -1.503 -1.528 -1.700	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594 -1.505 -1.409 -1.456 -1.614 -1.605	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532 -1.510 -1.381 -1.557 -1.897 -1.448
X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3 Y4 Y5 Y6	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	60094 143667 168651 269520 155522 143034 183980 133683 96194 79432 73131 101410 98670 94984 78743 53314	108163 67314 27336 107076 103228 81480 17730 29130 55535 52879 49828 49876 41422 40940 66748 58644	42777 60813 47385 54122 47055 43768 47446 53783 45438 42091 46577 40449 48017 34786 34338 73280 197036	-1.866 297 720 -1.005 -1.232 -1.416 -1.532 -1.694 -1.925 203 553 904 -1.146 -1.307 -1.566 -1.503 -1.528	-1.492 -1.902 597 -1.039 -1.474 -1.709 -1.846 -1.328 -1.357 -1.508 -1.500 -1.594 -1.505 -1.409 -1.456 -1.614	-1.445 -1.262 -1.601 -1.542 -1.444 -1.459 -1.532 -1.560 -1.421 -1.507 -1.485 -1.532 -1.510 -1.381 -1.557 -1.897

Date: 8-1-78

SMALL CHECKS

LP	Hz	fl	f ₂	£3	ø ₁	ø ₂	ø ₃
zø	4	1605'18	122315	62512	100	-1.575	-1.618
zl	5	187952	108138	41213	505	-1.604	-1.376
Z 2	6	241883	74778	98215	851	-1.924	-1.483
Z 3	7	306190	34440	71710	-1.107	568	-1.508
Z4	8	261844	123762	45325	-1.347	-1.118	-1.624
Z 5	9	218484	230825	61630	-1.579	-1.398	-1.366
z 6	10	176169	203916	79056	-1.727	-1.782	-1.557
z 7	11	137748	101525	47289	-1.822	176	-1.635
z 8	12	44562	73293	63151	028	874	-1.399
Z 9	13	44851	106733	65420	-1.887	-1.278	-1.495
ØA	14	30245	117341	47373	-1.425	-1.501	-1.626
1A	15	21457	71024	38248	-1.161	-1.633	-1.466
2A	16	36638	16499	60278	-1.062	-1.917	-1.429
3A	17	90720	49095	71903	-1.291	-1.537	-1.463
4A	18	135500	64945	44299	-1.415	-1.453	-1.448
5A	19	149543	79699	57005	-1.574	-1.532	-1.581
6A	20	127243	55700	179424	-1.980	-1.711	-1.401
7A	21	61736	29483	88913	204	-1.481	-1.434
8A	22	52354	60247	68139	753	-1.342	-1.497
9A	23	52993	76853	66016	995	-1.387	-1.492

Date: 8-9-78

LP	Hz	fl	f ₂	f ₃	\emptyset_1	\emptyset_2	ø ₃
ØB	23	238408	54003	50648	-1.107	-1.509	-1.494
18	22	158957	42242	43049	839	-1.346	-1.423
2B	21	145383	13540	69204	477	-1.518	-1.511
3B	20	159966	35110	444352	250	-1.312	659
4B	19	196834	500 99	15668	-1.935	-1.558	-1.657
5B	18	149843	49774	68923	-1.604	-1.373	-1.410
6B	17	174522	25303	31699	-1.305	-1.634	-1.59 9
7B	16	74589	28260	53694	-1.091	-1.559	-1.495
8 B	15	32122	40142	34974	859	-1.746	-1.254
9B	14	16389	91591	34184	401	-1.597	-1.812
ØC	13	39969	102842	52138	230	-1.256	-1.571
lC	12	56918	83834	40885	-1.936	889	-1.287
2C	11	124971	74265	14185	-1.805	328	-1.614
3C	10	183478	152366	53418	-1.712	-1.894	-1. 505
4C	9	220817	200288	60125	-1.563	-1.459	-1.300
5C	8	231905	173112	8778	-1.325	-1.090	-1.478
6C	7	217144	81191	43105	-1.104	609	-1.588
7C	6	241760	56881	69088	830	102	-1.652
8C	5	255947	98665	47164	479	-1.766	-1.083
9C	4	179257	84776	29697	115	-1.549	-1.908
				SMALI	CHECKS		
<u></u>		170904	92466	· · · · · · · · · · · · · · · · · · ·		1 570	7 023
80 10	4	179896	82466 53330	23239	163	-1.572	-1.931
מנ	5	177372	53329	23239 38228	163 485	-1.771	-1.144
1D 2D	5 6	177372 224 7 62	53329 72617	23239 38228 58000	163 485 848	-1.771 078	-1.144 -1.871
1D 2D 3D	5 6 7	177372 224762 220365	53329 72617 74472	23239 38228 58000 42910	163 485 848 -1.094	-1.771 078 637	-1.144 -1.871 -1.446
1D 2D 3D 4D	5 6 7 8	177372 224762 220365 195047	53329 72617 74472 146080	23239 38228 58000 42910 29757	163 485 848 -1.094 -1.358	-1.771 078 637 -1.069	-1.144 -1.871 -1.446 016
1D 2D 3D 4D 5D	5 6 7 8 9	177372 224762 220365 195047 194372	53329 72617 74472 146080 203940	23239 38228 58000 42910 29757 44565	163 485 848 -1.094 -1.358 -1.483	-1.771 078 637 -1.069 -1.480	-1.144 -1.871 -1.446 016 -1.186
1D 2D 3D 4D 5D 6D	5 6 7 8 9 10	177372 224762 220365 195047 194372 162154	53329 72617 74472 146080 203940 141041	23239 38228 58000 42910 29757 44565 39192	163 485 848 -1.094 -1.358 -1.483 -1.695	-1.771 078 637 -1.069 -1.480 -1.928	-1.144 -1.871 -1.446 016 -1.186 -1.542
19 29 39 49 50 60 70	5 6 7 8 9 10	177372 224762 220365 195047 194372 162154 105322	53329 72617 74472 146080 203940 141041 73525	23239 38228 58000 42910 29757 44565 39192 13839	163 485 848 -1.094 -1.358 -1.483 -1.695 -1.815	-1.771 078 637 -1.069 -1.480 -1.928 375	-1.144 -1.871 -1.446 016 -1.186 -1.542 -1.833
11 21 31 41 51 61 70 80	5 6 7 8 9 10 11 12	177372 224762 220365 195047 194372 162154 105322 76411	53329 72617 74472 146080 203940 141041 73525 82245	23239 38228 58000 42910 29757 44565 39192 13839 33482	163 485 848 -1.094 -1.358 -1.483 -1.695 -1.815 -1.955	-1.771 078 637 -1.069 -1.480 -1.928 375 868	-1.144 -1.871 -1.446 016 -1.186 -1.542 -1.833 -1.267
120000000000000000000000000000000000000	5 6 7 8 9 10 11 12 13	177372 224762 220365 195047 194372 162154 105322 76411 56991	53329 72617 74472 146080 203940 141041 73525 82245 86320	23239 38228 58000 42910 29757 44565 39192 13839 33482 35778	163 485 848 -1.094 -1.358 -1.483 -1.695 -1.815 -1.955 270	-1.771 078 637 -1.069 -1.480 -1.928 375 868 -1.260	-1.144 -1.871 -1.446 016 -1.186 -1.542 -1.833 -1.267 -1.504
19995566895	5 6 7 8 9 10 11 12 13 14	177372 224762 220365 195047 194372 162154 105322 76411 56991 67189	53329 72617 74472 146080 203940 141041 73525 82245 86320 70286	23239 38228 58000 42910 29757 44565 39192 13839 33482 35778 23485	163 485 848 -1.094 -1.358 -1.483 -1.695 -1.815 -1.955 270 690	-1.771 078 637 -1.069 -1.480 -1.928 375 868 -1.260 -1.545	-1.144 -1.871 -1.446 016 -1.186 -1.542 -1.833 -1.267 -1.504 -1.713
120000000000000000000000000000000000000	5 6 7 8 9 10 11 12 13 14 15	177372 224762 220365 195047 194372 162154 105322 76411 56991 67189 64924	53329 72617 74472 146080 203940 141041 73525 82245 86320 70286 50130	23239 38228 58000 42910 29757 44565 39192 13839 33482 35778 23485 37793	163485848 -1.094 -1.358 -1.483 -1.695 -1.815 -1.955270690867	-1.771 078 637 -1.069 -1.480 -1.928 375 868 -1.260 -1.545 -1.833	-1.144 -1.871 -1.446 016 -1.186 -1.542 -1.833 -1.267 -1.504 -1.713 -1.280
122222222222222222222222222222222222222	5 6 7 8 9 10 11 12 13 14 15 16	177372 224762 220365 195047 194372 162154 105322 76411 56991 67189 64924 120672	53329 72617 74472 146080 203940 141041 73525 82245 86320 70286 50130 23648	23239 38228 58000 42910 29757 44565 39192 13839 33482 35778 23485 37793 47191	163 485 848 -1.094 -1.358 -1.483 -1.695 -1.815 -1.955 270 690 867 -1.151	-1.771 078 637 -1.069 -1.480 -1.928 375 868 -1.260 -1.545 -1.833 -1.757	-1.144 -1.871 -1.446 016 -1.186 -1.542 -1.833 -1.267 -1.504 -1.713 -1.280 -1.503
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Date: 8-18-78

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Date: 9-1-78 PATTERNED BACKGROUND - EYES OPEN

IN 5 21842 29744 26517 -1.338 -1.389 -1.58 2N 6 18826 14282 30476 -1.525 -1.413 -1.51 3N 7 28128 24902 21541 -1.565 -1.276 -1.41 4N 8 44377 23810 27785 -1.456 -1.409 -1.49 5N 9 44671 21307 27394 -1.585 -1.270 -1.43 6N 10 45640 21582 23199 -1.622 -1.509 -1.54 7N 11 8112 19523 17218684 -1.503 -1.54 8N 12 10987 20112 17348 -1.446 -1.551 -1.43 9N 13 28360 18559 16932 -1.547 -1.413 -1.47 6O 14 24704 24442 15136 -1.292 -1.435 -1.39 10 15 18138 21975 16257 -1.819 -1.506 -1.47 20 16 13263 16926 15289 -1.899 -1.544 -1.56 30 17 5627 19189 13453 -1.774 -1.400 -1.44 40 18 18699 16203 19592 -1.011 -1.517 -1.41 50 19 50139 43888 35021 -1.488 -1.599 -1.65 60 20 9382 7506 36761143 -1.227 -1.69 60 20 9382 7506 36761143 -1.227 -1.69 70 21 25561 21429 14917 -1.259 -1.465 -1.44 90 23 18537 17831 16178 -1.509 -1.442 -1.46 Date: 9-4-78 UNPAITERNED BACKGROUND - EYES OPEN	IN 5 21842 29744 26517 -1.338 -1.389 -1.587 ZN 6 18826 14282 30476 -1.525 -1.413 -1.514 3N 7 28128 24902 21541 -1.565 -1.276 -1.413 4N 8 44377 23810 27785 -1.456 -1.409 -1.493 5N 9 44671 21307 27394 -1.585 -1.270 -1.438 6N 10 45640 21582 23199 -1.622 -1.509 -1.549 7N 11 8112 19523 17218684 -1.503 -1.546 8N 12 10987 20112 17348 -1.446 -1.551 -1.430 9N 13 28360 18559 16932 -1.547 -1.413 -1.477 6O 14 24704 24442 15136 -1.292 -1.394 10 15 18138 21975 16257 -1.819 -1.506 -1.475 20 16 13263 16926 15289 -1.899 -1.544 -1.540 30 17 5627 19189 13453 -1.774 -1.400 -1.403 40 18 18699 16203 19592 -1.011 -1.517 -1.416 50 19 50139 43888 35021 -1.488 -1.599 -1.657 60 20 9382 7506 36761143 -1.227 -1.691 70 21 25561 21429 14917 -1.259 -1.465 -1.448 80 22 19591 16836 15015 -1.387 -1.469 -1.482 90 23 18537 17831 16178 -1.509 -1.442 -1.401 Date: 9-4-78 UNPATTERNED BACKGROUND - EYES OPEN
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7P 11 51175 33461 39727 -1.511 -1.576 -1.4 8P 12 44910 35471 37814 -1.488 -1.408 -1.5 9P 13 47632 37703 39438 -1.497 -1.477 -1.49	7P 11 51175 33461 39727 -1.511 -1.576 -1.479 8P 12 44910 35471 37814 -1.488 -1.408 -1.522 9P 13 47632 37703 39438 -1.497 -1.477 -1.494 ØQ 14 39673 39773 38755 -1.441 -1.448 -1.448 1Q 15 46434 46531 39185 -1.425 -1.474 -1.478 2Q 16 24484 36595 36915 -1.537 -1.445 -1.469
8P 12 44910 35471 37814 -1.488 -1.408 -1.55	8P 12 44910 35471 37814 -1.488 -1.408 -1.522 9P 13 47632 37703 39438 -1.497 -1.477 -1.494 ØQ 14 39673 39773 38755 -1.441 -1.448 -1.448 1Q 15 46434 46531 39185 -1.425 -1.474 -1.478 2Q 16 24484 36595 36915 -1.537 -1.445 -1.469
op 13 47632 37703 39438 -1.497 -1.477 -1.49	9P 13 47632 37703 39438 -1.497 -1.477 -1.494 ØQ 14 39673 39773 38755 -1.441 -1.448 -1.448 1Q 15 46434 46531 39185 -1.425 -1.474 -1.478 2Q 16 24484 36595 36915 -1.537 -1.445 -1.469
3E TO 41007 01100 01100 11101 11101	ØQ 14 39673 39773 38755 -1.441 -1.448 -1.448 1Q 15 46434 46531 39185 -1.425 -1.474 -1.478 2Q 16 24484 36595 36915 -1.537 -1.445 -1.469
go 14 39673 39773 38755 -1.441 -1.448 -1.4	1Q 15 46434 46531 39185 -1.425 -1.474 -1.478 2Q 16 24484 36595 36915 -1.537 -1.445 -1.469
10 15 46434 46531 39185 -1.425 -1.474 -1.4	20 16 24484 36595 36915 -1.537 -1.445 -1.469
20 16 24484 36595 36915 -1.537 -1.445 -1.4	
30 17 44916 41108 38002 -1.413 -1.475 -1.4	3Q 17 44916 41108 38002 -1.413 -1.475 -1.469
40 18 45890 33519 31787 -1.585 -1.501 -1.5	40 18 45890 33519 31787 -1.585 -1.501 -1.507
50 19 40188 38835 35202 -1.514 -1.535 -1.4	5Q 19 40188 38835 35202 -1.514 -1.535 -1.482
6Q 20 35735 32166 23838 -1.549 -1.468 -1.5	6Q 20 35735 32166 23838 -1.549 -1.468 -1.506
7Q 21 25109 34437 34889 -1.527 -1.481 -1.5	7Q 21 25109 34437 34889 -1.527 -1.481 -1.512
80 22 43418 33952 34714 -1.476 -1.524 -1.4	80 22 43418 33952 34714 -1.476 -1.524 -1.494
90 23 27823 37994 34132 -1.481 -1.503 -1.4	00 00 00000 00004 04100 1 491 1 500 1 493

Date: 9-1-78

LARGE CHECKS

LP	Hz	fl	f ₂	f ₃	ø _l	ø ₂	ø ₃
ØJ	4	162978	94126	63066	-1.878	-1.407	-1.413
'n	5 6	111098	150838	51926	380	-1.571	-1.515
2.7	6	151383	85581	85422	778	~1.939	-1.330
37	7	197860	36144	67233	-1.070	799 -1.231	-1.658 -1.551
45	8	213252	105370	44086 57729	-1.309 -1.474	-1.231 -1.491	-1.408
5 <u>.</u>	9	186884	116343	63074	-1.4/4 -1.667	-1.743	-1.503
6J	10	185161 161500	97910 22215	55562	-1.816	-1.579	-1.533
7ゴ &J	11 12	117383	57346	57060	067	-1.244	-1.376
9J	13	74559	68051	59423	407	-1.385	-1.416
ØK	14	91527	60754	59268	820	-1.487	-1.512
1K	15	129461	57681	52702	-1.128	-1.553	-1.528
2K	16	157388	56318	52212	-1.370	-1.583	-1.524
3K	17	135709	49479	55038	-1.557	-1.461	-1.492
4K	18	117647	61529	56796	-1.676	-1.447	-1.467
5K	19	49684	69578	55069	-1.912	-1.528	-1.501
6K	20	31061	62105	45475	-1.999	-1.609	-1.408
7K	21	28353	39138	56864	-1.140	-1.525	-1.483
8K	22	36251	45105	52196	-1264	-1.494	-1.499
9K	23	71590	54337	54766	-1.382	-1.427	-1.475
				LARGE	CHECKS	,	
			·····				4 40
ΩT.	23	61950	51449	55523	- 1,391	-1.433	-1.490
ØL 11.	23 22	61950 53266	51449 43363	55523 53844	-1.391 -1.260	-1.433 -1.462	-1.490 -1.487
ÌL.	22	53266	43363	55523 53844 54895	-1.391 -1.260 -1.245		
1L 2L	22 21	53266 18482		53844	-1.260	-1.462	-1.487 -1.475 -1.508
1L 2L 3L	22 21 20	53266	43363 40338	53844 54895	-1.260 -1.245	-1.462 -1.533 -1.574 -1.544	-1.487 -1.475 -1.508 -1.501
1L 2L 3L 4L	22 21	53266 18482 9651	43363 40338 52100	53844 54895 51667	-1.260 -1.245 -1.737 -1.827 -1.680	-1.462 -1.533 -1.574 -1.544 -1.352	-1.487 -1.475 -1.508 -1.501 -1.426
1L 2L 3L	22 21 20 19	53266 18482 9651 41323	43363 40338 52100 64858	53844 54895 51667 51526 54985 53022	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477
1L 2L 3L 4L 5L	22 21 20 19 18	53266 18482 9651 41323 75462	43363 40338 52100 64858 72082 53847 42008	53844 54895 51667 51526 54985 53022 47252	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484
1L 2L 3L 4L 5L 6L	22 21 20 19 18 17 16	53266 18482 9651 41323 75462 102438 132105 106487	43363 40338 52100 64858 72082 53847 42008 53991	53844 54895 51667 51526 54985 53022 47252 46802	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531
1L 2L 3L 4L 5L 6L 7L	22 21 20 19 18 17 16 15	53266 18482 9651 41323 75462 102438 132105 106487 84158	43363 40338 52100 64858 72082 53847 42008 53991 63187	53844 54895 51667 51526 54985 53022 47252 46802 55778	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501
11 21 31 41 51 61 7 81 9 M	22 21 20 19 18 17 16 15 14	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.415	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488
1L 3L 4L 5L 6L 7L 8L 9L 9M 1M	22 21 20 19 18 17 16 15 14 13	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.415 -1.284	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462
11. 31. 41. 51. 61. 78. 81. 91. 91. 21.	22 21 20 19 18 17 16 15 14 13 12	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.415 -1.284 -1.624	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523
11.21.21.21.21.21.21.21.21.21.21.21.21.2	22 21 20 19 18 17 16 15 14 13 12 11	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193 182516	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758 84297	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749 57872	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808 -1.673	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.415 -1.284 -1.624 -1.796	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523 -1.547
11 21 21 21 21 21 21 21 21 21 21 21 21 2	22 21 20 19 18 17 16 15 14 13 12 11 10 9	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193 182516 211468	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758 84297 105444	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749 57872 57931	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808 -1.673 -1.484	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.415 -1.284 -1.624 -1.796 -1.536	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523 -1.547 -1.458
H 21 34 45 66 76 86 96 M 25 M 2	22 21 20 19 18 17 16 15 14 13 12 11 10 9	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193 182516 211468 250183	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758 84297 105444 116856	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749 57872 57931 35894	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808 -1.673 -1.484 -1.277	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.541 -1.545 -1.284 -1.624 -1.796 -1.536 -1.250	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523 -1.547 -1.458 -1.404
H 21 24 51 61 7 81 81 81 81 81 81 81 81 81 81 81 81 81	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193 182516 211468 250183 181550	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758 84297 105444 116856 42592	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749 57872 57931 35894 51038	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808 -1.673 -1.484 -1.277 987	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.541 -1.545 -1.284 -1.624 -1.796 -1.536 -1.250 697	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523 -1.547 -1.458 -1.404 -1.701
11 21 31 41 51 61 7 81 1 8 1 M M M M M M M M M M M M M M M	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7 6	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193 182516 211468 250183 181550 209918	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758 84297 105444 116856 42592 76556	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749 57872 57931 35894 51038 53876	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808 -1.673 -1.484 -1.277 987 752	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.415 -1.284 -1.624 -1.796 -1.536 -1.250 697 181	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523 -1.547 -1.458 -1.404 -1.701 -1.301
H 21 24 51 61 7 81 81 81 81 81 81 81 81 81 81 81 81 81	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8	53266 18482 9651 41323 75462 102438 132105 106487 84158 74252 102236 172193 182516 211468 250183 181550	43363 40338 52100 64858 72082 53847 42008 53991 63187 63275 39718 17758 84297 105444 116856 42592	53844 54895 51667 51526 54985 53022 47252 46802 55778 53997 46363 49749 57872 57931 35894 51038	-1.260 -1.245 -1.737 -1.827 -1.680 -1.559 -1.408 -1.149 915 390 133 -1.808 -1.673 -1.484 -1.277 987	-1.462 -1.533 -1.574 -1.544 -1.352 -1.421 -1.461 -1.534 -1.541 -1.541 -1.545 -1.284 -1.624 -1.796 -1.536 -1.250 697	-1.487 -1.475 -1.508 -1.501 -1.426 -1.477 -1.484 -1.531 -1.501 -1.488 -1.462 -1.523 -1.547 -1.458 -1.404 -1.701

Date: 5-10-78

RR	Hz	fl	\mathtt{f}_2	f ₃	ϕ_1	ø ₂	\emptyset_3
GØ.	23	40353	45224	38846	-1.532	-1.559	-1.454
G1.	22	53229	57867	26426	-1.539	-1.540	-1.415
G2	21	28633	65429	26254	-1.542	-1.481	-1.321
G3	20	30957	46461	104848	-1.372	-1.351	-1.866
G4	19	48317	47440	162875	-1.520	-1.571	-1.668
G 5	18	18549	44177	55980	-1.549	-1.489	-1.571
G6	17	68605	36878	38605	-1.374	-1.532	-1.492
G7	16	108810	27854	39082	-1.233	-1.509	-1.501
Ç8	15	39098	49383	44538	-1.219	-1.563	-1.471
G9	14	37246	43592	41806	-1.724	-1.418	-1.501
HQ'	13	66639	49414	46104	-1.871	-1.460	-1.519
Hl	12	31012	55083	47044	-1.628	-1.537	-1.486
H2	11	88001	61286	56207	-1.590	-1.510	-1.509
нз	10	87955	55154	47063	-1.543	-1.511	-1.522
H4	9	65322	53073	45501	-1.486	-1.388	-1.437
H5	8 7	61558	62748	36407	-1.378	-1.433	-1.521
H6		37873	13162	29929	-1.475	-1.676	-1.376
H7	6	39425	35262	31386	-1.441	-1.643	-1.542
н8	5	30582	38037	40467	-1.300	-1.533	-1.521
H9	4	19312	40000	39287	-1.537	-1.343	-1.478
							
				SMALL	CHECKS		
IØ	23	24814	47430	41315	-1.405	-1.620	-1.177
T1	22	63156	42649	3667	-1.557	-1.440	-1.940
12	21	27103	46972	176318	-1.642	-1.607	-1.009
I3	20	21771	47571	294259	-1.593	-1.473	359
I4	19	51931	63740	219247	-1.544	-1.601	-1.721
I5	18	15702	39469	44073	-1.476	-1.519	-1.844
16	17	21094	31018	20235	-1.374	-1.716	-1.480
I7	16	37940	27441	33984	-1.535	-1.519	-1.495
18	15	25069	38778	38586	-1.434	-1.468	-1.576
19	14	24671	19785	37219	-1.703	-1.597	-1.494
JØ	13	29556	32682	40928	-1.523	-1.619	-1.641
J1	12	29903	36789	29525	-1.551	-1.475	-1.488
J2	11	59619	35872	42468	-1.553	-1.407	-1.517
J3	10	56884	26423	38102	-1.413	-1.551	-1.489
J4	9	23794	42632	48841	-1.602	-1.575	-1.579
J5	8	34887	36220	32240	-1.377	-1.493	-1.452
J6	7	26475	20737	19614	-1.510	-1.553	-1.439
<i>3</i> 7	6	38352	40617	41110	-1.409	-1.399	-1.483
J8	5	24174	28165	35636	-1.349	-1.341	-1.508
J9	4	32273	39787	25014	-1.401	-1.392	-1.488

Date: 5-10-78

LARGE CHECKS

RR	HZ	£1	f ₂	£3	\emptyset_1	ø ₂	ø ₃
KØ	23	22951	59167	96114	-1.622	-1.849	-1.041
K1	22	31425	44629	4682	-1.501	-1.381	415
K2	21	24212	43721	249919	-1.859	-1.706	-1.005
кз	20	36298	23553	403078	-1. J	-1.557	379
K4	19	38063	48827	209955	-1.510	-1.590	-1.748
K5	18	34134	28105	74963	-1.668	-1.634	-1.954
K6	17	24623	38863	18939	-1.211	-1.568	-1.864
K7	16	39066	30575	38745	-1.370	-1.495	-1.471
к8	15	28877	32894	35612	-1.638	-1.373	-1.430
К9	14	38535	20947	30913	-1.769	-1.619	-1.578
LØ	13	36820	37086	40344	-1.554	-1.546	-1.546
LĹ	12	19669	33888	27524	-1.625	-1.354	-1.466
L2	11	97750	38718	35225	-1.522	-1.559	-1.539
ĽЗ	10	49780	48231	22298	-1.388	-1.622	-1.419
L4	9	20075	32244	35658	-1.299	-1.484	-1.501
L5	8	42041	26330	42267	143	-1.391	-1.511
L6	7	22769	26879	21544	-1.633	-1.492	-1.631
L7	6	35478	28739	35399	-1.554	-1.412	-1.443
L8	5	24450	²²⁰⁶⁶	21467	-1.389	-1.220	-1,535
L9	4	15433	24037	16662	-1.509	-1.482	-1.421

Date: 6-19-78

LARGE CHECKS

							
RR	Hz	fl	f ₂	f ₃	\emptyset_{1}	ø ₂	ø ₃
							W
MØ	23	78453	91202	77040	-1.428	-1.369	-1.508
ML	22	77965	57201	87622	-1.348	-1.435	-1.530
M2	21	57102	44059	122516	-1.378	-1.594	-1.462
MB	20	58933	58562	217116	-1.378	-1.625	-1.872
M4	19	53493	95151	86130	-1. 5 (a)	-1561	-1.635
M5	18	27938	61445	67795	-1.823	472	-1.538
M5	17	78564	53379	69834	-1.673	-1.486	-1.444
M7	16	81688	50096	31250	-1.575	-1.495	-1.394
M8	15	109892	49721	27821	-1.310	-1.369	-1.662
M9	14	67346	35384	36685	926	-1.374	-1.504
NO	13	55131	16651	37534	792	992	-1.437
NT	12	67873	21836	29587	393	232	-1.458
N2	11	115177	53822	31395	088	-1.855	-1.524
ΝЗ	10	114797	74393	22485	-1.749	-1.599	-1.650
N4	9 8	140733	64652	15812	-1.677	~1.284	-1.418
N5	8	188202	40027	49530	-1.464	-1.113	-1.663
N6	7	137190	26620	63669	-1.222	-1.602	-1.417
N7	6 5 4	30529	20936	23570	611	402	517
М8	5	45709	66739	53830	-1.119	132	-1.640
N9	4	84085	73063	48753	-1.125	-1.506	838
				SMAT.T.	CHECKS		
				SMALL	CHECKS		
00/	23	47216	14295			864	-1.581
01	23 22	47216 58590	14295 14303	23573	-1.567 -1.375	864 -1.787	-1.581 -1.681
00° 01 02	23 22 21		14295 14303 10066		-1.567		-1.581 -1.681 -1.423
01	22	58590	14303	23573 17599	-1.567 -1.375	-1.787	-1.681
01 02	22 21 20 19	58590 31683	14303 10066	23573 17599 47441	-1.567 -1.375 908	-1.787 546	-1.681 -1.423
01 02 03 04 05	22 21 20 19 18	58590 31683 34444 27299 31344	14303 10066 16070 26410 13133	23573 17599 47441 191788 36679 4263	-1.567 -1.375 908 962 923 -1.949	-1.787 546 -1.562 -1.466 -1.512	-1.681 -1.423 -1.411
01 02 03 04 05 06	22 21 20 19 18 17	58590 31683 34444 27299 31344 35299	14303 10066 16070 26410 13133 30466	23573 17599 47441 191788 36679 4263 13153	-1.567 -1.375 908 962 923 -1.949 257	-1.787 546 -1.562 -1.466 -1.512 -1.758	-1.681 -1.423 -1.411 -1.439 278 -1.608
01 02 03 04 05 06 07	22 21 20 19 18 17 16	58590 31683 34444 27299 31344 35299 46685	14303 10066 16070 26410 13133 30466 17317	23573 17599 47441 191788 36679 4263 13153 21949	-1.567 -1.375 908 962 923 -1.949 257 -1.488	-1.787 546 -1.562 -1.466 -1.512 -1.758 -1.388	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534
01 02 03 04 05 06 07 08	22 21 20 19 18 17 16 15	58590 31683 34444 27299 31344 35299 46685 73105	14303 10066 16070 26410 13133 30466 17317 7888	23573 17599 47441 191788 36679 4263 13153 21949 7775	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355	-1.787 546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688
01 02 03 04 05 06 07 08	22 21 20 19 18 17 16 15	58590 31683 34444 27299 31344 35299 46685 73105 41641	14303 10066 16070 26410 13133 30466 17317 7888 7268	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355 -1.584	-1.787 546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189 144	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585
01 02 03 04 05 06 07 08 09	22 21 20 19 18 17 16 15 14	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355 -1.584 -1.241	-1.787 546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189 144 -1.869	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585
01 02 03 04 05 06 07 08 09 PV	22 21 20 19 18 17 16 15 14 13	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355 -1.584 -1.241 824	-1.787 546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189 144 -1.869 -1.529	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585 -1.585
01 02 03 04 05 06 07 08 09 PØ P1 P2	22 21 20 19 18 17 16 15 14 13 12	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562 23097	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355 -1.584 -1.514	-1.787 546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189 144 -1.869 -1.529 -1.345	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.585 -1.585 -1.585 -1.647
01 02 03 04 05 06 07 08 09 PV P1 P2 P3	22 21 20 19 18 17 16 15 14 13 12 11	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279 14851	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527 13390	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562 23097 20402	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355 -1.584 -1.241 824 -1.514 -1.828	-1.787546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189144 -1.869 -1.529 -1.345966	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.585 -1.585 -1.585 -1.585 -1.476
O1 O2 O3 O4 O5 O6 O7 O8 O9 P0 P1 P2 P3 P4	22 21 20 19 18 17 16 15 14 13 12 11	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279 14851 49330	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527 13390 3365	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562 23097 20402 19245	-1.567 -1.375 908 962 923 -1.949 257 -1.488 -1.355 -1.584 -1.241 824 -1.514 -1.828 296	-1.787546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189144 -1.869 -1.529 -1.345966 -1.839	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585 -1.585 -1.585 -1.842 -1.647 -1.476 -1.387
01 02 03 04 05 06 07 08 09 PV P1 P2 P3 P4 P5	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279 14851 49330 77939	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527 13390 3365 55897	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562 23097 20402 19245 2544	-1.567 -1.375908962923 -1.949257 -1.488 -1.355 -1.584 -1.241824 -1.514 -1.828296 -1.603	-1.787546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189144 -1.869 -1.529 -1.345966 -1.839 -1.651	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585 -1.585 -1.585 -1.476 -1.476 -1.476
01 02 03 04 05 06 07 08 09 P0 P1 P2 P3 P4 P5 P6	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279 14851 49330 77939 20918	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527 13390 3365 55897 34131	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562 23097 20402 19245 2544 28969	-1.567 -1.375908962923 -1.949257 -1.488 -1.355 -1.584 -1.241824 -1.514 -1.828296 -1.603 -1.502	-1.787546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189144 -1.869 -1.529 -1.345966 -1.839 -1.651 -1.303	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585 -1.585 -1.585 -1.476 -1.476 -1.476 -1.476 -1.499
01 02 03 04 05 06 07 08 09 P0 P1 P2 P3 P4 P5 P6 P7	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7 6	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279 14851 49330 77939 20918 29506	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527 13390 3365 55897 34131 28761	23573 17599 47441 191788 36679 4263 13153 21949 77775 14132 16458 6562 23097 20402 19245 2544 28969 18296	-1.567 -1.375908962923 -1.949257 -1.488 -1.355 -1.584 -1.241824 -1.514 -1.828296 -1.603 -1.502 -1.771	-1.787546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189144 -1.869 -1.529 -1.345966 -1.839 -1.651 -1.303 -1.642	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585 -1.585 -1.585 -1.585 -1.476 -1.476 -1.476 -1.499 014
01 02 03 04 05 06 07 08 09 P0 P1 P2 P3 P4 P5 P6	22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7	58590 31683 34444 27299 31344 35299 46685 73105 41641 13614 49042 3279 14851 49330 77939 20918	14303 10066 16070 26410 13133 30466 17317 7888 7268 14632 51261 46527 13390 3365 55897 34131	23573 17599 47441 191788 36679 4263 13153 21949 7775 14132 16458 6562 23097 20402 19245 2544 28969	-1.567 -1.375908962923 -1.949257 -1.488 -1.355 -1.584 -1.241824 -1.514 -1.828296 -1.603 -1.502	-1.787546 -1.562 -1.466 -1.512 -1.758 -1.388 -1.189144 -1.869 -1.529 -1.345966 -1.839 -1.651 -1.303	-1.681 -1.423 -1.411 -1.439 278 -1.608 -1.534 -1.688 -1.585 -1.585 -1.585 -1.476 -1.476 -1.476 -1.476 -1.499

Date: 6-23-78

						-	
RR	Hz	f	f ₂	. [£] 3	\emptyset_1	\emptyset_2	ϕ_3
Q Ø	23	58919	24254	57332	-1.692	-1.311	-1.503
Q1	22	75004	12917	45798	-1,592	-1.588	-1.458
Q2	21	97271	66288	34628	-1.551	-1.822	-1.302
Q3	20	160068	88157	189810	-1.288	-1.540	483
Q4	19	96310	80465	54703	971	-1.493	-1.757
Q5	18	75483	43072	14613	527	-1.280	-1.572
Q6	17	122135	40538	42160	255	-1.215	-1.406
Q7	16	108005	5827	41650	-1.901	-1.269	-1.592
Q8	15	147639	24857	48369	-1.686	044	-1.483
Ω̈́9	14	141654	62937	51181	-1.340	-1.631	-1.547
RØ	13	133991	85901	43247	-1.336	-1.513	-1.520
Rl	12	120133	90393	45839	-1.129	-1,496	-1.427
R2	11	82781	67966	35241	-1.038	-1.258	-1.421
R3	10	21982	28546	47867	-1.546	527	-1.565
R4	9	31992	136241	13691	-1.816	-1.745	-1.477
R5	8	46162	108999	30681	-1.542	-1.380	-1.381
R6	7	27867	81228	48302	-1.342	-1.226	-1.443
R7	6	32362	2850	52955	-1.176	-1.009	-1.533
R8	5	80294	39199	24336	-1.340	-1.759	-1.252
R9	4	60629	65215	56157	-1.608	-1.369	-1.585
				LARGE	CHECKS	•	
sø	4	97320	56905	19013	-1.213	-1.569	449
sî	5	56926	61072	48732	-1.669	-1.965	-1.534
S2	6	89976	68902	23758	336	282	340
33	7	111175	41775	23839	839	697	-1.063
54	8	129406	47716	28006	-1.166	-1.106	-1.837
S 5	9	107013	74530	4645	-1.395	-1.401	926
S6	10	127111	51227	8264	-1.616	-1.687	609
S 7	11	112558	35978	17039	-1.966	092	-1.033
S8	12	114275	33677	4043	076	542	594
59	13	96809	28810	6992	275	-1.001	449
TØ	14	112767	24158	19833	647	-1.437	054
Tl	15	63365	21127	11691	-1.082	-1.538	331
T2	16	89968	15194	23737	-1.005	-1.578	-1.315
		45540					
1.3		40048	3550	20388	-1.562	303	-1.386
T3 T4	17	40048 15650	3550 16253	20388 35342	-1.562 -1.940	303 -1.342	-1.386 467
T4	17 18	15650	16253	35342	-1.940	-1.342	467
T4 T5	17 18 19	15650 50213	16253 30929	35342 36891	-1.940 -1.799	-1.342 -1.525	467 -1.788
T4 T5 T6	17 18 19 20	15650 50213 40931	16253 30929 19798	35342 36891 310640	-1.940 -1.799 -1.774	-1.342 -1.525 228	467 -1.788 730
T4 T5 T6 T7	17 18 19 20 21	15650 50213 40931 32193	16253 30929 19798 22825	35342 36891 310640 79074	-1.940 -1.799 -1.774 270	-1.342 -1.525 228 577	467 -1.788 730 -1.487
T4 T5 T6	17 18 19 20	15650 50213 40931	16253 30929 19798	35342 36891 310640	-1.940 -1.799 -1.774	-1.342 -1.525 228	467 -1.788 730

Date: 6-23-78

RR	Hz	£		£	ď	ø	ø
RR	F12	fl	£2	f ₃	$\varnothing_{\mathtt{l}}$	ø ₂	ø ₃
				- 4 - 4 - 11			
UØ.	4	45303	37095	34252	-1.422	258	-1.340
UL.	5	47257	1389	27097	-1.788	-1.112	-1.790
U2	6	20163	34622	26641	351	-1.333	-1.208
บ3	7	32600	31848	20493	602	-1.390	-1.777
U4	8	103494	51466	12361	-1.402	-1.735	263
U5	9	27352	10080	8715	-1.848	981	-1.427
U6	10	24763	24971	16644	100	-1.790	-1.523
ט7	11	42702	45708	15207	781	-1.131	-1.609
U8	12	32842	43014	12842	755	-1.555	-1.538
ຫ [ຼ]	13	56592	33771	46650	-1.157	-1.609	-1.469
VØ	14	89821	24006	35968	-1.176	-1.526	-1.441
V1	15	20751	34267	40169	-1.406	-1.469	~1.514
V2	16	113425	70407	60772	-1.738	-1.531	-1.495
V3	17	21541	33757	35741	032	-1.541	-1.477
V4	18	64571	31040	22713	-1.608	-1.513	-1.584
V 5	19	59144	41335	56237	-1.650	-1.423	-1.562
V6	20	48774	45712	262017	042	-1.524	030
V 7	21	24531	23974	95233	-1.289	-1.507	-1.461
V8	22	47188	34029	35924	-1.239	-1.532	-1.588
V9	23	52135	27614	61643	-1.174	-1.586	-1.498
المريب المنادد		——————————————————————————————————————		***			·
				UNPA	TTERNED		
Wild	4	29048	40757	, . ,	**************************************	-1.538	-1.511
WE WI	4 5	29048 33760	40757 35270	62189	-1.912	-1.538 -1.771	-1.511 -1.620
Wl	4 5 6	33760	35270	62189 21675	-1.912 -1.521	-1.771	-1.620
W1 W2	4 5 6 7	33760 22127	35270 20244	62189 21675 50923	-1.912 -1.521 -1.646	-1.771 739	-1.620 -1.518
Wl	5 6 7	33760 22127 16946	35270	62189 21675	-1.912 -1.521 -1.646 -1.537	-1.771	-1.620
W1 W2 W3 W4	5 6 7 8	33760 22127 16946 41545	35270 20244 76120 114697	62189 21675 50923 32170 26641	-1.912 -1.521 -1.646 -1.537 -1.395	-1.771 739 -1.170	-1.620 -1.518 -1.492 -1.452
W1 W2 W3	5 6 7	33760 22127 16946	35270 20244 76120	62189 21675 50923 32170	-1.912 -1.521 -1.646 -1.537	-1.771 739 -1.170 -1.509 -1.861	-1.620 -1.518 -1.492
W1 W2 W3 W4 W5	5 7 8 9	33760 22127 16946 41545 42620	35270 20244 76120 114697 93018	62189 21675 50923 32170 26641 47858	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929	-1.771 739 -1.170 -1.509	-1.620 -1.518 -1.492 -1.452 -1.477
W1 W2 W3 W4 W5 W6	5 6 7 8 9	33760 22127 16946 41545 42620 7920	35270 20244 76120 114697 93018 54109	62189 21675 50923 32170 26641 47858 47217	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754	-1.771 739 -1.170 -1.509 -1.861 638	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583
W1 W2 W3 W4 W5 W6 W7	5 6 7 8 9 10 11	33760 22127 16946 41545 42620 7920 49025	35270 20244 76120 114697 93018 54109 93254	62189 21675 50923 32170 26641 47858 47217 27182	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998	-1.771 739 -1.170 -1.509 -1.861 638 -1.339	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609
W1 W2 W3 W4 W5 W6 W7 W8 W9	5 6 7 8 9 10 11 12	33760 22127 16946 41545 42620 7920 49025 101079	35270 20244 76120 114697 93018 54109 93254 74540	62189 21675 50923 32170 26641 47858 47217 27182 38526	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394
W1 W2 W3 W4 W5 W6 W7 W8	5 6 7 8 9 10 11 12 13	33760 22127 16946 41545 42620 7920 49025 101079 116394	35270 20244 76120 114697 93018 54109 93254 74540 47197	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582 -1.559	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521
W1 W2 W3 W4 W5 W6 W7 W8 W9 X8	5 6 7 8 9 10 11 12 13	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582 -1.559 -1.661	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383
W1 W2 W3 W4 W5 W6 W7 W8 W9 X1	5 6 7 8 9 10 11 12 13 14 15	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582 -1.559 -1.661 059	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451
W1 W2 W3 W5 W6 W7 W8 W9 W1 X1 X2	5 6 7 8 9 10 11 12 13 14 15 16	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085 123390	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206 12713	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674 38539	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718 -1.940	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582 -1.559 -1.661 059 872	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451
W123 W4 W5 W7 W8 W7 X1 X1 X1 X1	5 6 7 8 9 10 11 12 13 14 15 16 17	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085 123390 104021	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206 12713 46492	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674 38539 33137	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718 -1.940 202	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582 -1.559 -1.661 059 872 -1.218	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451 -1.457 -1.504
W1 W3 W4 W5 W6 W7 W8 W9 XX XX XX XX	5 6 7 8 9 10 11 12 13 14 15 16 17 18	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085 123390 104021 113718	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206 12713 46492 60958	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674 38539 33137 10907	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718 -1.940 202 438	-1.771739 -1.170 -1.509 -1.861638 -1.339 -1.582 -1.559 -1.661059872 -1.218 -1.362	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451 -1.457 -1.504 -1.742
W12 W3 W4 W5 W6 W7 W8 W XX X	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085 123390 104021 113718 104992	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206 12713 46492 60958 74396	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674 38539 33137 10907 58072	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718 -1.940 202 438 892	-1.771 739 -1.170 -1.509 -1.861 638 -1.339 -1.582 -1.559 -1.661 059 872 -1.218 -1.362 -1.574	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451 -1.457 -1.504 -1.742 -1.776
W W W W W W W W W X X X X X X X X X X X	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085 123390 104021 113718 104992 159924	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206 12713 46492 60958 74396 64037	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674 38539 33137 10907 58072 304145	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718 -1.940 202 438 892 -1.309	-1.771739 -1.170 -1.509 -1.861638 -1.339 -1.582 -1.559 -1.661059872 -1.218 -1.362 -1.574 -1.769	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451 -1.457 -1.504 -1.742 -1.776
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	33760 22127 16946 41545 42620 7920 49025 101079 116394 127208 120085 123390 104021 113718 104992 159924 106855	35270 20244 76120 114697 93018 54109 93254 74540 47197 45376 17206 12713 46492 60958 74396 64037 51328	62189 21675 50923 32170 26641 47858 47217 27182 38526 41914 28819 33674 38539 33137 10907 58072 304145 43296	-1.912 -1.521 -1.646 -1.537 -1.395 -1.754 -1.929 998 -1.231 -1.351 -1.557 -1.718 -1.940 202 438 892 -1.309 -1.421	-1.771739 -1.170 -1.509 -1.861638 -1.339 -1.582 -1.559 -1.661059872 -1.218 -1.362 -1.574 -1.769 -1.852	-1.620 -1.518 -1.492 -1.452 -1.477 -1.583 -1.609 -1.394 -1.521 -1.383 -1.451 -1.457 -1.504 -1.742 -1.776 902 -1.364

Date: 6-26-78

							_
RR	Hz	fl	f ₂	£3	ø _l	ø ₂	ø ₃
ΥØ	4	56177	49453	73818	-1.547	-1.342	-1.461
Yl	5	68217	70706	36824	-1.624	-1.653	-1.511
Y2	6	30405	11027	67574	-1.725	053	-1.493
Y3	7	42417	67935	16191	-1.594	-1.072	-1.623
¥4	8	41156	117412	29724	-1.551	-1.373	-1.469
Y5	9	65200	121571	56694	-1.617	-1.814	-1.453
Y6	10	44224	74623	37421	188	541	-1.657
¥7	1.1	70900	100436	19601	901	-1.279	-1.743
Y8	12	106135	79263	27953	-1.144	-1.481	-1.375
Y9	13	107025	42386	34902	-1.308	-1.611	-1.513
zø	14	98907	63300	43550	-1.461	-1.742	-1.294
Zl	15	164834	39173	32704	-1.670	-1.958	-1.537
Z 2	16	161755	24003	27709	026	724	-1.465
Z 3	17	136311	37491	25119	288	-1.025	-1.561
Z4	18	155255	47789	14010	512	-1.291	972
Z 5	19	182898	66043	30189	871	-1.542	-1.891
Z 6	20	58804	82330	166607	-1.027	-1.657	935
27	21	74385	48388	22682	-1.429	028	-1.599
z 8	22	57647	19649	22486	-1.325	541	-1.522
Z 9	23	54817	35395	28843	-1.573	846	-1.337
				UNPA	TTERNED		
ØA	23	71845	29687	26520	-1.556	757	-1.500
1A	22	97872	20946	8928	-1.445	306	-1.781
2A	21	108146	42769	40379	-1.292	-1.885	-1.444
3A	20	158471	48162	128540	-1.180	-1.747	305
4A	19	155508	91072	28320	876	-1.480	-1.918
5A	18	126780	57207	5091	578	-1.175	-1.117
6A	17	129391	47648	30099	209	982	-1.459
7A	16	146956	8907	22703	-1.911	545	-1.539
8A	15	143609	24743	32681	-1.654	-1.916	-1.448
9A	14	125178	58741	6841	-1.492	-1.726	-1.748
ØB	13	121121	45592	32944	-1.312	-1.558	-1.615
18	12	105519	90069	26102	-1.162	-1.410	-1.373
2B	11	124707	91403	27163	936	-1.187	-1.466
3B	10	225792	159016	41891	-1.049	-1.571	-1.760
4B	9	32517	128006	48824	-1.758	~1.967	-1.543
5B	8	24698	117968	18832	-1.753	-1.496	-1.641
6B	7	29046	88847	24177	-1.532	-1.233	-1.158
7B	6	10607	21528	27656	-1.832	838	-1.595
8B	5	34440	47911	9833	-1.524	-1.665	-1.181
9B	4	69134	31834	42578	-1.648	-1.508	-1.563

LARGE CHECKS

Date:	8-4-7	8		LARGE	CHECKS		
RR	Hz	f ₁	f ₂	f ₃	Ø ₁	ø ₂	ø ₃
ØС	4	63956	66103	22466	-1.333	-1.545	-1.42
ic	5	72670	49857	78342	-1.441	-1.694	-1.5]
2C	5 6	70099	39891	59298	-1.442	-1.492	-1.50
3C		64060 91724	42376 67345	62652 56159	-1.281	-1.423	-1.48
4C 5C	8 9	91724	65211	56159 57857	-1.360 -1.517	-1.407 -1.545	-1.45 -1.46
5C 6C	10	105802	77726	5/85/ 64930	-1.51/ -1.614	-1.545 -1.542	-1.46
7C	11	69183	40732	46984	-1.776	-1.542 -1.580	-1.40
8C	12	65716	32516	61055	-1.776 -1.925	-1.511	~1.50
9C	13	16443	62606	64051	723	-1.429	-1.43
ØD	14	29767	56849	52371	-1.180	-1.439	-1.55
110 110	15	101770	56563	56746	-1.272	-1.572	-1.53
2D	16	110703	46329	57817	-1.355	-1.548	-1.42
31D	17		59107	80786	-1.584	-1.495	-1.49
4D	18	98562	68769	68072	-1.683	-1.467	-1.48
5D	19	70699	64338	47950	-1.693	-1.471	-1.37
6D	20	29160	46978	422315	-1.552	-1.532	63
7D	21	31515	46656	47596	-1.534	-1.404	-1.58
8D	22	52114	68404	53085	-1.363	-1.486	-1.64
9D	23	39320	84324	42075	-1.572	-1.453	-1.57
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		· · · · · · · · · · · · · · · · · · ·		LARGE	CHECKS		a de la companya de l
9E	4	125341	82750	52275	-1.476	-1.530	-1.36
1E	5	80531	69641	60752	-1.624	-1.683	-1.52
2E	6	20211	33080	54002	-1.559	-1.529	-1.50
3E	7	48512	42226	67262	-1.323	-1.294	-1.50
4E	8	97126	60537	52615	-1.281	-1.191	-1.43
5E	9	94654	62113	48700	-1.421	-1.400	-1.48
6E	10	114625	66911	60443	-1.568	-1.572	-1.48
7E	11	28410	18265	49483	-1.589	-1.182	-1.39
8E	12	12771	37720	40037	-1.905	-1.218	-1.55
9E	13	27111	69073	51.009	192	-1.443	-1.49
9 F	14	17482	43804	49577	828	-1.605	-1.49
1F	15	89826	61252	30938	-1.051	-1.490	-1.3
2F	16	104417	51682	55129	-1.375	-1.509	-1.54
3F	17	91893	64809	59376	-1.481	-1.544	-1.55
4F	18	96504	62955	76271	-1.618	-1.535	-1.56
5F	19	59773	68433	57217	-1.646	-1.458	-1.3
6F	20	57098	49231	351925	-1.694	-1.401	- ,5
7F	21	39000	58212	32490	-1.543	-1.467	-1.7
8F	22	31430	35062	49444	-1.419	-1.412	-1.3
9F	23	67101	77552	49668	-1.531	-1.422	-1.39
				A-31			
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Date: 8-7-78 PATTERNED BACKGROUND - EYES OPEN	ate:	8-7-78	PATTERNED	BACKGROUND -	EYES OPE	V
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RR	Hz	f ₁	£2	f ₃	$\emptyset_1$	$\emptyset_2$	ø ₃
		<b></b>					<b></b>
ØG	4	35628	40359	34243	-1.549	-1.623	-1.556
1G	5	31530	25084	32817	-1.416	-1.431	-1.421
2G	6	27596	37806	27778	-1.331	-1.508	-1.483
3G	7	30076	31072	31088	-1.199	-1.524	-1.489
4G	8	37840	42718	24638	-1.479	-1.401	-1.560
5G	9	28670	29710	15591	-1.500	-1.668	-1.379
6G	10	29559	31501	25878	-1.221	-1.254	-1.275
7G	11	36060	33361	22935	-1.474	-1.500	-1.453
8G	12	29412	28423	26678	-1.610	-1.524	-1.521
9G	13	21525	39543	32962	-1.350	-1.553	-1.346
ØН	14	35543	28852	31292	-1.501	-1.550	-1.386
lH	15	40178	20668	36206	-1.507	-1.427	-1.466
2H	16	23084	41542	23392	-1.276	-1.550	-1.800
3H	17	21316	21698	34269	-1.611	-1.491	-1.405
4H	18	22233	37148	38268	-1.600	-1.519	-1.543
5H	19	23539	25233	27481	-1.404	-1.378	910
6H	20	45670	26290	521802	-1.526	-1.491	387
7H	21	17866	37473	45538	-1.482	-1.526	113
8H	. 22	16436	28701	27927	-1.315	-1.432	-1.487
9H	23	41115	40416	8776	-1.515 -1.526	-1.434	069
חכ	23	41112	40410	0//0	-1.520	-1.434	009
		UNP	ATTERNED I	BACKGROUND	- EYES OPI	en e	
-						<del>, , , , , , , , , , , , , , , , , , , </del>	
ØI	4	74698	21666	15886	960	-1.698	-1.851
lI	5	22413	31131	25562	-1.491	-1.501	-1.488
2I	6	28422	29665	24045	-1.501	-1.493	-1.550
31	7	17584	20974	26923	-1.662	-1.496	-1.576
<b>4</b> I	8	18170	39937	22558	-1.296	-1.453	-1.438
<b>5</b> I	9	24452	30685	27743	-1.638	-1.380	-1.480
<b>6</b> I	10	30304	33148	22748	-1.702	-1.343	-1.494
<b>7</b> I	11	19819	26199	28417	-1.390	-1.468	-1.525
81	12	16414	11262	25480	-1.198	-1.620	-1.562
91	13	28552	29872	29704	-1.575	-1.650	-1.519
ØJ	14	31589	21040	27083	-1.654	-1.552	-1.574
'n	15	11340	24066	18145	-1.795	-1.533	-1.504
2,7	16	21773	31018	26102	-1.608	-1.552	-1.518
3J			2002c	11985	-1.536	-1.512	-1.511
	17	24669	28926				
<b>4</b> J	18	25517	24005	43985	-1.674	-1.444	-1.297
4J 5J	18 19	25517 5675	24005 20728	43985 39281	-1.674 -1.598	-1.444 -1.547	-1.297 -1.036
4J 5J 6J	18 19 20	25517 5675 28231	24005 20728 29441	43985 39281 523507	-1.674 -1.598 -1.357	-1.444 -1.547 -1.274	-1.297 -1.036 -1.393
4J 5J 6J 7J	18 19 20 21	25517 5675 28231 20932	24005 20728 29441 5929	43985 39281 523507 42463	-1.674 -1.598 -1.357 -1.539	-1.444 -1.547 -1.274 -1.358	-1.297 -1.036 -1.393 -1.880
4ゴ 5ゴ 6ゴ 7ゴ 8ゴ	18 19 20 21 22	25517 5675 28231 20932 27029	24005 20728 29441 5929 28060	43985 39281 523507 42463 24010	-1.674 -1.598 -1.357 -1.539 -1.475	-1.444 -1.547 -1.274 -1.358 -1.48J	-1.297 -1.036 -1.393 -1.880 -1.540
4J 5J 6J 7J	18 19 20 21	25517 5675 28231 20932	24005 20728 29441 5929	43985 39281 523507 42463	-1.674 -1.598 -1.357 -1.539	-1.444 -1.547 -1.274 -1.358	-1.297 -1.036 -1.393 -1.880

Date: 8-30-78

RR	Hz	fl	f ₂	f ₃	ø ₁	ø ₂	ø ₃
ØK	23	37568	29030	49974	-1.503	-1.508	-1.503
1K	22	44887	42497	42257	-1.558	-1.489	-1.518
2K	21	40039	38535	51598	-1.560	-1.543	-1.496
3K	20	47558	37975	75405	-1.407	-1.500	-1.483
4K	19	29285	46787	42749	-1.513	-1.506	-1.490
5K	18 17	36601 32176	41596 41062	39430 40626	-1.571 -1.304	-1.477	-1.485
6K 7K	16	28676	37909	38309	-1.441	-1.451 -1.552	-1.451 -1.506
8K	15	30741	36567	41316	-1.390	-1.352 -1.469	-1.467
9K	14	20820	42225	42807	-1.481	-1.472	-1.487
ØĽ.	13	48153	32361	36801	-1.232	-1.530	-1.454
îĹ	12	21518	42101	36641	-1.305	-1.505	-1.453
<u>2L</u>	11	73206	43588	38909	-1.616	-1.563	-1.617
3 <u>T</u>	10	75315	33586	34450	-1.339	-1.369	-1.490
4 <u>L</u>	9	59177	24610	36236	-1.359	-1.593	-1.506
5 <u>L</u>	8	58249	42158	36800	-1.370	-1.470	-1.500
6L	7	7770	36230	33487	-1.872	-1.531	-1.537
7 <u>L</u>	6	48316	39170	36516	046	-1.550	-1.500
8L	5	46238	51877	37140	-1.661	-1.378	-1.360
9L	4	88607	16948	37823	-1.479	-1.283	-1.477
<del>,</del>				SMALI	CHECKS		
ØM	4	85947	1,9474	29601	-1.571	-1.038	-1.446
1M	5 6	77205	50181	32309	-1.982	-1.498	-1.444
2M	6	19798	41294	42930	208	-1.613	-1.570
3M	7	44444	26398	28792	497	-1.393	-1.365
4M	8	32172	30247	29957	-1.087	-1.482	-1.507
5M	9	12400	23595	30243	-1.419	-1.604	-1.501
6M 7M	10 11	40288 98035	24497 33902	34247 25098	-1.508	-1.559	-1.530
/M 8M	12	26227	33902 31600	25098 26802	-1.480 -1.820	-1.410 -1.452	-1.456 -1.413
9M	13	20242	27987	26568	-1.721	-1.432	-1.440
ON N	14	19381	30509	27820	-1.462	-1.503	-1.512
1N	15	32563	28122	25606	-1.591	-1.610	-1.532
2N	16	27354	23048	40432	-1.287	-1.444	-1.452
3N	17	36450	27286	28415	-1.520	-1.541	-1.524
4N	18	56951	24385	24759	-1.422	-1.504	-1.458
5N	19	36823	30129	28981	-1.635	-1.458	-1.520
6N	20	24237	20488	43874	-1.724	-1.557	-1.293
7N	21	14897	23078	24004	-1.241	-1.429	-1.487
810	22	19989	23606	23966	-1.168	-1.397	-1.432
9N	23	24496	30013	30849	-1.540	-1.545	-1.495
				A-33			

Date: 9-6-78 PATTERNED BACKGROUND - EYES OPEN

10 5 38219 31239 29929 -1.515 -1.402 -1.541 20 6 45822 62493 25572 -1.177 -1.442 -1.432 30 7 11197 14280 20340 -1.452 -1.681 -1.421 40 8 37315 31773 30867 -1.472 -1.500 -1.547 50 9 26897 15859 30113 -1.061 -1.134 -1.332 60 10 50277 21127 27137 -1.538 -1.459 -1.377 70 11 38368 65370 43467187 -1.754 -1.555 80 12 15130 24020 24978 -1.557 -1.480 -1.441 90 13 25728 33003 24715 -1.406 -1.522 -1.489 ØP 14 14091 19078 33793 -1.413 -1.552 -1.372 2P 16 23315 20467 28395 -1.299 -1.304 -1.356 3P 17 26614 31829 27841 -1.509 -1.482 -1.357 4P 18 31584 29890 30983 -1.565 -1.560 -1.431 5P 19 27938 29478 28822 -1.544 -1.511 -1.515 6P 20 25649 35717 26594 -1.769 -1.610191 7P 21 26329 26920 30649 -1.494 -1.315 -1.367 8P 22 7261 36149 18924 -1.281 -1.439 -1.306 9P 23 16345 35159 23964 -1.654 -1.403 -1.520  UNDATTERNED BACKGROUND - EYES OPEN	RR	Hz	fl	f ₂	f ₃	ø _l	ø ₂	ø ₃
20 6 45822 62493 25572 -1.177 -1.442 -1.432								-1.452
30 7 11197 14280 20340 -1.452 -1.681 -1.421 40 8 37315 31773 30867 -1.472 -1.500 -1.547 50 9 26897 15859 30113 -1.061 -1.134 -1.332 60 10 50277 21127 27137 -1.538 -1.459 -1.371 70 11 38368 65370 43467187 -1.754 -1.555 80 12 15130 24020 24978 -1.557 -1.480 -1.471 90 13 25728 33003 24715 -1.406 -1.522 -1.489  GP 14 14091 19078 33793 -1.413 -1.352 -1.372 1P 15 25304 28433 30168 -1.585 -1.529 -1.437 2P 16 23315 20467 28395 -1.299 -1.304 -1.352 4P 18 31584 29890 30983 -1.565 -1.560 -1.431 5P 19 27938 29478 28822 -1.544 -1.511 -1.513 6P 20 25649 35717 26594 -1.769 -1.610 -1.91 7P 21 26329 26920 30649 -1.494 -1.315 -1.365 8P 22 7261 36149 18924 -1.654 -1.403 -1.526  UNPAUTERNED BACKGROUND - EYES OPEN   AA 23 24730 32174 25362 -1.344 -1.551 -1.472 -0.001 AD 20 37153 29089 221357 -1.435 -1.439 -1.356 AC 21 27075 27802 40534 -1.480 -1.472 -0.001 AD 20 37153 29089 221357 -1.435 -1.403 -1.526   AA 23 24730 32174 25362 -1.344 -1.551 -1.475 -1.474 AG 17 25573 25028 23673 -1.515 -1.575 -1.475 AF 18 37679 37685 75302 -1.612 -1.475 -1.411 AG 17 25573 25028 23673 -1.515 -1.575 -1.457 AH 16 27571 18915 22874 -1.513 -1.405 -1.386 AI 15 15967 25411 23911 -1.361 -1.565 -1.556 AI 14 29330 24691 18340 -1.630 -1.516 -1.543 AK 13 10684 19552 32451 -1.361 -1.361 -1.565 AI 14 29330 24691 18340 -1.630 -1.516 -1.544 AN 10 32182 21137 30411 -1.785 -1.489 -1.444 AO 9 45887 .75544 23331 -1.146 -1.406 -1.504 AP 8 72960 46802 24594 -1.458 -1.369 -1.448 AO 9 45887 .75544 23331 -1.146 -1.406 -1.504 AP 8 72960 46802 24594 -1.458 -1.369 -1.448 AO 9 45887 .75544 23331 -1.146 -1.406 -1.504 AP 8 72960 46802 24594 -1.458 -1.369 -1.448 AO 9 45887 .75544 23331 -1.156 -1.557 -1.557 AF AF 6 15147 27664 30988 -1.673 -1.561 -1.435 AF 1 14664 24292 27901 -1.559 -1.555 -1.557 AF 6 15147 27664 30988 -1.673 -1.561 -1.435 AF 1 16664 24292 279								
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#### APPENDIX B

## Regression Coefficients

# I. PHASE - Three degrees of freedom

RMDA 
$$y = .0294x^2 - .5323x - 0.589$$

RMDA  $y = .0032x^2 - .1418x - 1.4560$ 

RMDI  $y = .2105x^2 - .2132x - .7214$ 

LPZØ  $y = -.1015x^2 + .7983x - 2.1826$ 

LPXØ  $y = .0329x^2 - .6325x + .2148$ 

LPTØ  $y = .0029x^2 - .6325x - .8503$ 

RRØM  $y = .0029x^2 - .3366x - .2865$ 

RRØM  $y = .0037x^2 - .7141x + 1.0641$ 

RRWØ  $y = .0074x^2 - .3261x - .4714$ 

SPEK  $y = .0074x^2 - .3261x - .4714$ 

### II. AMPLITUDE - Four degrees of freedom

RMAA 
$$y = -.0072x^3 + .1994x^2 - 3.6353x + 53.9340$$

RMYØ - DA  $y = .3747x^3 - 12.6295x^2 + 152.4572x - 343.544$ 

RMDA  $y = .1447x^3 - 8.4724x^2 + 121.0685x - 250.792$ 

RMØA - EA  $y = -.1053x^3 + 3.9425x^2 - 35.5912x + 183.6381$ 

RMØA  $y = -.0007x^3 + 2.0202x^2 - 20.4195x + 165.4450$ 

RMWØ - FA  $y = -1.0933x^3 + 20.0573x^2 - 106.407x + 273.1473$ 

#### II. AMPLITUDE cont.

RRØI - AA

y =

RMØT 
$$y = -1.1305x^3 + 21.3911x^2 - 116.556x + 280.5491$$

RMØQ - ØX  $y = -.1239x^3 + 2.8236x^2 - 25.8911x + 112.3798$ 

LPØB - NØ  $y = 2.8894x^3 - 54.2895x^2 + 395.7388x - 739.022$ 

LPØB - NØ  $y = .37804x^3 - 72.0054x^2 + 533.9489x - 1071.51$ 

LPPØ - ØL  $y = .2111x^3 - 5.8366x^2 + 54.4187x + 19.6811$ 

LPRØ  $y = 1.1235x^3 - 24.1156x^2 + 206.5515x - 427.354$ 

LPEØ - TØ  $y = .0675x^3 + 3.1828x^2 - 14.9686x + 84.9571$ 

LPTØ  $y = .0071x^3 + 6.8095x^2 - 59.5138x + 258.6053$ 

LPØN  $y = .3909x^3 - 7.9765x^2 + 65.4728x - 150.466$ 

LPØP  $y = .0220x^3 - .4149x^2 + 2.7508x + 41.6054$ 

RRUØ - ØM  $y = -.2906x^3 + 5.9284x^2 - 50.0475x + 189.5445$ 

RRØM  $y = -.3931x^3 + 8.4972x^2 - 76.6056x + 277.9998$ 

RRØØ - ØA  $y = -.7072x^3 - 14.9137x^2 - 114.870x + 321.7287$ 

RRØØ - SØ  $y = .0917x^3 - 2.5825x^2 + 26.9147x + .8586$ 

RRØØ  $y = -.5895x^3 + 12.5922x^2 - 97.0847x + 261.4221$ 

RRØØ  $y = -.1842x^3 + 1.2281x^2 + 10.6877x + 23.3075$ 

RRØS - ØO  $y = .0576x^3 - 1.1628x^2 + 8.9955x + 9.7553$ 

RRØI - AA

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#### 18. SUPPLEMENTARY NOTES

Thesis for partial fulfillment of the requirement for a Master of Science in Physiological Optics

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Visual Evoked Response Electrophysiology Contrast Sensitivity Steady-state VER

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Electrophysical and psychophysical evidence indicates that there are channels in the visual system that are more sensitive to either spatiallystructured stimuli or luminance-modulated stimuli. This sensitivity or tuning was demonstrated by having the largest or optimum response produced by either spatially-structured or luminance-modulated stimuli. The purpose of this study is to determine if the steady-state visually evoked response to three stimuli is significantly and predictably altered by the choice of temporal

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frequency. It is expected that, for each observer, there will be an optimal temporal frequency or frequencies corresponding to a given pattern size, contrast and intensity. Also, this relationship will likely vary between individuals, but will remain relatively constant for a given observer over time.

Three subjects were each presented with three stimuli. These stimuli were: (1) a square pattern of small checks where each check subtended 15 minutes of arc; (2) a square pattern of large checks where each check subtended 57 minutes of arc; and (3) an unpatterned square stimulus. The check stimuli were presented in such a manner that alternate checks were 1800 out of phase with each other and the unpatterned stimulus was presented as a luminance charge. Each stimulus presentation series contained 20 temporal frequencies presented in numerical sequence with the lowest frequency being 4 Hz and the highest at 23 Hz.

The results of this study were plotted using either the relative amplitude of response or phase change as a function of the temporal frequency of the stimulus. When comparing each subject's response, the relative amplitude, curve shape, stimulus frequency of the largest response, and signal-to-noise ratio were considered. None of the subjects responded in exactly the same manner.

The results of this study were compared to the studies conducted by Regan (1977, 1978), Tyler, Apkarian, and Nakayama (1978), Spekreijse, Estevez, and Reits (1977), and van der Tweel and Verduyn (1965). The response manifested by the subjects in this study were similar to the studies to which they were compared.

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